

# EE101: Diode circuits

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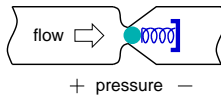
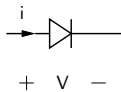
**M. B. Patil**

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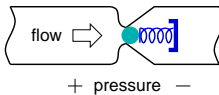
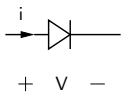
[www.ee.iitb.ac.in/~sequel](http://www.ee.iitb.ac.in/~sequel)

Department of Electrical Engineering  
Indian Institute of Technology Bombay

# Diodes

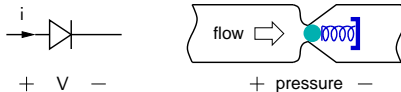


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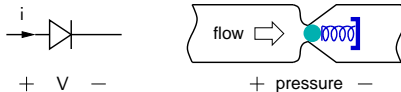
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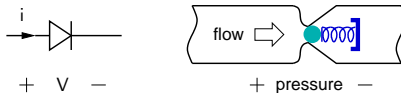
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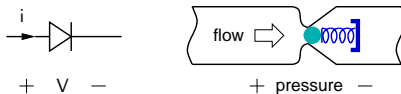


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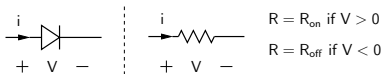


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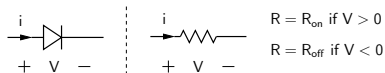
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- \* In the reverse direction, the diode resistance is much larger and may often be treated as infinite (i.e., the diode may be replaced by an open circuit).

## Simple models: $R_{\text{on}}/R_{\text{off}}$ model



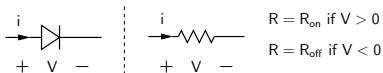


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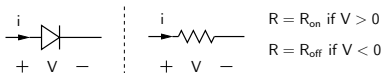
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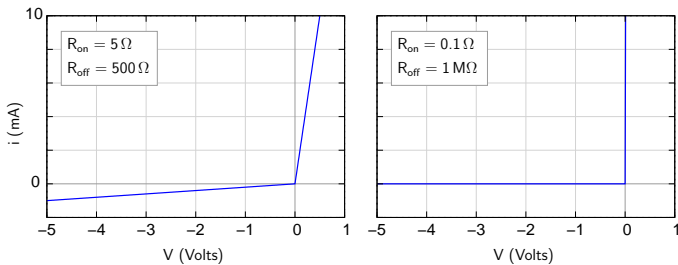


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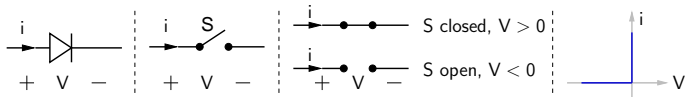
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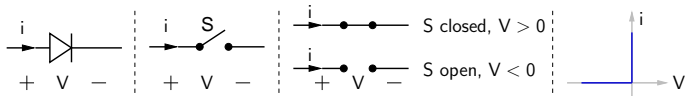
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## Simple models: ideal switch

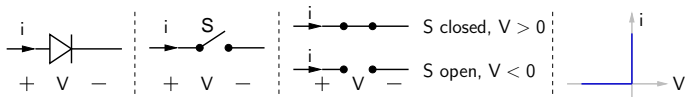


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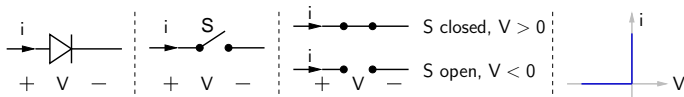
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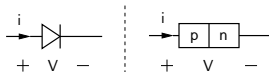
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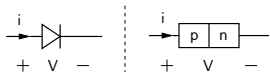
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- \* The actual values of  $V$  and  $i$  for a diode in a circuit get determined by the  $i$ - $V$  relationship of the diode *and* the constraints on  $V$  and  $i$  imposed by the circuit.

# Shockley diode equation





## Shockley diode equation



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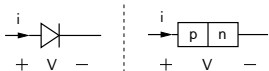
$k_B$  = Boltzmann's constant =  $1.38 \times 10^{-23} \text{ J/K}$ .

$q$  = electron charge =  $1.602 \times 10^{-19} \text{ Coul}$ .

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$V_T \approx 25 \text{ mV}$  at room temperature ( $27^{\circ}\text{C}$ ).

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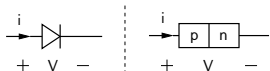
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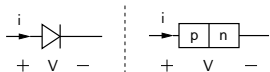
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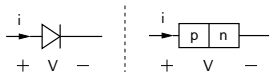
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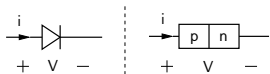
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- \* The “turn-on” voltage ( $V_{\text{on}}$ ) of a diode depends on the value of  $I_s$ .  $V_{\text{on}}$  may be defined as the voltage at which the diode starts carrying a substantial forward current (say, a few mA).  
For a silicon diode,  $V_{\text{on}} \approx 0.7 \text{ V}$ .  
For a GaAs diode,  $V_{\text{on}} \approx 1.1 \text{ V}$ .

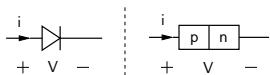
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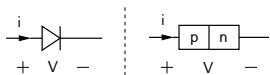


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$V$	$x = V/V_T$	$e^x$	$i$ (Amp)
0.1	3.87	$0.479 \times 10^2$	$0.469 \times 10^{-11}$
0.2	7.74	$0.229 \times 10^4$	$0.229 \times 10^{-9}$
0.3	11.6	$0.110 \times 10^6$	$0.110 \times 10^{-7}$
0.4	15.5	$0.525 \times 10^7$	$0.525 \times 10^{-6}$
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0.62	24.0	$0.260 \times 10^{11}$	$0.260 \times 10^{-2}$
0.64	24.8	$0.565 \times 10^{11}$	$0.565 \times 10^{-2}$
0.66	25.5	$0.122 \times 10^{12}$	$0.122 \times 10^{-1}$
0.68	26.3	$0.265 \times 10^{12}$	$0.265 \times 10^{-1}$
0.70	27.1	$0.575 \times 10^{12}$	$0.575 \times 10^{-1}$
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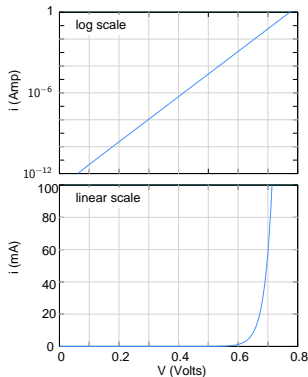
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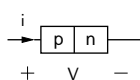
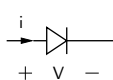
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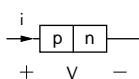
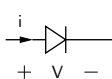


## Shockley equation and simple models

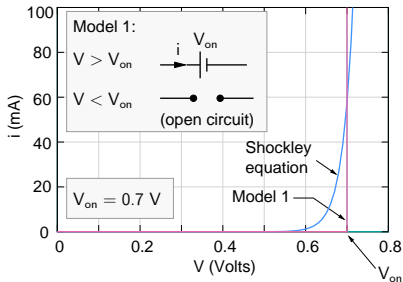


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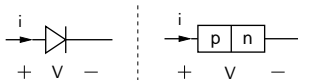
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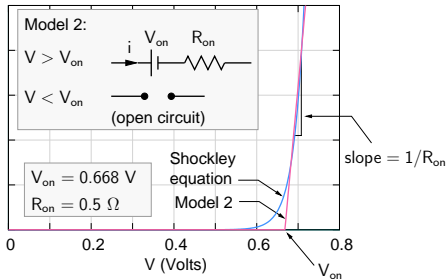
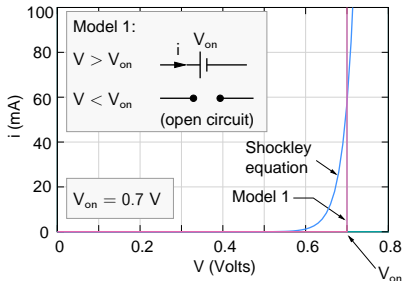
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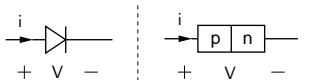
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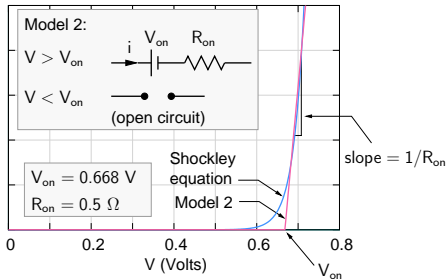
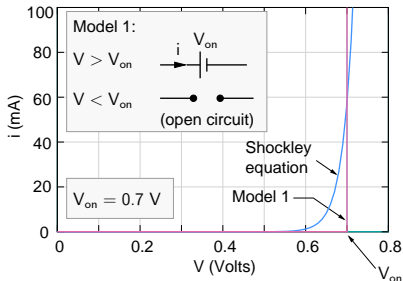
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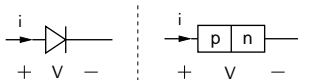


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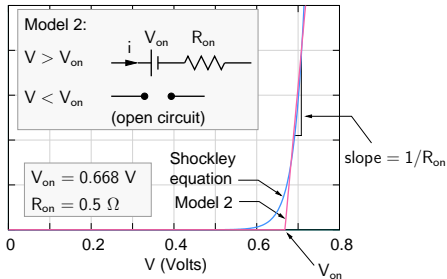
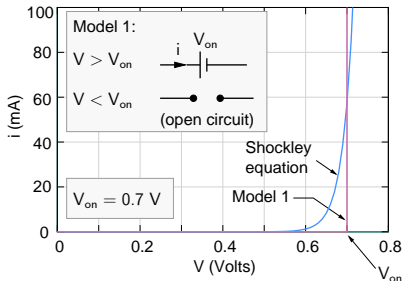


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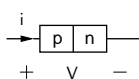
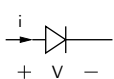


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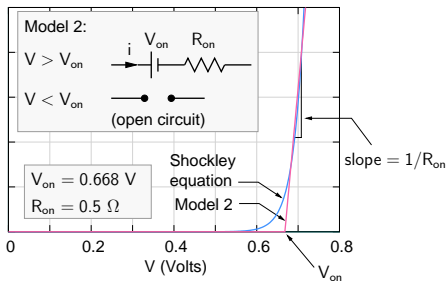
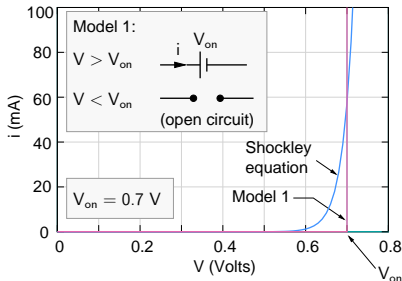


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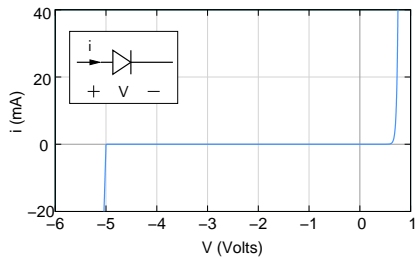


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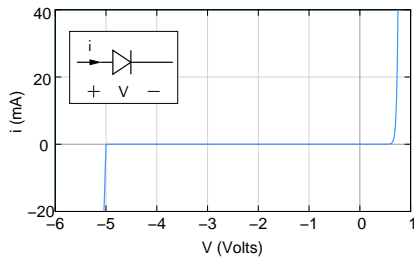


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- \* Note that the “battery” shown in the above models is not a “source” of power! It can only absorb power (see the direction of the current), causing heat dissipation.

## Reverse breakdown



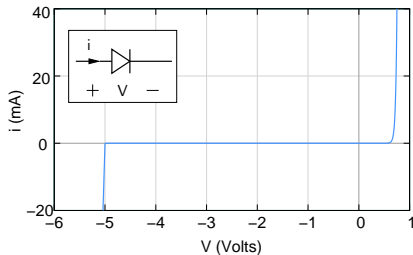
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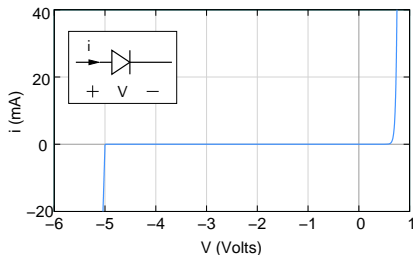


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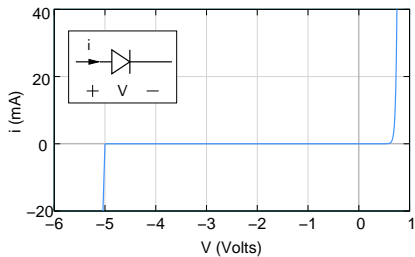
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- \* A real diode cannot withstand indefinitely large reverse voltages and “breaks down” at a certain voltage called the “breakdown voltage” ( $V_{BR}$ ).

## Reverse breakdown



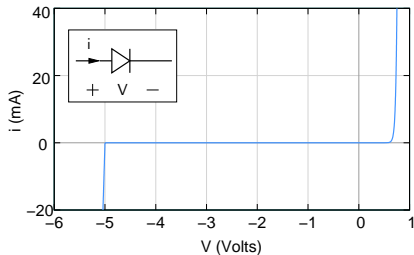
- \* In the reverse direction, an ideal diode presents a large resistance for *any* applied voltage.
- \* A real diode cannot withstand indefinitely large reverse voltages and “breaks down” at a certain voltage called the “breakdown voltage” ( $V_{BR}$ ).
- \* When the reverse bias  $V_R > V_{BR}$ , the diode allows a large amount of current. If the current is not constrained by the external circuit, the diode would get damaged.

## Reverse breakdown



Symbol for a Zener diode

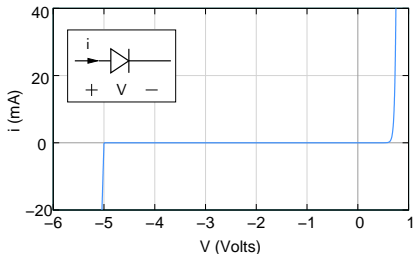
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Symbol for a Zener diode

- \* A wide variety of diodes is available, with  $V_{BR}$  ranging from a few Volts to a few thousand Volts! Generally, higher the breakdown voltage, higher is the cost.

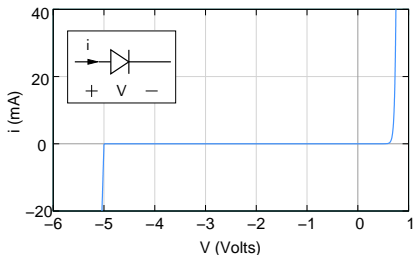
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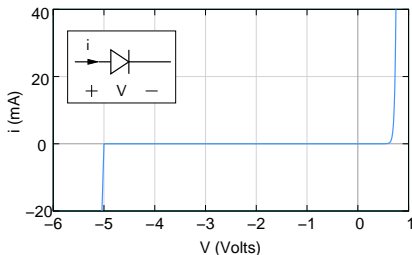
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- \* Typically, circuits are designed so that the reverse bias across any diode is less than the  $V_{BR}$  rating for that diode.
- \* “Zener” diodes typically have  $V_{BR}$  of a few Volts, which is denoted by  $V_Z$ . They are often used to limit the voltage swing in electronic circuits.

## Diode types

Apart from their use as switches, diodes are also used for several other purposes. The choice of materials used, fabrication techniques, and packaging depend on the functionality expected from the device.



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- \* **Light-emitting diodes (LEDs)** emit light when a forward bias is applied. Typically, LEDs are made of III-V semiconductors.

An LED emits light of a specific wavelength (e.g., red, green, yellow, blue).

White LEDs combine individual LEDs that emit the three primary colors (red, green, blue) or use a phosphor material to convert monochromatic light from a blue or UV LED to broad-spectrum white light.

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## Diode types

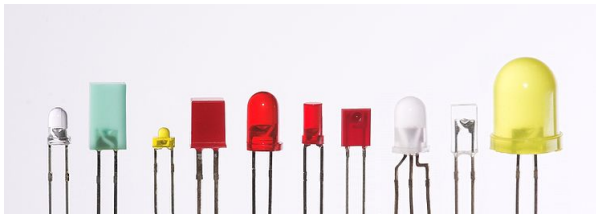
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(source: wikipedia)

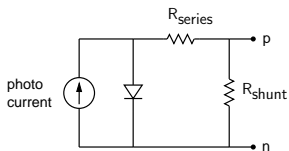
## Diode types

- \* **Solar cells** are generally silicon diodes designed to generate current efficiently when solar radiation is incident on the device. A “solar panel” has a large number of individual solar cells connected in series/parallel configuration. A solar cell can be modelled as a diode in parallel with a current source (representing the photocurrent). In addition, parasitic series and shunt resistances need to be considered.

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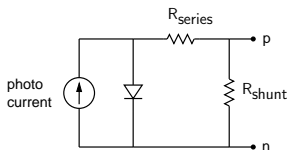
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A solar cell can be modelled as a diode in parallel with a current source (representing the photocurrent). In addition, parasitic series and shunt resistances need to be considered.



- \* **Photodiodes** are used to detect optical signals (DC or time-varying) and to convert them into electrical signals which can be subsequently processed by electronic circuits. They are used in fibre-optic communication systems, image processing, etc.

A photodiode works on the same principle as a solar cell, i.e., it converts light into a current. However, its design is optimized for high-sensitivity, low-noise, or high-frequency operation, depending on the application.

- \* In DC situations, for each diode in the circuit, we need to establish whether it is on or off, replace it with the corresponding equivalent circuit, and then obtain the quantities of interest.

# Diode circuit analysis

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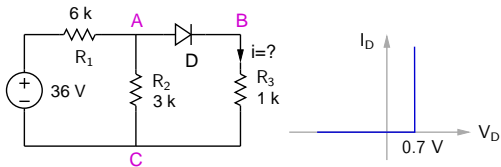
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- \* In AC (small-signal) situations, the diode can be replaced by its small-signal model, and phasor analysis is used. We will illustrate this procedure for a BJT amplifier later.

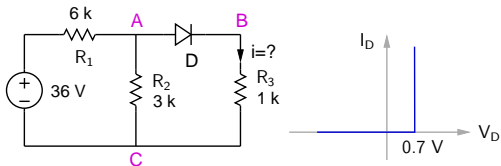
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- \* In AC (small-signal) situations, the diode can be replaced by its small-signal model, and phasor analysis is used. We will illustrate this procedure for a BJT amplifier later.
- \* Note that there are diode circuits in which the exponential nature of the diode I-V relationship is made use of. For these circuits, computer simulation would be required to solve the resulting non-linear equations.

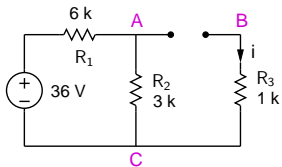
## Diode circuit example



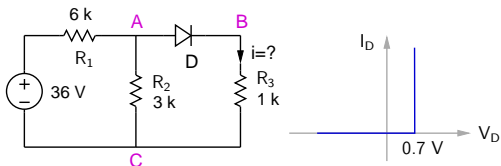
## Diode circuit example



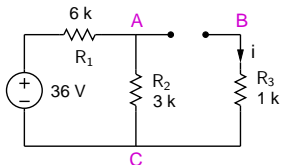
Case 1: D is off.



## Diode circuit example



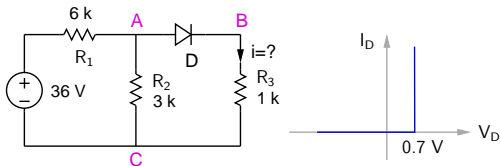
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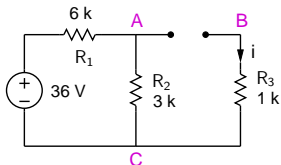
$$V_{AB} = V_{AC} = \frac{3}{9} \times 36 = 12 \text{ V},$$

which is not consistent with our assumption of D being off.

## Diode circuit example



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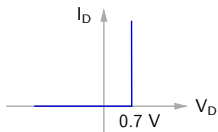
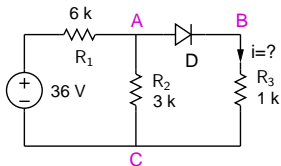


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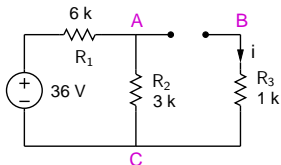
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→ D must be on.

## Diode circuit example



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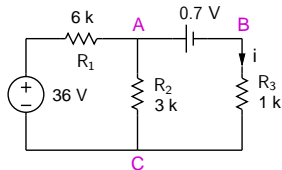


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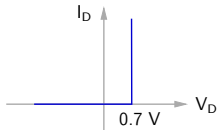
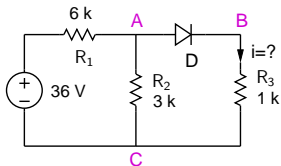
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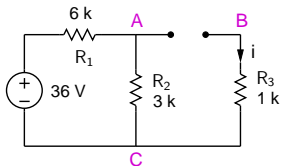
Case 2: D is on.



# Diode circuit example



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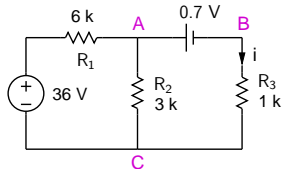


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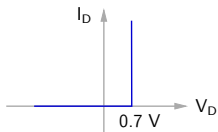
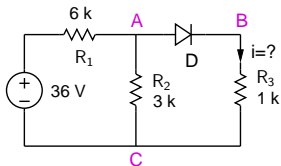
Taking  $V_C = 0 \text{ V}$ ,

$$\frac{V_A - 36}{6 \text{ k}} + \frac{V_A}{3 \text{ k}} + \frac{V_A - 0.7}{1 \text{ k}} = 0,$$

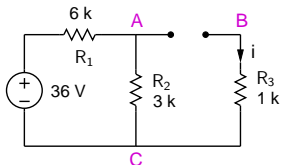
$$\rightarrow V_A = 4.47 \text{ V}, i = 3.77 \text{ mA}.$$



## Diode circuit example



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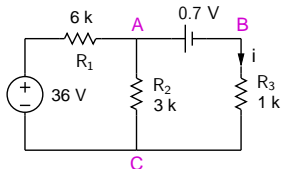


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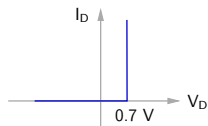
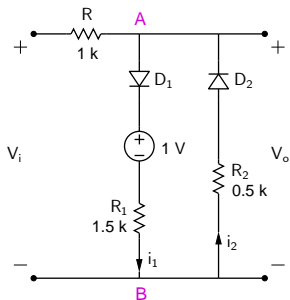
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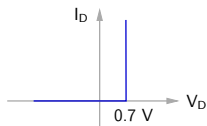
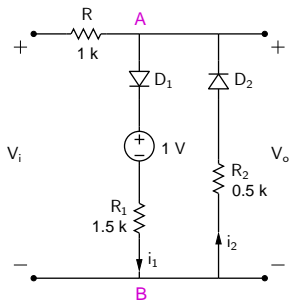
Remark: Often, we can figure out by inspection if a diode is on or off.

## Diode circuit example



- (a) Plot  $V_o$  versus  $V_i$  for  $-5\text{ V} < V_i < 5\text{ V}$ .
- (b) Plot  $V_o(t)$  for a triangular input:  
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## Diode circuit example

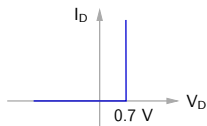
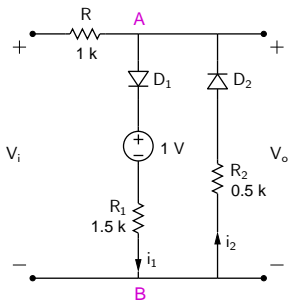


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## Diode circuit example



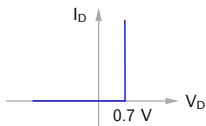
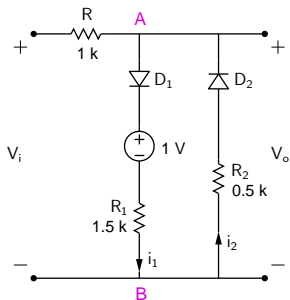
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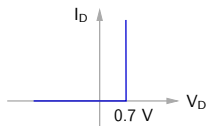
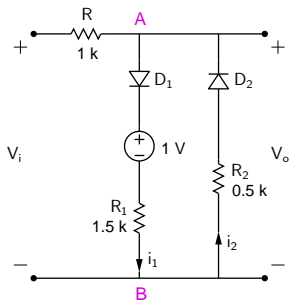
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$\Rightarrow V_{AB} > 1.7 \text{ V} \Rightarrow D_2$  cannot conduct.

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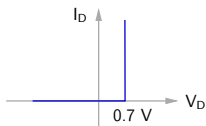
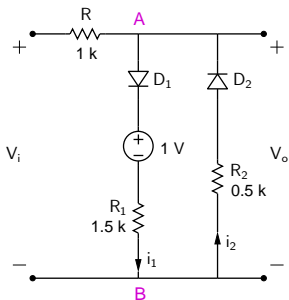
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Similarly, if  $D_2$  is on,  $V_{BA} > 0.7 \text{ V}$ , i.e.,  $V_{AB} < -0.7 \text{ V} \Rightarrow D_1$  cannot conduct.

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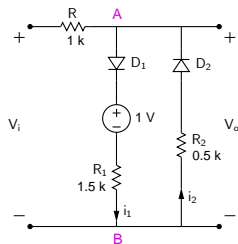
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Clearly,  $D_1 \text{ on} \Rightarrow D_2 \text{ off}$ , and  $D_2 \text{ on} \Rightarrow D_1 \text{ off}$ .

## Diode circuit example (continued)

- \* For  $-0.7 \text{ V} < V_i < 1.7 \text{ V}$ , both  $D_1$  and  $D_2$  are off.  
→ no drop across  $R$ , and  $V_o = V_i$ .

(1)





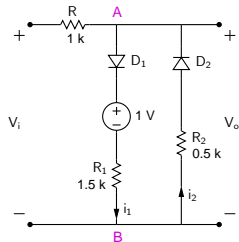
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\* For  $V_i < -0.7 \text{ V}$ ,  $D_2$  conducts. →  $V_o = -0.7 - i_2 R_2$ .  
Use KVL to get  $i_2$ :  $V_i + i_2 R_2 + 0.7 + R i_2 = 0$ .

$$\rightarrow i_2 = -\frac{V_i + 0.7}{R + R_2}, \text{ and}$$

$$V_o = -0.7 - R_2 i_2 = \frac{R_2}{R + R_2} V_i - 0.7 \frac{R}{R + R_2}. \quad (2)$$



## Diode circuit example (continued)

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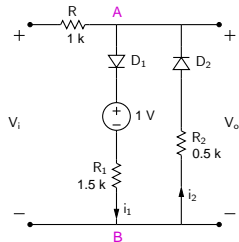
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- \* For  $V_i > 1.7 \text{ V}$ ,  $D_1$  conducts. →  $V_o = 0.7 + 1 + i_1 R_1$ .  
Use KVL to get  $i_1$ :  $-V_i + i_1 R + 0.7 + 1 + i_1 R_1 = 0$ .

$$\rightarrow i_1 = \frac{V_i - 1.7}{R + R_1}, \text{ and}$$

$$V_o = 1.7 + R_1 i_1 = \frac{R_1}{R + R_1} V_i + 1.7 \frac{R}{R + R_1}. \quad (3)$$



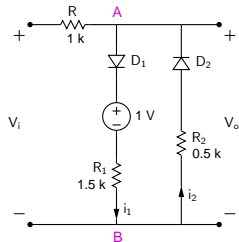
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- \* For  $-0.7 \text{ V} < V_i < 1.7 \text{ V}$ , both  $D_1$  and  $D_2$  are off.  
→ no drop across  $R$ , and  $V_o = V_i$ . (1)

- \* For  $V_i < -0.7 \text{ V}$ ,  $D_2$  conducts. →  $V_o = -0.7 - i_2 R_2$ .  
Use KVL to get  $i_2$ :  $V_i + i_2 R_2 + 0.7 + R i_2 = 0$ .  
→  $i_2 = -\frac{V_i + 0.7}{R + R_2}$ , and  
$$V_o = -0.7 - R_2 i_2 = \frac{R_2}{R + R_2} V_i - 0.7 \frac{R}{R + R_2} . \quad (2)$$

- \* For  $V_i > 1.7 \text{ V}$ ,  $D_1$  conducts. →  $V_o = 0.7 + 1 + i_1 R_1$ .  
Use KVL to get  $i_1$ :  $-V_i + i_1 R + 0.7 + 1 + i_1 R_1 = 0$ .  
→  $i_1 = \frac{V_i - 1.7}{R + R_1}$ , and  
$$V_o = 1.7 + R_1 i_1 = \frac{R_1}{R + R_1} V_i + 1.7 \frac{R}{R + R_1} . \quad (3)$$

- \* Using Eqs. (1)-(3), we plot  $V_o$  versus  $V_i$ .  
(SEQUEL file: ee101\_diode\_circuit\_1.sqproj)



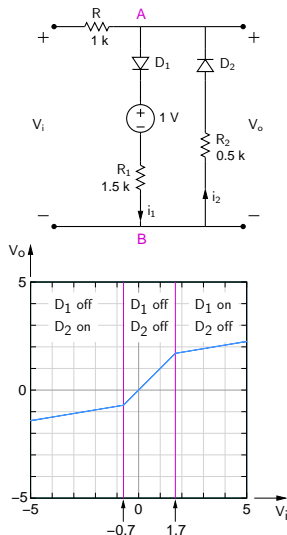
## Diode circuit example (continued)

- \* For  $-0.7 \text{ V} < V_i < 1.7 \text{ V}$ , both  $D_1$  and  $D_2$  are off.  
 $\rightarrow$  no drop across  $R$ , and  $V_o = V_i$ . (1)

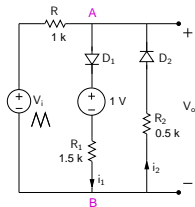
- \* For  $V_i < -0.7 \text{ V}$ ,  $D_2$  conducts.  $\rightarrow V_o = -0.7 - i_2 R_2$ .  
 Use KVL to get  $i_2$ :  $V_i + i_2 R_2 + 0.7 + R i_2 = 0$ .  
 $\rightarrow i_2 = -\frac{V_i + 0.7}{R + R_2}$ , and  
 $V_o = -0.7 - R_2 i_2 = \frac{R_2}{R + R_2} V_i - 0.7 \frac{R}{R + R_2}$ . (2)

- \* For  $V_i > 1.7 \text{ V}$ ,  $D_1$  conducts.  $\rightarrow V_o = 0.7 + 1 + i_1 R_1$ .  
 Use KVL to get  $i_1$ :  $-V_i + i_1 R + 0.7 + 1 + i_1 R_1 = 0$ .  
 $\rightarrow i_1 = \frac{V_i - 1.7}{R + R_1}$ , and  
 $V_o = 1.7 + R_1 i_1 = \frac{R_1}{R + R_1} V_i + 1.7 \frac{R}{R + R_1}$ . (3)

- \* Using Eqs. (1)-(3), we plot  $V_o$  versus  $V_i$ .  
 (SEQUEL file: ee101\_diode\_circuit\_1.sqproj)

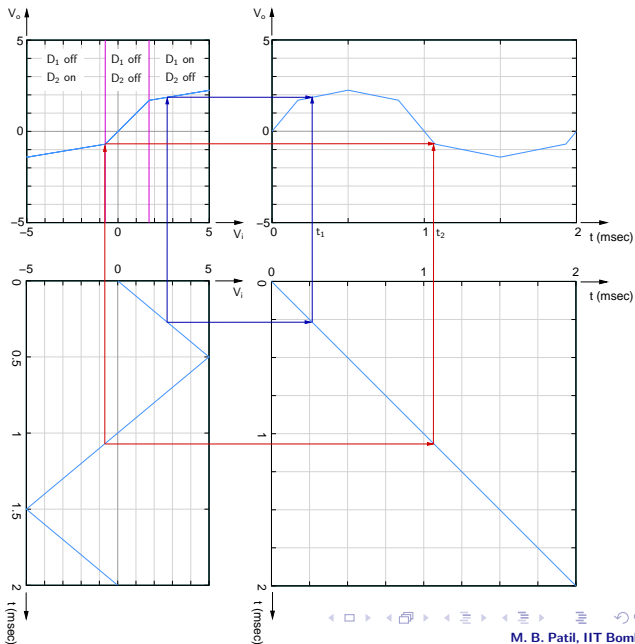


# Diode circuit example (continued)

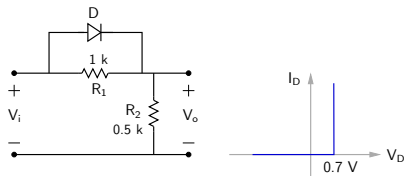


Point-by-point construction of  $V_o$  versus  $t$ :

Two time points,  $t_1$  and  $t_2$ , are shown as examples.

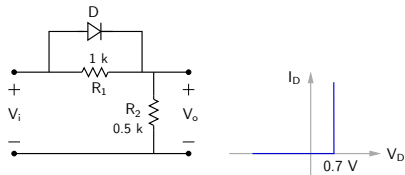


## Diode circuit example

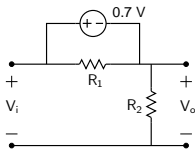


Plot  $V_o$  versus  $V_i$  for  $-5 \text{ V} < V_i < 5 \text{ V}$ .

# Diode circuit example

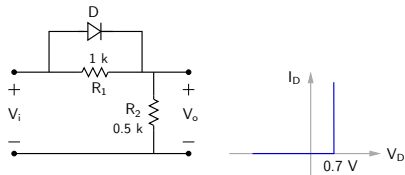


Plot  $V_o$  versus  $V_i$  for  $-5\text{ V} < V_i < 5\text{ V}$ .

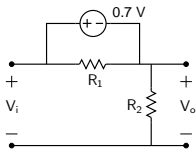


D on  
 $V_o = V_i - 0.7$

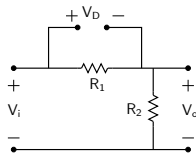
# Diode circuit example



Plot  $V_o$  versus  $V_i$  for  $-5\text{ V} < V_i < 5\text{ V}$ .



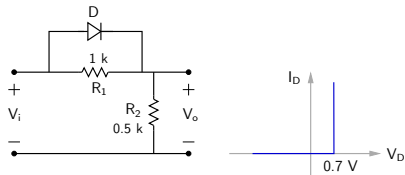
D on  
 $V_o = V_i - 0.7$



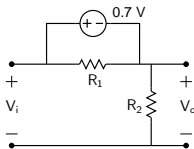
D off  
 $V_o = \frac{R_2}{R_1 + R_2} V_i$



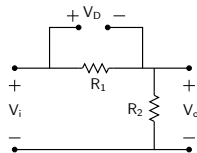
## Diode circuit example



Plot  $V_o$  versus  $V_i$  for  $-5\text{ V} < V_i < 5\text{ V}$ .



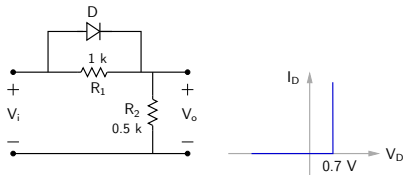
D on  
 $V_o = V_i - 0.7$



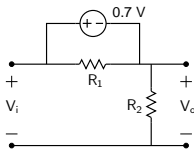
D off  
 $V_o = \frac{R_2}{R_1 + R_2} V_i$

At what value of  $V_i$  will the diode turn on?

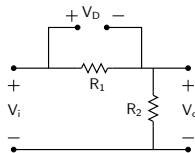
## Diode circuit example



Plot  $V_o$  versus  $V_i$  for  $-5\text{ V} < V_i < 5\text{ V}$ .



D on  
 $V_o = V_i - 0.7$

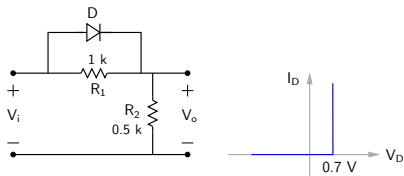


D off  
 $V_o = \frac{R_2}{R_1 + R_2} V_i$

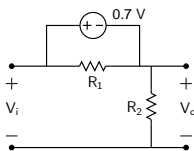
At what value of  $V_i$  will the diode turn on?

In the off state,  $V_D = \frac{R_1}{R_1 + R_2} V_i$ .

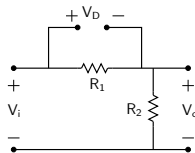
## Diode circuit example



Plot  $V_o$  versus  $V_i$  for  $-5\text{ V} < V_i < 5\text{ V}$ .



D on  
 $V_o = V_i - 0.7$



D off  
 $V_o = \frac{R_2}{R_1 + R_2} V_i$

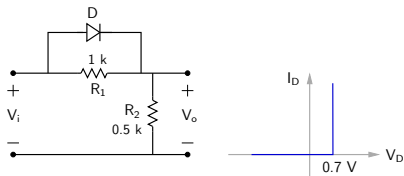
At what value of  $V_i$  will the diode turn on?

In the off state,  $V_D = \frac{R_1}{R_1 + R_2} V_i$ .

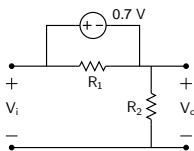
For  $D$  to change to the on state,  $V_D = 0.7\text{ V}$ .

i.e.,  $V_i = \frac{R_1 + R_2}{R_1} \times 0.7 = 1.05\text{ V}$ .

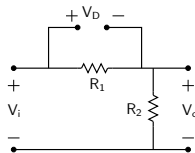
## Diode circuit example



Plot  $V_o$  versus  $V_i$  for  $-5\text{ V} < V_i < 5\text{ V}$ .



D on  
 $V_o = V_i - 0.7$



D off  
 $V_o = \frac{R_2}{R_1 + R_2} V_i$

At what value of  $V_i$  will the diode turn on?

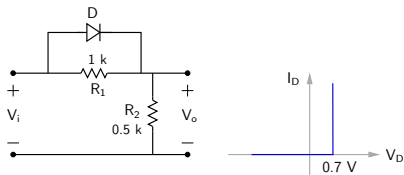
In the off state,  $V_D = \frac{R_1}{R_1 + R_2} V_i$ .

For  $D$  to change to the on state,  $V_D = 0.7\text{ V}$ .

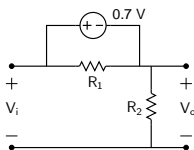
i.e.,  $V_i = \frac{R_1 + R_2}{R_1} \times 0.7 = 1.05\text{ V}$ .

(SEQUEL file: ee101\_diode\_circuit\_2.sqproj)

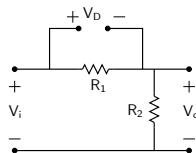
# Diode circuit example



Plot  $V_o$  versus  $V_i$  for  $-5\text{ V} < V_i < 5\text{ V}$ .



D on  
 $V_o = V_i - 0.7$



D off  
 $V_o = \frac{R_2}{R_1 + R_2} V_i$

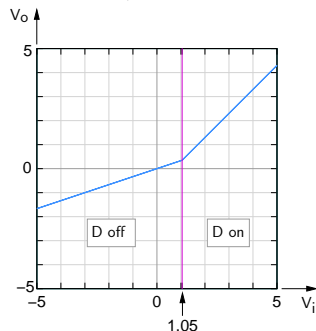
At what value of  $V_i$  will the diode turn on?

In the off state,  $V_D = \frac{R_1}{R_1 + R_2} V_i$ .

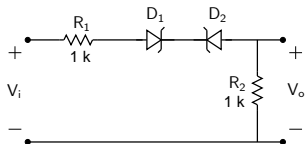
For  $D$  to change to the on state,  $V_D = 0.7\text{ V}$ .

i.e.,  $V_i = \frac{R_1 + R_2}{R_1} \times 0.7 = 1.05\text{ V}$ .

(SEQUEL file: ee101\_diode\_circuit\_2.sqproj)



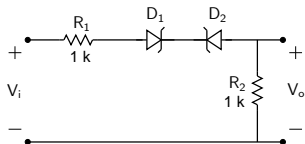
## Diode circuit example



$$V_{on} = 0.7\text{ V}, V_Z = 5\text{ V}.$$

Plot  $V_o$  versus  $V_i$ .

## Diode circuit example



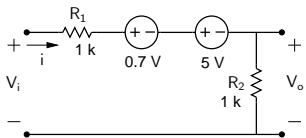
$$V_{on} = 0.7 \text{ V}, V_Z = 5 \text{ V}.$$

Plot  $V_o$  versus  $V_i$ .

---

For a current to flow, we have two possibilities:

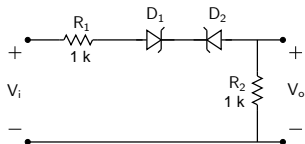
$D_1$  on (forward),  $D_2$  in reverse breakdown



$$V_o = iR_2 = \frac{V_i - 5.7}{R_1 + R_2} R_2$$

Since  $i > 0$ , this can happen only when  $V_i > 5.7 \text{ V}$ .

## Diode circuit example

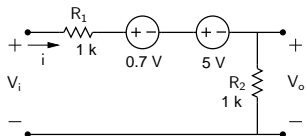


$$V_{on} = 0.7 \text{ V}, V_Z = 5 \text{ V}.$$

Plot  $V_o$  versus  $V_i$ .

For a current to flow, we have two possibilities:

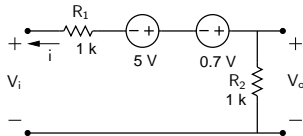
$D_1$  on (forward),  $D_2$  in reverse breakdown



$$V_o = iR_2 = \frac{V_i - 5.7}{R_1 + R_2} R_2$$

Since  $i > 0$ , this can happen only when  $V_i > 5.7 \text{ V}$ .

$D_2$  on (forward),  $D_1$  in reverse breakdown

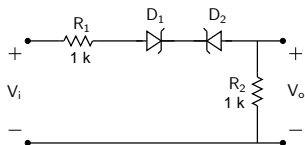


$$V_o = -iR_2 = \frac{V_i + 5.7}{R_1 + R_2} R_2$$

Since  $i > 0$ , this can happen only when  $V_i < -5.7 \text{ V}$ .

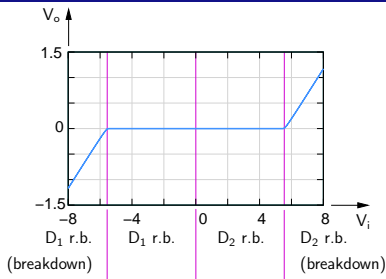


## Diode circuit example



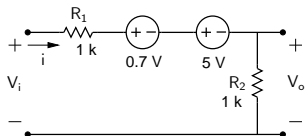
$$V_{on} = 0.7 \text{ V}, V_Z = 5 \text{ V}.$$

Plot  $V_o$  versus  $V_i$ .



For a current to flow, we have two possibilities:

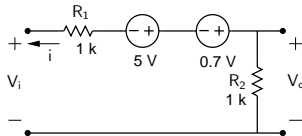
$D_1$  on (forward),  $D_2$  in reverse breakdown



$$V_o = iR_2 = \frac{V_i - 5.7}{R_1 + R_2} R_2$$

Since  $i > 0$ , this can happen only when  $V_i > 5.7 \text{ V}$ .

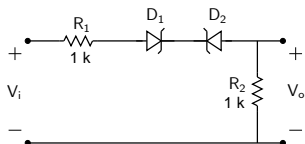
$D_2$  on (forward),  $D_1$  in reverse breakdown



$$V_o = -iR_2 = \frac{V_i + 5.7}{R_1 + R_2} R_2$$

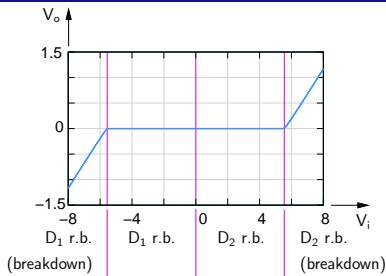
Since  $i > 0$ , this can happen only when  $V_i < -5.7 \text{ V}$ .

## Diode circuit example



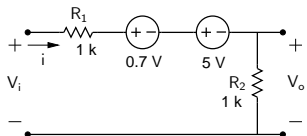
$$V_{on} = 0.7 \text{ V}, V_Z = 5 \text{ V}.$$

Plot  $V_o$  versus  $V_i$ .



For a current to flow, we have two possibilities:

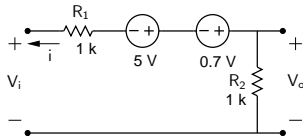
$D_1$  on (forward),  $D_2$  in reverse breakdown



$$V_o = iR_2 = \frac{V_i - 5.7}{R_1 + R_2} R_2$$

Since  $i > 0$ , this can happen only when  $V_i > 5.7 \text{ V}$ .

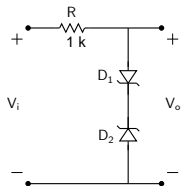
$D_2$  on (forward),  $D_1$  in reverse breakdown



$$V_o = -iR_2 = \frac{V_i + 5.7}{R_1 + R_2} R_2$$

Since  $i > 0$ , this can happen only when  $V_i < -5.7 \text{ V}$ .

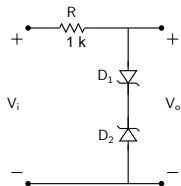
## Diode circuit example (voltage limiter)



$V_{\text{on}} = 0.7\text{ V}$ ,  $V_Z = 5\text{ V}$ .

Plot  $V_o$  versus  $V_i$ .

## Diode circuit example (voltage limiter)

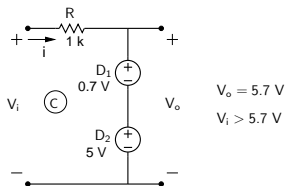


$$V_{\text{on}} = 0.7\text{ V}, V_Z = 5\text{ V}.$$

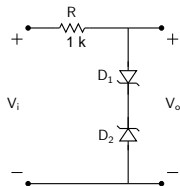
Plot  $V_o$  versus  $V_i$ .

For a current to flow, we have two possibilities:

$D_1$  on (forward),  $D_2$  in reverse breakdown



## Diode circuit example (voltage limiter)

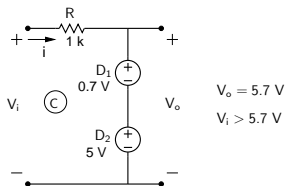


$$V_{on} = 0.7 \text{ V}, V_Z = 5 \text{ V}.$$

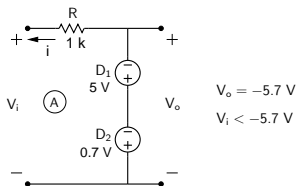
Plot  $V_o$  versus  $V_i$ .

For a current to flow, we have two possibilities:

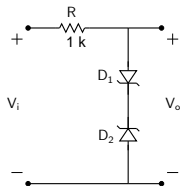
$D_1$  on (forward),  $D_2$  in reverse breakdown



$D_2$  on (forward),  $D_1$  in reverse breakdown



# Diode circuit example (voltage limiter)

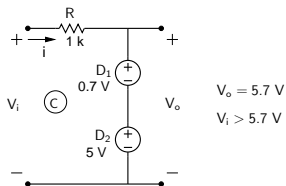


$$V_{on} = 0.7 \text{ V}, V_Z = 5 \text{ V}.$$

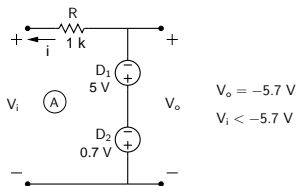
Plot  $V_o$  versus  $V_i$ .

For a current to flow, we have two possibilities:

$D_1$  on (forward),  $D_2$  in reverse breakdown

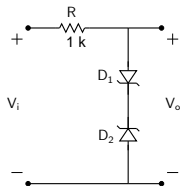


$D_2$  on (forward),  $D_1$  in reverse breakdown



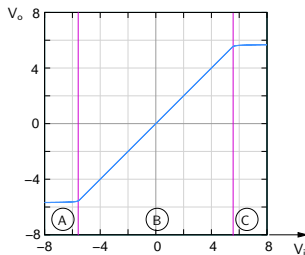
In the range,  $-5.7 \text{ V} < V_i < 5.7 \text{ V}$ , no current flows, and  $V_o = V_i$ . (B)

# Diode circuit example (voltage limiter)



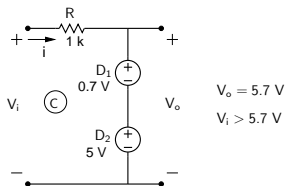
$$V_{on} = 0.7 \text{ V}, V_Z = 5 \text{ V}.$$

Plot  $V_o$  versus  $V_i$ .

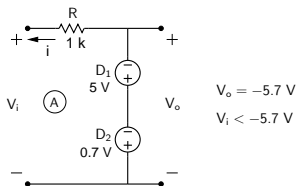


For a current to flow, we have two possibilities:

$D_1$  on (forward),  $D_2$  in reverse breakdown

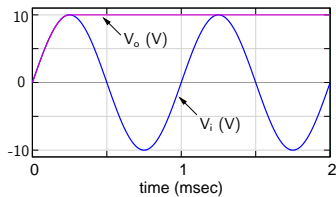
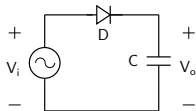


$D_2$  on (forward),  $D_1$  in reverse breakdown



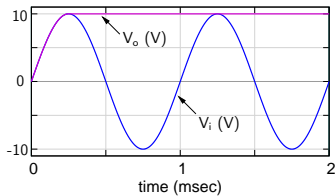
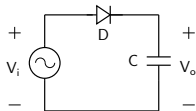
In the range,  $-5.7 \text{ V} < V_i < 5.7 \text{ V}$ , no current flows, and  $V_o = V_i$ . (B)

# Peak detector



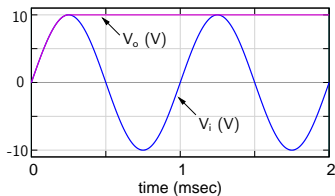
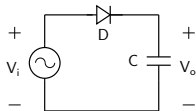


# Peak detector



Let  $V_o(t) = 0$  V at  $t = 0$ , and assume the diode to be ideal, with  $V_{on} = 0$  V.

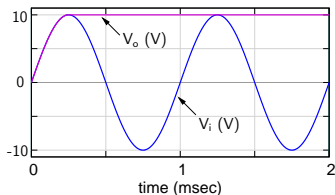
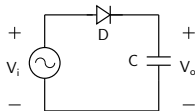
## Peak detector



Let  $V_o(t) = 0$  V at  $t = 0$ , and assume the diode to be ideal, with  $V_{on} = 0$  V.

For  $0 < t < T/4$ ,  $V_i$  rises from 0 to  $V_m$ . As a result, the capacitor charges.

## Peak detector

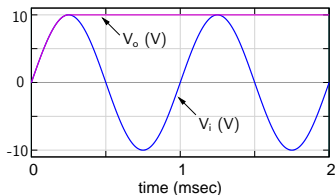
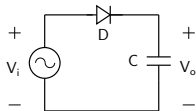


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Since the on resistance of the diode is small, time constant  $\tau \ll T/4$ ; therefore the charging process is instantaneous  $\Rightarrow V_o(t) = V_i(t)$ .

## Peak detector



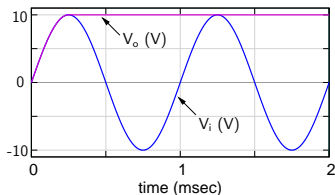
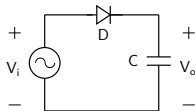
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For  $t > T/4$ ,  $V_i$  starts falling. The capacitor holds the charge it had at  $t = T/4$  since the diode prevents discharging.

## Peak detector



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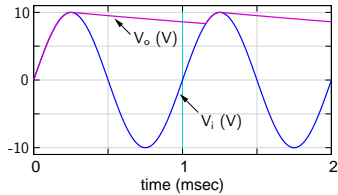
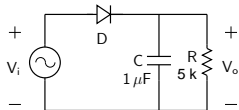
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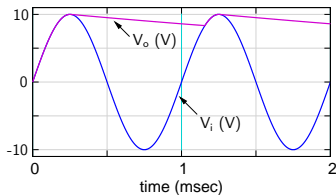
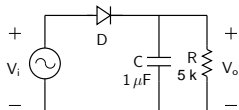
For  $t > T/4$ ,  $V_i$  starts falling. The capacitor holds the charge it had at  $t = T/4$  since the diode prevents discharging.

SEQUEL file: ee101.diode\_circuit\_5.sqproj

## Peak detector (continued)

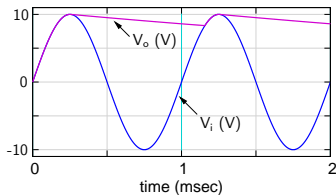
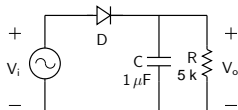


## Peak detector (continued)



If a resistor is added in parallel, a discharging path is provided for the capacitor, and the capacitor voltage falls after reaching the peak.

## Peak detector (continued)

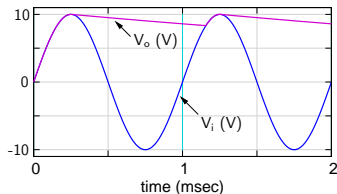
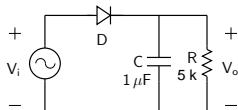


If a resistor is added in parallel, a discharging path is provided for the capacitor, and the capacitor voltage falls after reaching the peak.

When  $V_i > V_o$ , the capacitor charges again. The time constant for the charging process is  $\tau = R_{Th}C$ , where  $R_{Th} = R \parallel R_{on}$  is the Thevenin resistance seen by the capacitor,  $R_{on}$  being the on resistance of the diode.



## Peak detector (continued)

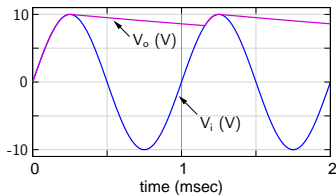
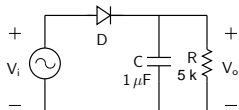


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Since  $\tau \ll T$ , the charging process is instantaneous.

## Peak detector (continued)



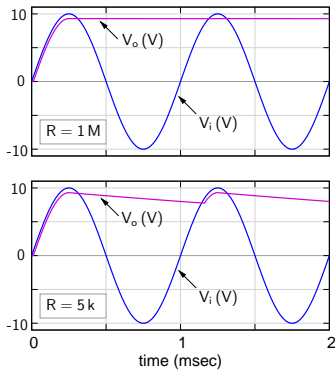
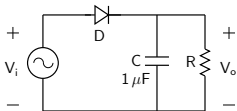
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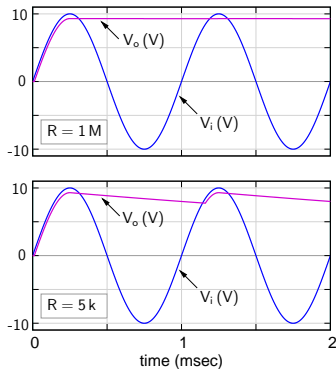
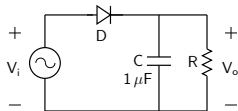
Since  $\tau \ll T$ , the charging process is instantaneous.

SEQUEL file: ee101\_diode\_circuit\_5a.sqproj

## Peak detector (with $V_{on} = 0.7\text{ V}$ )

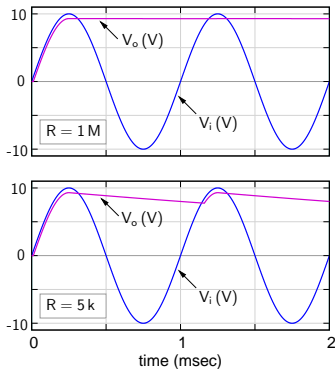
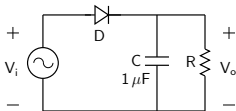


## Peak detector (with $V_{on} = 0.7 \text{ V}$ )



With  $V_{on} = 0.7 \text{ V}$ , the capacitor charges up to  $(V_m - 0.7 \text{ V})$ .

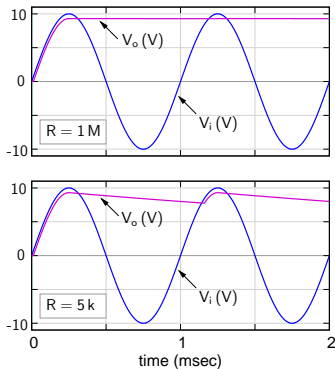
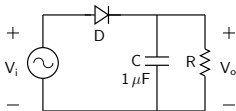
## Peak detector (with $V_{on} = 0.7\text{ V}$ )



With  $V_{on} = 0.7\text{ V}$ , the capacitor charges up to  $(V_m - 0.7\text{ V})$ .

Apart from that, the circuit operation is similar.

## Peak detector (with $V_{on} = 0.7 \text{ V}$ )

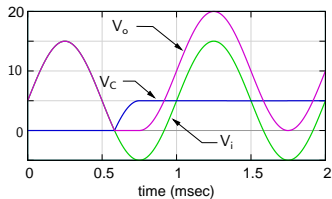
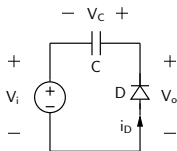


With  $V_{on} = 0.7 \text{ V}$ , the capacitor charges up to  $(V_m - 0.7 \text{ V})$ .

Apart from that, the circuit operation is similar.

SEQUEL file: ee101\_diode\_circuit\_5a.sqproj

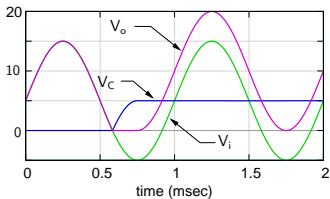
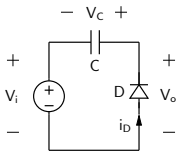
# Clamped capacitor



\* Assume  $V_{on} = 0$  V for the diode.

When  $D$  conducts,  $V_D = -V_o = 0 \Rightarrow V_C + V_i = 0$ , i.e.,  $V_C = -V_i$ .

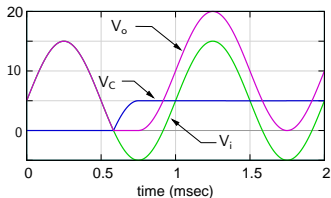
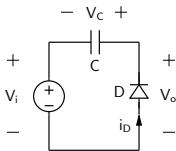
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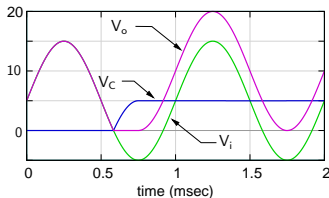
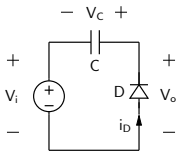


# Clamped capacitor



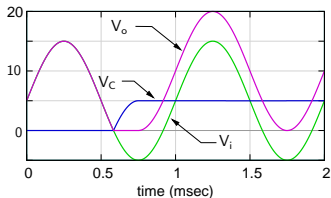
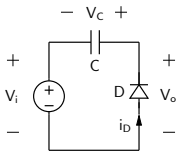
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- \* The net result is that the capacitor gets charged to a voltage  $V_C = -V_i$ , corresponding to the maximum negative value of  $V_i$ , and holds that voltage thereafter. Let us call this voltage  $V_C^0$  (a constant).

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- \*  $V_o(t) = V_C(t) + V_i(t) = V_C^0 + V_i(t)$ , which is a “level-shifted” version of  $V_i$ .

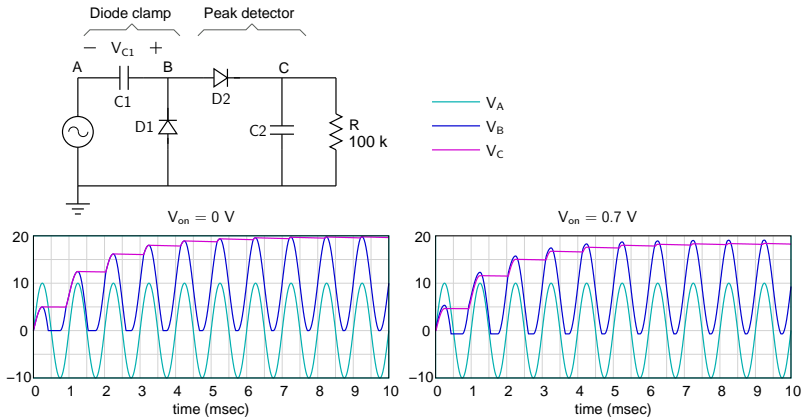
# Clamped capacitor



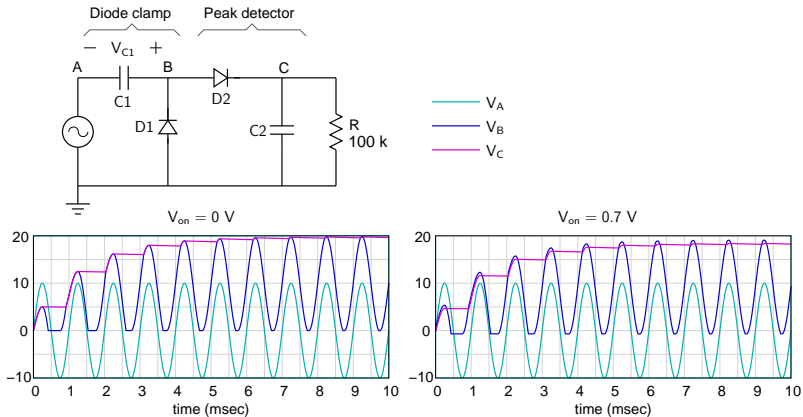
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(SEQUEL file: ee101\_diode\_circuit.6.sqproj)

# Voltage doubler

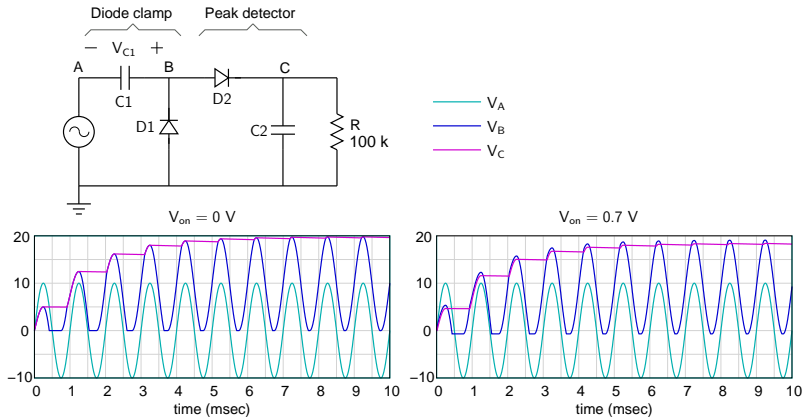


# Voltage doubler



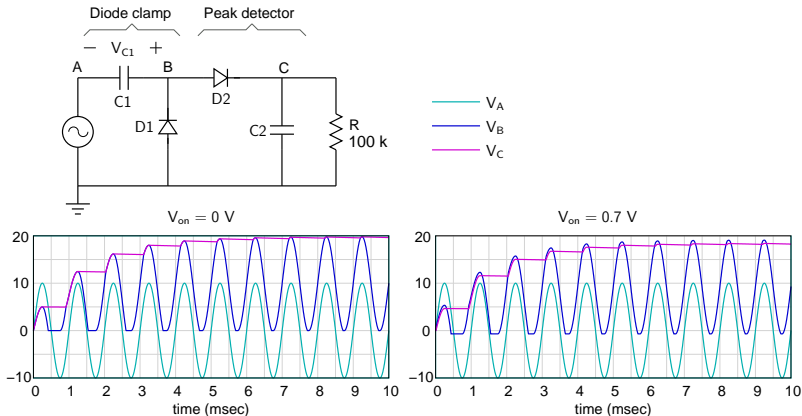
- \* The diode clamp shifts  $V_A$  up by  $V_m$  (the amplitude of the AC source), making  $V_B$  go from 0 to  $2V_m$ .

# Voltage doubler



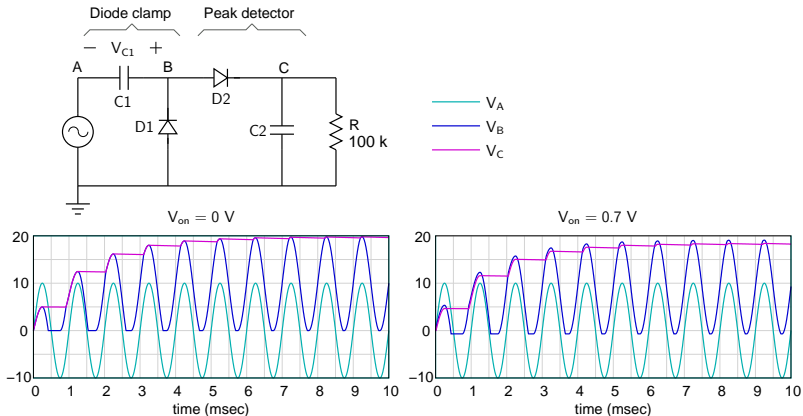
- \* The diode clamp shifts  $V_A$  up by  $V_m$  (the amplitude of the AC source), making  $V_B$  go from 0 to  $2V_m$ .
- \* The peak detector detects the peak of  $V_B$  ( $2V_m$  w.r.t. ground), and holds it constant.

# Voltage doubler



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- \* Note that it takes a few cycles to reach steady state. Plot  $V_{C1}$ ,  $i_{D1}$ ,  $i_{D2}$  versus  $t$  and explain the initial behaviour of the circuit.

# Voltage doubler



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(SEQUEL file: ee101.voltage-doubler.sqproj)