

Some new links between graph theory and optimal charging/discharging control strategies

Madhu N. Belur
EE, IIT Bombay

<http://www.ee.iitb.ac.in/~belur/talks/>

21st April, 2015

- Optimal charging/discharging of RLC circuits
- Actual energy stored in state v_0 is **geometric** mean of
 - ‘minimum required’ energy for charging state v_0 , and
 - ‘maximum extractable’ energy while discharging from v_0 .
- Generalization to the **multi-state** case of the ‘geometric’ mean
- Positive real balancing in Model Order Reduction

- 1 Generalize the intuitive notion: a port needed for controlling a circuit
- 2 Formulate port/capacitor/inductor relative locations which cause common eigenspaces in
 - state transition matrix A (of any state space realization)
 - required supply energy matrix K_{reqd}
 - available storage energy matrix K_{avail}
- 3 Generalize the geometric mean property to the matrix (multistate) case

- For an undirected graph $G(V, E)$: with $|V| = n$ nodes, the Laplacian $L \in \mathbb{R}^{n \times n}$

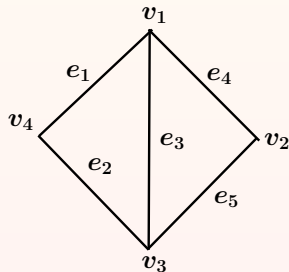
$$L := D - N$$

D is the diagonal ‘degree’ matrix

(degree of a node: number of edges incident on that node)

N is the **neighbourhood (adjacency)** matrix:

$N_{ij} := 1$, if nodes v_i and v_j are neighbours, 0 otherwise.



$$L = \begin{bmatrix} 3 & -1 & -1 & -1 \\ -1 & 2 & -1 & 0 \\ -1 & -1 & 3 & -1 \\ -1 & 0 & -1 & 2 \end{bmatrix}$$

L is symmetric and positive semi-definite matrix: at least one eigenvalue at 0

- For an undirected graph $G(V, E)$: with $|V| = n$ nodes, the Laplacian $L \in \mathbb{R}^{n \times n}$

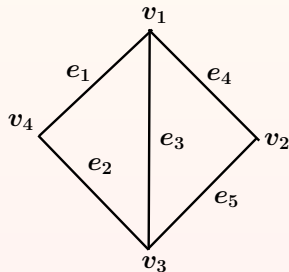
$$L := D - N$$

D is the diagonal ‘degree’ matrix

(degree of a node: number of edges incident on that node)

N is the **neighbourhood (adjacency)** matrix:

$N_{ij} := 1$, if nodes v_i and v_j are neighbours, 0 otherwise.



$$L = \begin{bmatrix} 3 & -1 & -1 & -1 \\ -1 & 2 & -1 & 0 \\ -1 & -1 & 3 & -1 \\ -1 & 0 & -1 & 2 \end{bmatrix}$$

L is symmetric and positive semi-definite matrix: at least one eigenvalue at 0

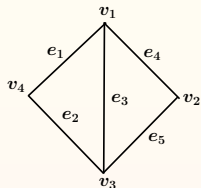
For graph $G(V, E)$, associate unit resistor to each edge in E

For graph $G(V, E)$, associate unit resistor to each edge in E

Introduce a ground node 0, connect unit capacitor between node i in V to node 0

For graph $G(V, E)$, associate unit resistor to each edge in E

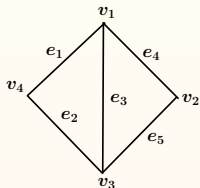
Introduce a ground node 0, connect unit capacitor between node i in V to node 0



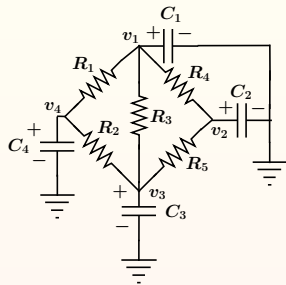
$$L = \begin{bmatrix} 3 & -1 & -1 & -1 \\ -1 & 2 & -1 & 0 \\ -1 & -1 & 3 & -1 \\ -1 & 0 & -1 & 2 \end{bmatrix}$$

For graph $G(V, E)$, associate unit resistor to each edge in E

Introduce a ground node 0, connect unit capacitor between node i in V to node 0

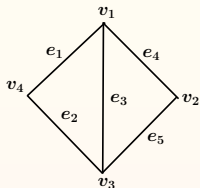


$$L = \begin{bmatrix} 3 & -1 & -1 & -1 \\ -1 & 2 & -1 & 0 \\ -1 & -1 & 3 & -1 \\ -1 & 0 & -1 & 2 \end{bmatrix}$$

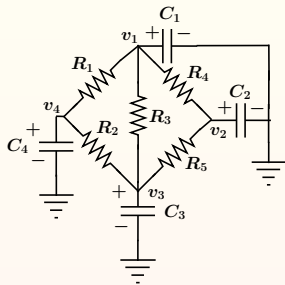


For graph $G(V, E)$, associate unit resistor to each edge in E

Introduce a ground node 0, connect unit capacitor between node i in V to node 0



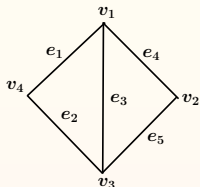
$$L = \begin{bmatrix} 3 & -1 & -1 & -1 \\ -1 & 2 & -1 & 0 \\ -1 & -1 & 3 & -1 \\ -1 & 0 & -1 & 2 \end{bmatrix}$$



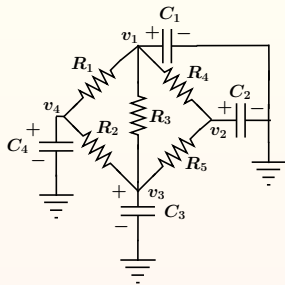
$$\frac{d}{dt} \begin{bmatrix} v_1 \\ v_2 \\ v_3 \\ v_4 \end{bmatrix} = -L \begin{bmatrix} v_1 \\ v_2 \\ v_3 \\ v_4 \end{bmatrix}$$

For graph $G(V, E)$, associate unit resistor to each edge in E

Introduce a ground node 0, connect unit capacitor between node i in V to node 0



$$L = \begin{bmatrix} 3 & -1 & -1 & -1 \\ -1 & 2 & -1 & 0 \\ -1 & -1 & 3 & -1 \\ -1 & 0 & -1 & 2 \end{bmatrix}$$

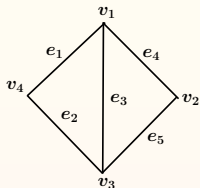


$$\frac{d}{dt} \begin{bmatrix} v_1 \\ v_2 \\ v_3 \\ v_4 \end{bmatrix} = -L \begin{bmatrix} v_1 \\ v_2 \\ v_3 \\ v_4 \end{bmatrix}$$

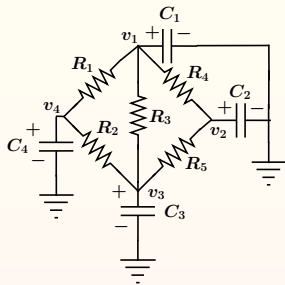
- Second **smallest** eigenvalue of L (for a connected graph): algebraic connectivity decides ‘mixing time’: time-constant for equalizing voltage across capacitors.
- Edge **conductances** \leftrightarrow edge weights \leftrightarrow off-diagonal terms in L
- Capacitances different? Need ‘balancing’: this talk

For graph $G(V, E)$, associate unit resistor to each edge in E

Introduce a ground node 0, connect unit capacitor between node i in V to node 0



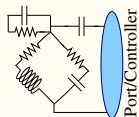
$$L = \begin{bmatrix} 3 & -1 & -1 & -1 \\ -1 & 2 & -1 & 0 \\ -1 & -1 & 3 & -1 \\ -1 & 0 & -1 & 2 \end{bmatrix}$$



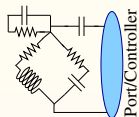
$$\frac{d}{dt} \begin{bmatrix} v_1 \\ v_2 \\ v_3 \\ v_4 \end{bmatrix} = -L \begin{bmatrix} v_1 \\ v_2 \\ v_3 \\ v_4 \end{bmatrix}$$

- Second **smallest** eigenvalue of L (for a connected graph): algebraic connectivity decides ‘mixing time’: time-constant for equalizing voltage across capacitors.
- Edge **conductances** \leftrightarrow edge weights \leftrightarrow off-diagonal terms in L
- Capacitances different? Need ‘balancing’: this talk
- With ports:
 - ★ **optimal** charging/discharging
 - ★ port location for controllability: general LTI systems

Hinged graphs: decoupled: uncontrollable?

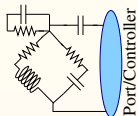


Hinged graphs: decoupled: uncontrollable?



- ★ Electrical networks: much structure
- ★ General (sparse) LTI systems have **less** graph structure
- ★ **Bipartite** graphs: edges between equation set and variable set

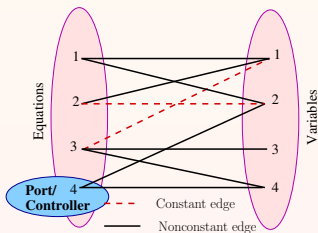
Hinged graphs: decoupled: uncontrollable?



- ★ Electrical networks: much structure
- ★ General (sparse) LTI systems have **less** graph structure
- ★ **Bipartite** graphs: edges between equation set and variable set

- Two types of equations (left nodes):
 - plant equations (left-top nodes): given to us
 - controller equations (left-bottom nodes): what **we** connect at the port: to-be-designed
 - ★ feedback controller: **additional** laws

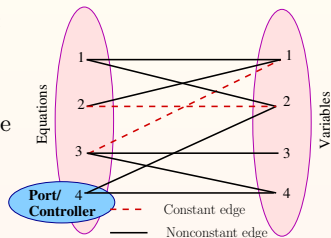
- Plant structure: equation-variable interaction
- Controller structure: sensor/actuator interaction constraint



- **Controlled** system: **square** polynomial matrix: plant and controller/port equations
- # equations = # variables: (determined system of equations)
- One-to-one correspondence \equiv 'marriage' \equiv matching
- All nodes get matched \equiv **perfect** matching
- Terms in determinant \leftrightarrow perfect matchings

Pole-placement, structural controllability

- Given equation-variable graph structure of the **plant** and **controller**:
find conditions on controller structure for arbitrary pole-placement
- Those edges that occur in **some** perfect matching:
'admissible'.
- Discard the rest
- Resulting graph if connected: **elementary** bipartite graph: well-studied (Lovasz & Plummer)
- Classify edges into **plant/controller** edges
(plant edges: constant and non-constant)



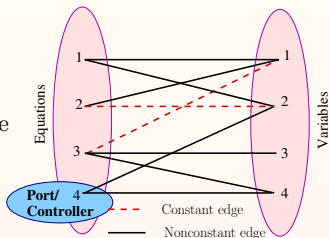
Theorem

Given plant and controller structure, following are equivalent

- arbitrary pole-placement possible
- every admissible plant edge occurs in some loop containing controller edges

Pole-placement, structural controllability

- Given equation-variable graph structure of the **plant** and **controller**:
find conditions on controller structure for arbitrary pole-placement
- Those edges that occur in **some** perfect matching:
'admissible'.
- Discard the rest
- Resulting graph if connected: **elementary** bipartite graph: well-studied (Lovasz & Plummer)
- Classify edges into **plant/controller** edges
(plant edges: constant and non-constant)



Theorem

Given plant and controller structure, following are equivalent

- arbitrary pole-placement possible
- every admissible plant edge occurs in some loop containing controller edges

(with R. Kalaimani and S. Krishnan (Math): Linear Algebra & its Applications: 2013)

Techniques from matching theory aspects of graph theory

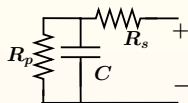
Consider the RC circuit

Initially (at $t = -\infty$) discharged: $v_C(-\infty) = 0$

Finally (at $t = +\infty$) discharged: $v_C(+\infty) = 0$

Actual energy at $t = 0$: $\frac{1}{2}Cv_0^2$ with $v_C(0) = v_0$ V

Energy supplied/extracted from the **port**



Consider the RC circuit

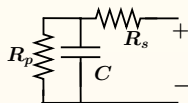
Initially (at $t = -\infty$) discharged: $v_C(-\infty) = 0$

Finally (at $t = +\infty$) discharged: $v_C(+\infty) = 0$

Actual energy at $t = 0$: $\frac{1}{2}Cv_0^2$ with $v_C(0) = v_0$ V

Energy supplied/extracted from the **port**

- Charge optimally (from $v_C(-\infty) = 0$)
minimize net energy **supplied** at the port: ‘**required** supply’



Consider the RC circuit

Initially (at $t = -\infty$) discharged: $v_C(-\infty) = 0$

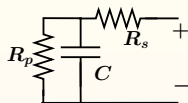
Finally (at $t = +\infty$) discharged: $v_C(+\infty) = 0$

Actual energy at $t = 0$: $\frac{1}{2}Cv_0^2$ with $v_C(0) = v_0$ V

Energy supplied/extracted from the **port**

- Charge optimally (from $v_C(-\infty) = 0$)
minimize net energy **supplied** at the port: ‘**required** supply’

Charging: * too **quick** (over **short** time interval) \equiv much $i^2 R_s$ losses in R_s



Consider the RC circuit

Initially (at $t = -\infty$) discharged: $v_C(-\infty) = 0$

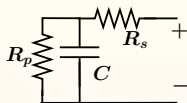
Finally (at $t = +\infty$) discharged: $v_C(+\infty) = 0$

Actual energy at $t = 0$: $\frac{1}{2}Cv_0^2$ with $v_C(0) = v_0$ V

Energy supplied/extracted from the **port**

- Charge optimally (from $v_C(-\infty) = 0$)
minimize net energy **supplied** at the port: ‘**required** supply’

Charging:
★ too **quick** (over **short** time interval) \equiv much $i^2 R_s$ losses in R_s
★ too **slow** (over **wide** time interval) \equiv C discharges through R_p



Optimal charging and discharging

Consider the RC circuit

Initially (at $t = -\infty$) discharged: $v_C(-\infty) = 0$

Finally (at $t = +\infty$) discharged: $v_C(+\infty) = 0$

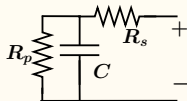
Actual energy at $t = 0$: $\frac{1}{2}Cv_0^2$ with $v_C(0) = v_0$ V

Energy supplied/extracted from the **port**

- Charge optimally (from $v_C(-\infty) = 0$)
minimize net energy **supplied** at the port: ‘**required** supply’

Charging:
★ too **quick** (over **short** time interval) \equiv much $i^2 R_s$ losses in R_s
★ too **slow** (over **wide** time interval) \equiv C discharges through R_p

- **Discharge** optimally (to $v_C(+\infty) = 0$): ‘**available** storage’
maximum net energy to be **extracted** from the port



Consider the RC circuit

Initially (at $t = -\infty$) discharged: $v_C(-\infty) = 0$

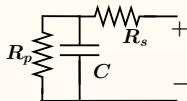
Finally (at $t = +\infty$) discharged: $v_C(+\infty) = 0$

Actual energy at $t = 0$: $\frac{1}{2}Cv_0^2$ with $v_C(0) = v_0$ V

Energy supplied/extracted from the **port**

- Charge optimally (from $v_C(-\infty) = 0$)
minimize net energy **supplied** at the port: ‘**required** supply’

Charging: * too **quick** (over **short** time interval) \equiv much i^2R_s losses in R_s
* too **slow** (over **wide** time interval) \equiv C discharges through R_p
- **Discharge** optimally (to $v_C(+\infty) = 0$): ‘**available** storage’
maximum net energy to be **extracted** from the port
- * Optimize between too much i^2R_s losses and simultaneous discharge through R_p



Optimal charging and discharging

Consider the RC circuit

Initially (at $t = -\infty$) discharged: $v_C(-\infty) = 0$

Finally (at $t = +\infty$) discharged: $v_C(+\infty) = 0$

Actual energy at $t = 0$: $\frac{1}{2}Cv_0^2$ with $v_C(0) = v_0$ V

Energy supplied/extracted from the **port**

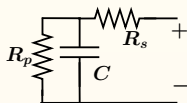
- Charge optimally (from $v_C(-\infty) = 0$)
minimize net energy **supplied** at the port: ‘**required** supply’

Charging:
★ too **quick** (over **short** time interval) \equiv much i^2R_s losses in R_s
★ too **slow** (over **wide** time interval) \equiv C discharges through R_p

- **Discharge** optimally (to $v_C(+\infty) = 0$): ‘**available** storage’
maximum net energy to be **extracted** from the port
- ★ Optimize between too much i^2R_s losses and simultaneous discharge through R_p

In general, suppose $v_C(0) = v_0$: available and required energies: **quadratic** in v_0

$$\frac{1}{2}K_{\text{avail}} v_0^2 \leq \frac{1}{2}Cv_0^2 \leq \frac{1}{2}K_{\text{reqd}} v_0^2$$



- $\frac{1}{2}Cv_0^2$ is **geometric** mean of $\frac{1}{2}K_{\text{reqd}}v_0^2$ and $\frac{1}{2}K_{\text{avail}}v_0^2$
- Why **geometric**? Why not arithmetic/harmonic means?

Optimal charging/discharging: single state

- $\frac{1}{2}Cv_0^2$ is **geometric** mean of $\frac{1}{2}K_{\text{reqd}}v_0^2$ and $\frac{1}{2}K_{\text{avail}}v_0^2$
- Why **geometric**? Why not arithmetic/harmonic means?

$$\text{(while charging)} \quad \frac{C}{K_{\text{reqd}}} = \frac{K_{\text{avail}}}{C} \quad \text{(while discharging)}$$

- $\frac{1}{2}Cv_0^2$ is **geometric** mean of $\frac{1}{2}K_{\text{reqd}}v_0^2$ and $\frac{1}{2}K_{\text{avail}}v_0^2$
- Why **geometric**? Why not arithmetic/harmonic means?

$$\text{(while charging)} \quad \frac{C}{K_{\text{reqd}}} = \frac{K_{\text{avail}}}{C} \quad \text{(while discharging)}$$

- Perhaps not too surprising: at optimal (charging/discharging) rates same **fraction** of energy is best **transferred across** resistors.

For n number of ‘memory elements’ (L and C),

- ★ let $x \in \mathbb{R}^n$: the state: vector of capacitor voltages and inductor currents

- $\frac{1}{2}Cv_0^2$ is **geometric** mean of $\frac{1}{2}K_{\text{reqd}}v_0^2$ and $\frac{1}{2}K_{\text{avail}}v_0^2$
- Why **geometric**? Why not arithmetic/harmonic means?

$$\text{(while charging)} \quad \frac{C}{K_{\text{reqd}}} = \frac{K_{\text{avail}}}{C} \quad \text{(while discharging)}$$

- Perhaps not too surprising: at optimal (charging/discharging) rates same **fraction** of energy is best **transferred across** resistors.

For n number of ‘memory elements’ (L and C),

- ★ let $x \in \mathbb{R}^n$: the state: vector of capacitor voltages and inductor currents
- ★ required supply = $x^T(K_{\text{reqd}})x$ and available storage = $x^T(K_{\text{avail}})x$ with
- ★ K_{avail} and K_{reqd} **symmetric $n \times n$ matrices**

- $\frac{1}{2}Cv_0^2$ is **geometric** mean of $\frac{1}{2}K_{\text{reqd}}v_0^2$ and $\frac{1}{2}K_{\text{avail}}v_0^2$
- Why **geometric**? Why not arithmetic/harmonic means?

$$\text{(while charging)} \quad \frac{C}{K_{\text{reqd}}} = \frac{K_{\text{avail}}}{C} \quad \text{(while discharging)}$$

- Perhaps not too surprising: at optimal (charging/discharging) rates same **fraction** of energy is best **transferred across** resistors.

For n number of ‘memory elements’ (L and C),

- ★ let $x \in \mathbb{R}^n$: the state: vector of capacitor voltages and inductor currents
- ★ required supply = $x^T(K_{\text{reqd}})x$ and available storage = $x^T(K_{\text{avail}})x$ with
- ★ K_{avail} and K_{reqd} **symmetric $n \times n$ matrices**
- ★ Standard Riccati equation procedures (from a state space representation of RLC network) to compute K_{avail} and K_{reqd}
- ★ Geometric mean of **matrices??**

$\dot{x} = Ax + Bi$ and $v = Cx + Di$: minimal state space realization of **biproper** impedance matrix $Z(s)$

x is vector of capacitor voltages and inductor currents and $x(0) = a \in \mathbb{R}^n$

$\dot{x} = Ax + Bi$ and $v = Cx + Di$: minimal state space realization of **biproper** impedance matrix $Z(s)$

x is vector of capacitor voltages and inductor currents and $x(0) = a \in \mathbb{R}^n$

Suppose $x(0) = a \in \mathbb{R}^n$ is a given voltage/current **configuration**

- **Required** supply is $a^T K_{\text{reqd}} a$ and **available** storage is $a^T K_{\text{avail}} a$:
 K_{reqd} and K_{avail} are maximum and minimum solutions of the Algebraic Riccati Equation (ARE):

$$A^T K + KA + (KB - C^T)(D + D^T)^{-1}(B^T K - C) \leq 0$$

- **Quadratic** in unknown $K \in \mathbb{R}^{n \times n}$ (we seek symmetric solutions)
- Multi-state: symmetric solutions of ARE/ARI form a ‘poset’ (partially **ordered set**): K_{avail} and K_{reqd} are minimum/maximum elements
- My work so far: uncontrollable case (with D. Pal, S. Karikalan, C. Athalye: IJC 2014, SIAM 2008)
- Today: network topology link

Assume biproper impedance $Z(s)$ and admittance $Y(s)$: construct $\frac{d}{dt}x = A_z x + B_z i$, $v = C_z x + D_z i$ and $\frac{d}{dt}x = A_y x + B_y v$, $i = C_y x + D_y v$.

- Construct \hat{x} has $2n$ components: consists of x and ‘dual state’ λ :
 - ★ original state x (capacitor voltage/inductor current), and
 - ★ the dual/adjoint/Lagrange multiplier λ
 - ★ Admittance $Y(s)$ gives $2n \times 2n$ matrix H_y
 - ★ Impedance $Z(s)$ gives $2n \times 2n$ matrix H_z

New results

Assume biproper impedance $Z(s)$ and admittance $Y(s)$: construct $\frac{d}{dt}x = A_z x + B_z i$, $v = C_z x + D_z i$ and $\frac{d}{dt}x = A_y x + B_y v$, $i = C_y x + D_y v$.

- Construct \hat{x} has $2n$ components: consists of x and ‘dual state’ λ :
 - ★ original state x (capacitor voltage/inductor current), and
 - ★ the dual/adjoint/Lagrange multiplier λ
 - ★ Admittance $Y(s)$ gives $2n \times 2n$ matrix H_y
 - ★ Impedance $Z(s)$ gives $2n \times 2n$ matrix H_z

Optimal trajectories dynamics: **independent** of impedance/admittance state-space realization:

$$\frac{d}{dt}\hat{x} = H_y \hat{x}, \quad \frac{d}{dt}\hat{x} = H_z \hat{x} \quad \text{then} \quad H_y = H_z$$

Common eigenspaces

Suppose some capacitors form cutsets with ports: those states

- ★ result in imaginary axis eigenvalues of A_z

New results

Assume biproper impedance $Z(s)$ and admittance $Y(s)$: construct $\frac{d}{dt}x = A_z x + B_z i$, $v = C_z x + D_z i$ and $\frac{d}{dt}x = A_y x + B_y v$, $i = C_y x + D_y v$.

- Construct \hat{x} has $2n$ components: consists of x and ‘dual state’ λ :
 - ★ original state x (capacitor voltage/inductor current), and
 - ★ the dual/adjoint/Lagrange multiplier λ
 - ★ Admittance $Y(s)$ gives $2n \times 2n$ matrix H_y
 - ★ Impedance $Z(s)$ gives $2n \times 2n$ matrix H_z

Optimal trajectories dynamics: **independent** of impedance/admittance state-space realization:

$$\frac{d}{dt}\hat{x} = H_y \hat{x}, \quad \frac{d}{dt}\hat{x} = H_z \hat{x} \quad \text{then} \quad H_y = H_z$$

Common eigenspaces

Suppose some capacitors form cutsets with ports: those states

- ★ result in imaginary axis eigenvalues of A_z
- ★ span common eigenspaces of A_z , K_{reqd} and K_{avail} (and all K)

New results

Assume biproper impedance $Z(s)$ and admittance $Y(s)$: construct $\frac{d}{dt}x = A_z x + B_z i$, $v = C_z x + D_z i$ and $\frac{d}{dt}x = A_y x + B_y v$, $i = C_y x + D_y v$.

- Construct \hat{x} has $2n$ components: consists of x and ‘dual state’ λ :
 - ★ original state x (capacitor voltage/inductor current), and
 - ★ the dual/adjoint/Lagrange multiplier λ
 - ★ Admittance $Y(s)$ gives $2n \times 2n$ matrix H_y
 - ★ Impedance $Z(s)$ gives $2n \times 2n$ matrix H_z

Optimal trajectories dynamics: **independent** of impedance/admittance state-space realization:

$$\frac{d}{dt}\hat{x} = H_y \hat{x}, \quad \frac{d}{dt}\hat{x} = H_z \hat{x} \quad \text{then} \quad H_y = H_z$$

Common eigenspaces

Suppose some capacitors form cutsets with ports: those states

- ★ result in imaginary axis eigenvalues of A_z
- ★ span common eigenspaces of A_z , K_{reqd} and K_{avail} (and all K)
- ★ are in the nullspace of $K_{\text{reqd}} - K_{\text{avail}}$

New results

Assume biproper impedance $Z(s)$ and admittance $Y(s)$: construct $\frac{d}{dt}x = A_z x + B_z i$, $v = C_z x + D_z i$ and $\frac{d}{dt}x = A_y x + B_y v$, $i = C_y x + D_y v$.

- Construct \hat{x} has $2n$ components: consists of x and ‘dual state’ λ :
 - ★ original state x (capacitor voltage/inductor current), and
 - ★ the dual/adjoint/Lagrange multiplier λ
 - ★ Admittance $Y(s)$ gives $2n \times 2n$ matrix H_y
 - ★ Impedance $Z(s)$ gives $2n \times 2n$ matrix H_z

Optimal trajectories dynamics: **independent** of impedance/admittance state-space realization:

$$\frac{d}{dt}\hat{x} = H_y \hat{x}, \quad \frac{d}{dt}\hat{x} = H_z \hat{x} \quad \text{then} \quad H_y = H_z$$

Common eigenspaces

Suppose some capacitors form cutsets with ports: those states

- ★ result in imaginary axis eigenvalues of A_z
- ★ span common eigenspaces of A_z , K_{reqd} and K_{avail} (and all K)
- ★ are in the nullspace of $K_{\text{reqd}} - K_{\text{avail}}$

Also: for L forming loops with ports, and ‘LC tanks’ forming cutsets/loops with ports

Geometric mean of matrices?

Recall: $K_{\text{reqd}} \times K_{\text{avail}} = c^2$. Generalize to many states?

- Assume multiport RC network
- ‘Normalize’ all states by c_i , i.e. $v_i \rightarrow \sqrt{\frac{c_i}{2}} v_i$
- In the new state variables, $v_0^T v_0$ is total **actual** energy
- **Diagonal** similarity transformation on A (of state space). Then

Geometric mean of matrices?

Recall: $K_{\text{reqd}} \times K_{\text{avail}} = c^2$. Generalize to many states?

- Assume multiport RC network
- ‘Normalize’ all states by c_i , i.e. $v_i \rightarrow \sqrt{\frac{c_i}{2}} v_i$
- In the new state variables, $v_0^T v_0$ is total **actual** energy
- **Diagonal** similarity transformation on A (of state space). Then

In the new state-space basis, $K_{\text{avail}} \leq I \leq K_{\text{reqd}}$

Geometric mean of matrices?

Recall: $K_{\text{reqd}} \times K_{\text{avail}} = c^2$. Generalize to many states?

- Assume multiport RC network
- ‘Normalize’ all states by c_i , i.e. $v_i \rightarrow \sqrt{\frac{c_i}{2}} v_i$
- In the new state variables, $v_0^T v_0$ is total **actual** energy
- **Diagonal** similarity transformation on A (of state space). Then

In the new state-space basis, $K_{\text{avail}} \leq I \leq K_{\text{reqd}}$

$(K_{\text{avail}})^{-1} = K_{\text{reqd}}$: ‘geometric mean’ (post-normalization)

Geometric mean of matrices?

Recall: $K_{\text{reqd}} \times K_{\text{avail}} = c^2$. Generalize to many states?

- Assume multiport RC network
- ‘Normalize’ all states by c_i , i.e. $v_i \rightarrow \sqrt{\frac{c_i}{2}} v_i$
- In the new state variables, $v_0^T v_0$ is total **actual** energy
- **Diagonal** similarity transformation on A (of state space). Then

In the new state-space basis, $K_{\text{avail}} \leq I \leq K_{\text{reqd}}$

$(K_{\text{avail}})^{-1} = K_{\text{reqd}}$: ‘geometric mean’ (post-normalization)

In other words,

Capacitor voltage normalizing achieves ‘**positive real balancing**’!

Geometric mean of matrices?

Recall: $K_{\text{reqd}} \times K_{\text{avail}} = c^2$. Generalize to many states?

- Assume multiport RC network
- ‘Normalize’ all states by c_i , i.e. $v_i \rightarrow \sqrt{\frac{c_i}{2}} v_i$
- In the new state variables, $v_0^T v_0$ is total **actual** energy
- **Diagonal** similarity transformation on A (of state space). Then

In the new state-space basis, $K_{\text{avail}} \leq I \leq K_{\text{reqd}}$

$(K_{\text{avail}})^{-1} = K_{\text{reqd}}$: ‘geometric mean’ (post-normalization)

In other words,

Capacitor voltage normalizing achieves ‘**positive real balancing**’!

- For a system with transfer matrix $G(s)$,
passive $\equiv G(s)$ is positive real
(no poles in ORHP, and $G(s) + G(-s)^T \geq 0$ for each s in complex RHP)
- Positive real balancing:

Geometric mean of matrices?

Recall: $K_{\text{reqd}} \times K_{\text{avail}} = c^2$. Generalize to many states?

- Assume multiport RC network
- ‘Normalize’ all states by c_i , i.e. $v_i \rightarrow \sqrt{\frac{c_i}{2}} v_i$
- In the new state variables, $v_0^T v_0$ is total **actual** energy
- **Diagonal** similarity transformation on A (of state space). Then

In the new state-space basis, $K_{\text{avail}} \leq I \leq K_{\text{reqd}}$

$(K_{\text{avail}})^{-1} = K_{\text{reqd}}$: ‘geometric mean’ (post-normalization)

In other words,

Capacitor voltage normalizing achieves ‘**positive real balancing**’!

- For a system with transfer matrix $G(s)$,
passive $\equiv G(s)$ is positive real
(no poles in ORHP, and $G(s) + G(-s)^T \geq 0$ for each s in complex RHP)
- Positive real balancing: **find** state-space basis such that:

$$\begin{aligned} \text{ARE1:} \quad & A^T K + K A + (K B - C^T)(D + D^T)^{-1}(B^T K - C) = 0 \quad \text{and} \\ \text{ARE2:} \quad & P A^T + A P + (P C^T - B)(D + D^T)^{-1}(C P - B^T) = 0 \end{aligned}$$

have **identical** solution sets $\subset \mathbb{R}^{n \times n}$

Geometric mean of matrices?

Recall: $K_{\text{reqd}} \times K_{\text{avail}} = c^2$. Generalize to many states?

- Assume multiport RC network
- ‘Normalize’ all states by c_i , i.e. $v_i \rightarrow \sqrt{\frac{c_i}{2}} v_i$
- In the new state variables, $v_0^T v_0$ is total **actual** energy
- **Diagonal** similarity transformation on A (of state space). Then

In the new state-space basis, $K_{\text{avail}} \leq I \leq K_{\text{reqd}}$

$(K_{\text{avail}})^{-1} = K_{\text{reqd}}$: ‘geometric mean’ (post-normalization)

In other words,

Capacitor voltage normalizing achieves ‘**positive real balancing**’!

- For a system with transfer matrix $G(s)$,
passive $\equiv G(s)$ is positive real
(no poles in ORHP, and $G(s) + G(-s)^T \geq 0$ for each s in complex RHP)
- Positive real balancing: **find** state-space basis such that:

$$\begin{aligned} \text{ARE1:} \quad & A^T K + K A + (K B - C^T)(D + D^T)^{-1}(B^T K - C) = 0 \quad \text{and} \\ \text{ARE2:} \quad & P A^T + A P + (P C^T - B)(D + D^T)^{-1}(C P - B^T) = 0 \end{aligned}$$

have **identical** solution sets $\subset \mathbb{R}^{n \times n}$
 $\Leftrightarrow (K_{\text{max}})^{-1} = K_{\text{min}}$

- Balancing useful in Model Order Reduction (MOR)
 - Balanced truncation:
discard those states that are ‘very’ uncontrollable **and** ‘very’ unobservable
 - **Retain** states only if:
 - ★ very controllable (low $x^T P^{-1} x$) **and**
 - ★ very observable (high $x^T Q x$)
- Controllability Grammian P & Observability Grammian Q

¹We do **not** get **diagonal** solutions: so-called ‘principal-axis’ balanced

- Balancing useful in Model Order Reduction (MOR)
- Balanced truncation:
discard those states that are ‘very’ uncontrollable **and** ‘very’ unobservable
- **Retain** states only if:
 - ★ very controllable (low $x^T P^{-1} x$) **and**
 - ★ very observable (high $x^T Q x$)

Controllability Grammian P & Observability Grammian Q

Procedure: simultaneous diagonalization of P and Q

¹We do **not** get **diagonal** solutions: so-called ‘principal-axis’ balanced

Why positive real balancing: MOR

- Balancing useful in Model Order Reduction (MOR)
 - Balanced truncation:
discard those states that are ‘very’ uncontrollable **and** ‘very’ unobservable
 - **Retain** states only if:
 - ★ very controllable (low $x^T P^{-1} x$) **and**
 - ★ very observable (high $x^T Q x$)
- Controllability Grammian P & Observability Grammian Q
Procedure: simultaneous diagonalization of P and Q
- In general, **positive real** balancing: simultaneous diagonalization (of K and L)
Involves Riccati equation solution: then Cholesky factorization
 - We showed¹ :

for RC circuits

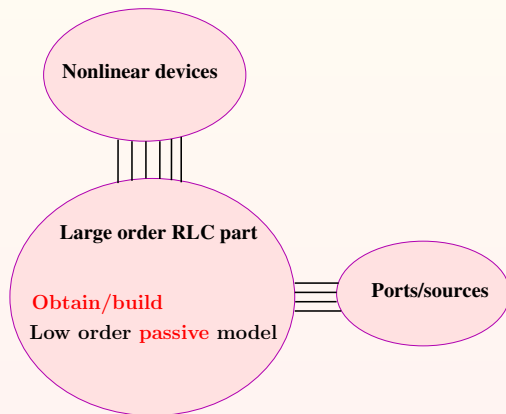
capacitor voltage **normalizing** results in **balancing**.

- Also true for: RL, and ‘symmetric’ realizations $A = A^T$ (of the state space)
(Recall Laplacian $L = L^T$ in RC example: though no ports there)

¹We do **not** get **diagonal** solutions: so-called ‘principal-axis’ balanced

Passive **reduced-order** LTI models: important for

- circuit simulation and analysis,
- controller design



- RL systems
- Multi-agents:
 - Network of many agents to achieve a task collectively
 - Surveillance pursuit-evasion games
 - Controlled through port \equiv one or more agents are 'leaders'
 - Laplacian matrix arises for single-integrator dynamics
- Network of Voltage-Source-Inverters (VSI) forming a microgrid (after neglecting sufficiently quick dynamics):
with Iyer, Chandorkar: IEEE-Trans-PEL 2010 & IEEE-Trans-Energy Conv 2011
- Mass-damper systems
- Other so-called ZIP (Zero-Interlacing-Pole) systems

- Controller locations that achieve controllability/pole-placement
- Optimal charging/discharging matrix relations with RLC locations
- Positive real balancing and state variable normalization

- Controller locations that achieve controllability/pole-placement
- Optimal charging/discharging matrix relations with RLC locations
- Positive real balancing and state variable normalization

Thank you for your attention

- Controller locations that achieve controllability/pole-placement
- Optimal charging/discharging matrix relations with RLC locations
- Positive real balancing and state variable normalization

Thank you for your attention

Also thanks to:

- R.U. Chavan, R.K. Kalaimani, Dr. Krishnan (Math), Ameer K. Mulla.
- Vinamzi Samuel and Kaushik Mallick (MTP with me):
OpenModelica/Python/Scilab based package