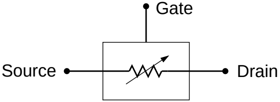
EE101: JFET operation and characteristics

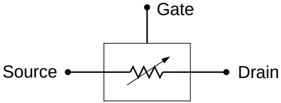
M. B. Patil
mbpatil@ee.iitb.ac.in
www.ee.iitb.ac.in/~sequel

Department of Electrical Engineering
Indian Institute of Technology Bombay

Field-effect transistors

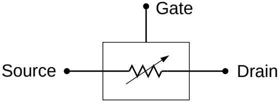


Field-effect transistors



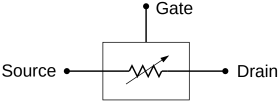
∗ A Field-Effect Transistor (FET) has a gate (G) terminal which controls the current flow between the other two terminals, viz., source (S) and drain (D).

Field-effect transistors



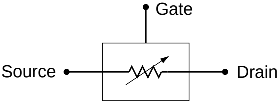
- A Field-Effect Transistor (FET) has a gate (G) terminal which controls the current flow between the other two terminals, viz., source (S) and drain (D).
- In simple terms, a FET can be thought of as a resistance connected between S and D, which is a function of the gate voltage V_G.

Field-effect transistors



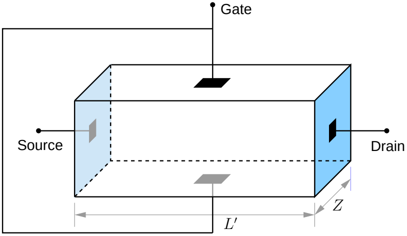
- ∗ A Field-Effect Transistor (FET) has a gate (G) terminal which controls the current flow between the other two terminals, viz., source (S) and drain (D).
- ∗ In simple terms, a FET can be thought of as a resistance connected between S and D, which is a function of the gate voltage V_G.
- ∗ The mechanism of gate control varies in different types of FETs, e.g., JFET, MESFET, MOSFET, HEMT.

Field-effect transistors

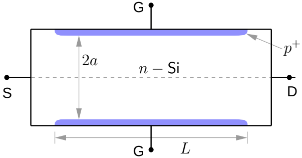


- A Field-Effect Transistor (FET) has a gate (G) terminal which controls the current flow between the other two terminals, viz., source (S) and drain (D).
- In simple terms, a FET can be thought of as a resistance connected between S and D, which is a function of the gate voltage V_G.
- The mechanism of gate control varies in different types of FETs, e.g., JFET, MESFET, MOSFET, HEMT.
- FETs can be used for analog and digital applications. In each case, the fact that the gate is used to control current flow between S and D plays a crucial role.

Junction Field-effect transistors (JFET)

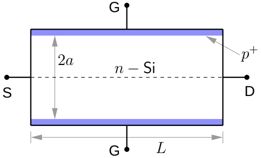


3D view



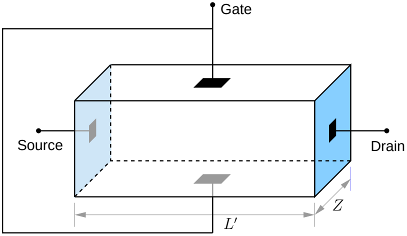
(Not drawn to scale. Typically, $L \gg 2a$.)

Cross−sectional view

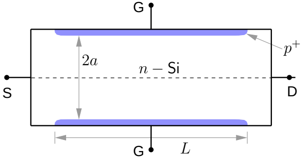


Simplified structure

Junction Field-effect transistors (JFET)

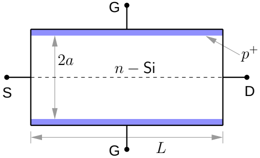


3D view



(Not drawn to scale. Typically, $L \gg 2a$.)

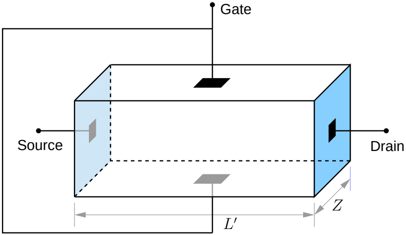
Cross−sectional view



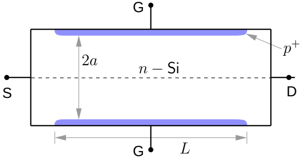
Simplified structure

- The *n*-type region between the top and bottom p^+ regions offers a resistance to current flow. The resistance depends on V_G.

Junction Field-effect transistors (JFET)

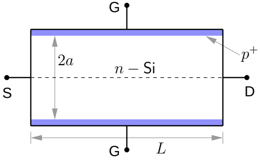


3D view



(Not drawn to scale. Typically, $L \gg 2a$.)

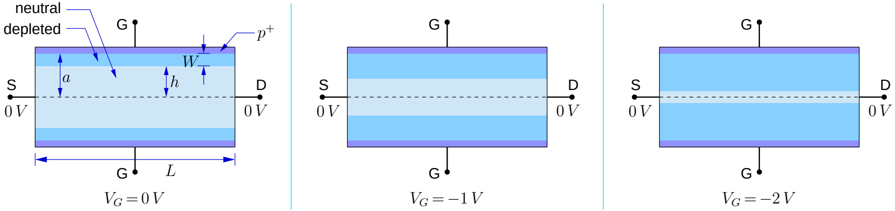
Cross−sectional view



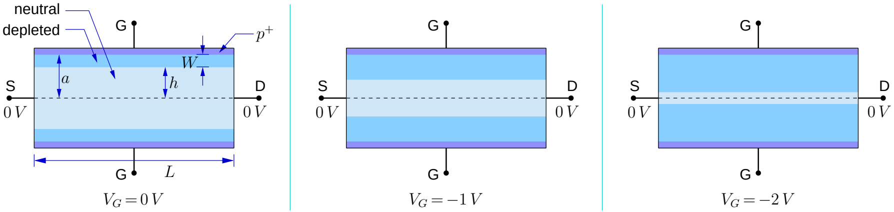
Simplified structure

- The *n*-type region between the top and bottom p^+ regions offers a resistance to current flow. The resistance depends on V_G.
- We will first consider the case, $V_D = V_S = 0\ V$.

JFET with $V_S = V_D = 0\ V$

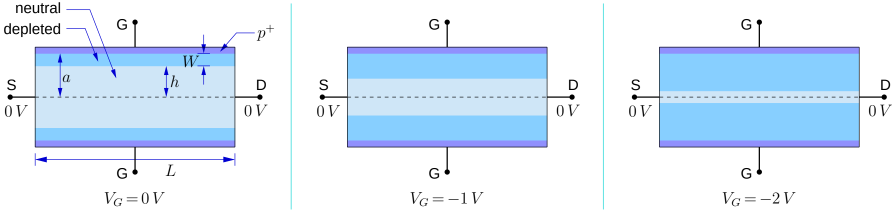


JFET with $V_S = V_D = 0\ V$



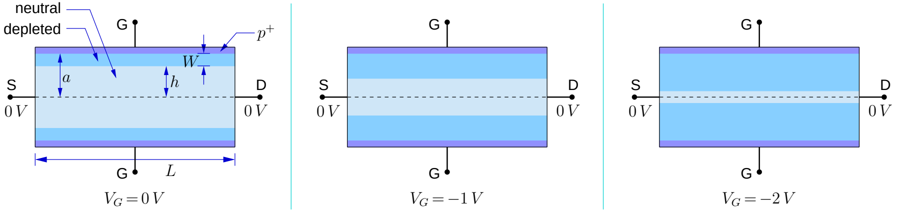
- The bias across the p-n junction is $(V_G - V_S)$, i.e., V_G, since $V_S = V_D = 0\ V$.

JFET with $V_S = V_D = 0\ V$



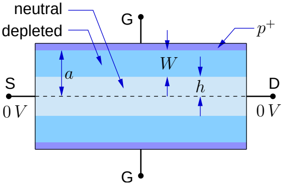
- The bias across the *p*-*n* junction is $(V_G - V_S)$, i.e., V_G, since $V_S = V_D = 0\ V$.
- As the reverse bias across the junction is increased (by making V_G more negative), the depletion region widens, and the resistance offered by the *n*-region increases.

JFET with $V_S = V_D = 0\ V$

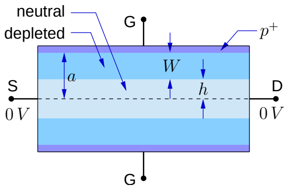


- The bias across the *p*-*n* junction is $(V_G - V_S)$, i.e., V_G, since $V_S = V_D = 0\ V$.
- As the reverse bias across the junction is increased (by making V_G more negative), the depletion region widens, and the resistance offered by the *n*-region increases.
- When the reverse bias becomes large enough, the depletion region consumes the entire *n*-region. The corresponding V_G is called the "pinch-off" voltage.

JFET: pinch-off voltage

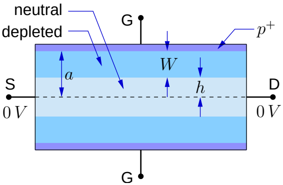


JFET: pinch-off voltage



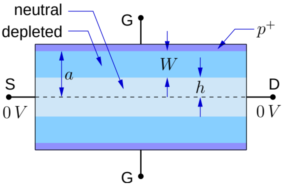
- $V_P = V_G$ for which $h = 0$, i.e., $W = a$.

JFET: pinch-off voltage



- $V_P = V_G$ for which $h = 0$, i.e., $W = a$.
- For a p^+-n junction, $W = \sqrt{\dfrac{2\,\epsilon\,(V_{\mathrm{bi}} - V)}{q\,N_d}}$, where V_{bi} is the built-in potential of the junction.

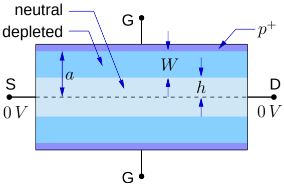
JFET: pinch-off voltage



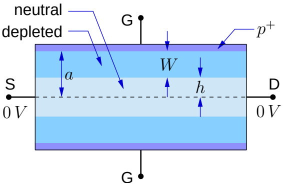
- $V_P = V_G$ for which $h = 0$, i.e., $W = a$.
- For a p^+-n junction, $W = \sqrt{\dfrac{2\,\epsilon\,(V_{\text{bi}} - V)}{q\,N_d}}$, where V_{bi} is the built-in potential of the junction.
- For pinch-off, $W = a = \sqrt{\dfrac{2\,\epsilon\,(V_{\text{bi}} - V)}{q\,N_d}}$

  $\Rightarrow V_P = V_{\text{bi}} - \dfrac{q\,N_d\,a^2}{2\,\epsilon}$.

JFET: pinch-off voltage

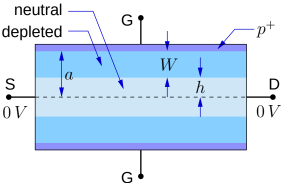


JFET: pinch-off voltage



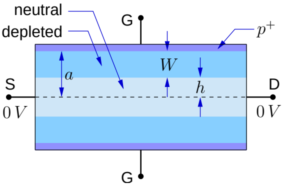
- For pinch-off, $W = a = \sqrt{\dfrac{2\,\epsilon\,(V_{\rm bi} - V)}{q\,N_d}} \Rightarrow V_P = V_{\rm bi} - \dfrac{q\,N_d\,a^2}{2\,\epsilon}$.

JFET: pinch-off voltage



- For pinch-off, $W = a = \sqrt{\dfrac{2\,\epsilon\,(V_{\text{bi}} - V)}{q\,N_d}} \Rightarrow V_P = V_{\text{bi}} - \dfrac{q\,N_d\,a^2}{2\,\epsilon}$.
- Example: $N_d = 2 \times 10^{15}\,\text{cm}^{-3}$, $a = 1.5\,\mu\text{m}$, $V_{\text{bi}} = 0.8\,V$.

JFET: pinch-off voltage

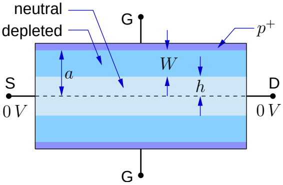


- For pinch-off, $W = a = \sqrt{\dfrac{2\,\epsilon\,(V_{\text{bi}} - V)}{q\,N_d}} \Rightarrow V_P = V_{\text{bi}} - \dfrac{q\,N_d\,a^2}{2\,\epsilon}$.
- Example: $N_d = 2 \times 10^{15}\ \text{cm}^{-3}$, $a = 1.5\ \mu\text{m}$, $V_{\text{bi}} = 0.8\ V$.

$$W = 0.8 - \frac{(1.6 \times 10^{-19}\ \text{Coul})(2 \times 10^{15}\ \text{cm}^{-3})((1.5 \times 10^{-4})^2\ \text{cm}^2)}{2 \times 11.7 \times 8.85 \times 10^{-14}\ F/\text{cm}}$$

$$= 0.8 - 3.48 \approx -2.7\ V\ .$$

JFET: pinch-off voltage



- For pinch-off, $W = a = \sqrt{\dfrac{2\,\epsilon\,(V_{\text{bi}} - V)}{q\,N_d}} \Rightarrow V_P = V_{\text{bi}} - \dfrac{q\,N_d\,a^2}{2\,\epsilon}$.

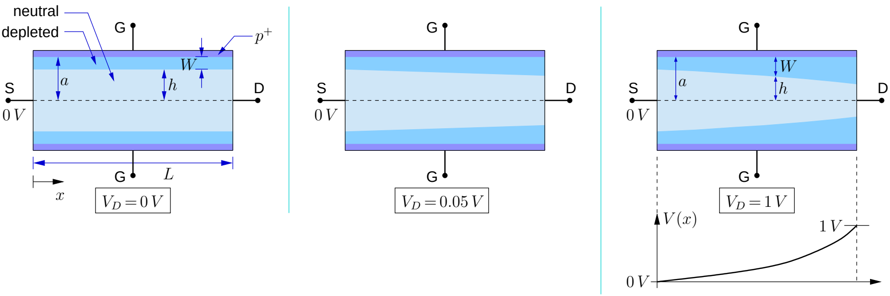
- Example: $N_d = 2 \times 10^{15}\,\text{cm}^{-3}$, $a = 1.5\,\mu\text{m}$, $V_{\text{bi}} = 0.8\,V$.

$$W = 0.8 - \frac{(1.6 \times 10^{-19}\,\text{Coul})(2 \times 10^{15}\,\text{cm}^{-3})((1.5 \times 10^{-4})^2\,\text{cm}^2)}{2 \times 11.7 \times 8.85 \times 10^{-14}\,F/\text{cm}}$$

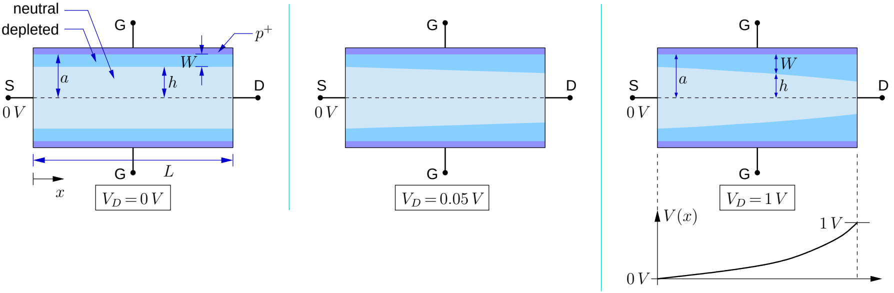
$$= 0.8 - 3.48 \approx -2.7\,V\,.$$

$\Rightarrow$ If a gate voltage $V_G = -2.7\,V$ is applied, the *n*-channel gets pinched off, and the device resistance becomes very large.

JFET with $V_G = \text{constant},\ V_D \neq 0\ V$

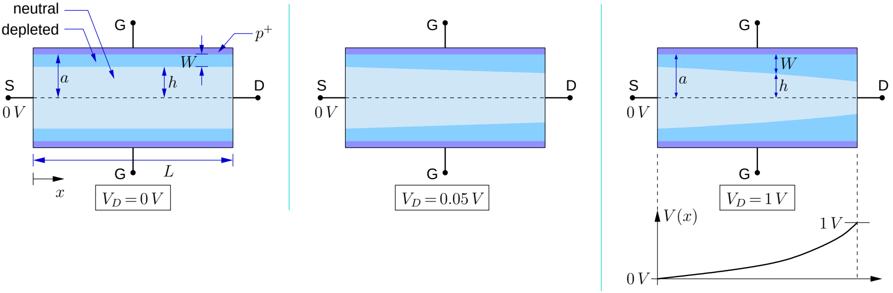


JFET with $V_G =$ constant, $V_D \neq 0\ V$



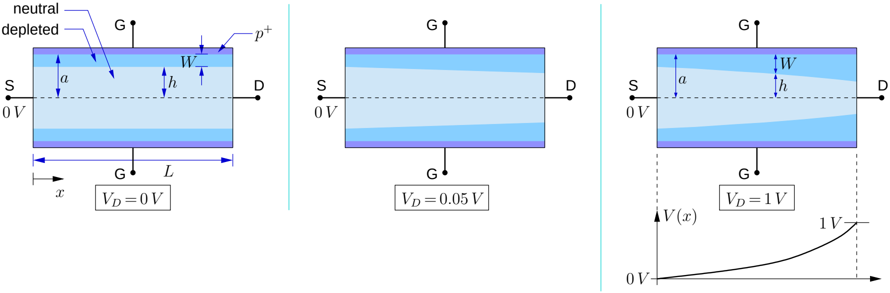
- ∗ Consider an *n*-JFET with V_G constant (and not in pinch-off mode).

JFET with $V_G =$ constant, $V_D \neq 0\,V$



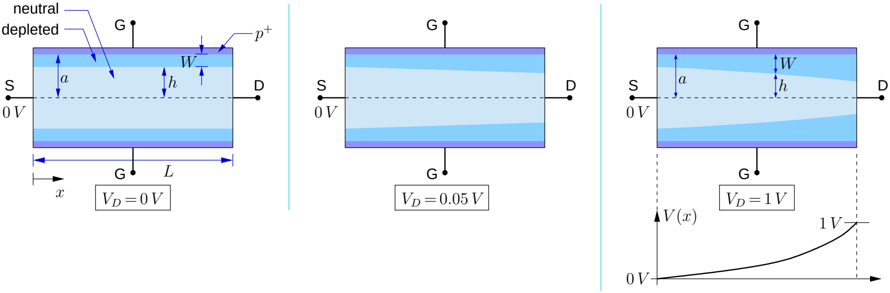
- ∗ Consider an *n*-JFET with V_G constant (and not in pinch-off mode).
  If a positive V_D is applied, the potential $V(x)$ inside the channel from S to D (along the dashed line) increases from $0\ V$ to V_D.

JFET with $V_G =$ constant, $V_D \neq 0\ V$



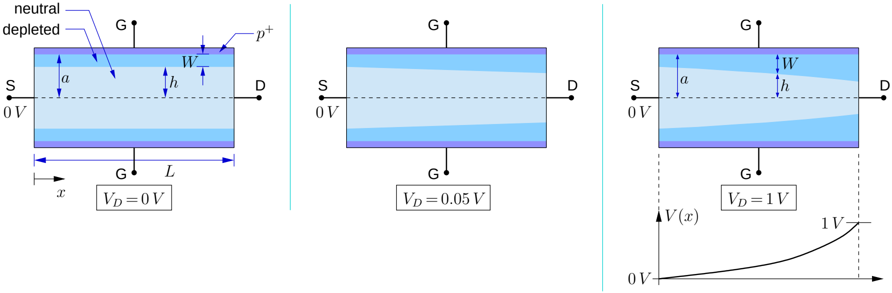
∗ Consider an *n*-JFET with V_G constant (and not in pinch-off mode).
If a positive V_D is applied, the potential $V(x)$ inside the channel from S to D (along the dashed line) increases from 0 V to V_D.
Note that W and h are now functions of x such that, $W(x) + h(x) = a$.

JFET with $V_G = \text{constant}$, $V_D \neq 0\ V$



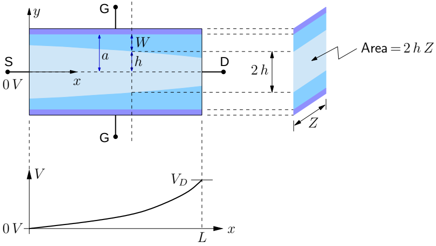
- * Consider an n-JFET with V_G constant (and not in pinch-off mode).
  If a positive V_D is applied, the potential $V(x)$ inside the channel from S to D (along the dashed line) increases from 0 V to V_D.
  Note that W and h are now functions of x such that, $W(x) + h(x) = a$.
- * Since the p-n junction bias at a given x is $(V_G - V(x))$, the drain end of the channel has a larger reverse bias than the source end.

JFET with $V_G =$ constant, $V_D \neq 0\,V$

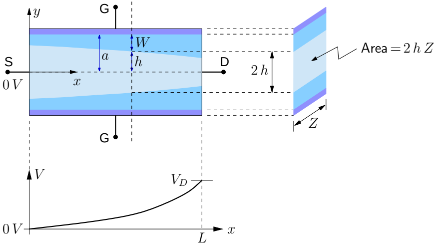


- * Consider an n-JFET with V_G constant (and not in pinch-off mode).
  If a positive V_D is applied, the potential $V(x)$ inside the channel from S to D (along the dashed line) increases from $0\,V$ to V_D.
  Note that W and h are now functions of x such that, $W(x) + h(x) = a$.
- * Since the p-n junction bias at a given x is $(V_G - V(x))$, the drain end of the channel has a larger reverse bias than the source end.
  $\Rightarrow$ the depletion region is wider at the drain.

JFET: derivation of I_D equation



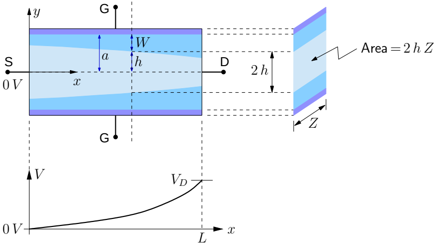
JFET: derivation of I_D equation



Consider a slice of the device. The current density at any point in the neutral region is assumed to be in the x direction, and given by,

$$J_n = q\mu_n nE + qD_n \frac{dn}{dx} \approx q\mu_n nE = q\mu_n N_d \frac{dV}{dx} \ ,$$

JFET: derivation of I_D equation

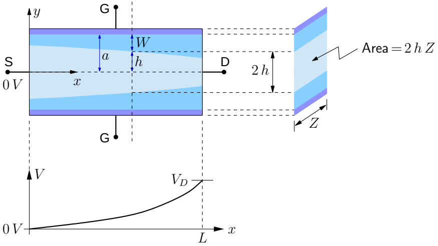


Consider a slice of the device. The current density at any point in the neutral region is assumed to be in the x direction, and given by,

$$J_n = q\mu_n nE + qD_n \frac{dn}{dx} \approx q\mu_n nE = q\mu_n N_d \frac{dV}{dx}\ ,$$

where we have neglected the diffusion current, since $n \approx N_d \Rightarrow \dfrac{dn}{dx} = 0$.

JFET: derivation of I_D equation



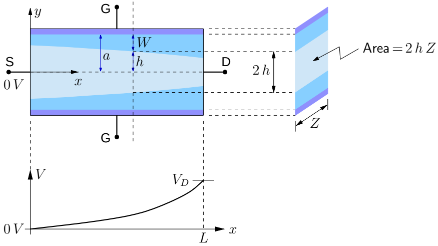
Consider a slice of the device. The current density at any point in the neutral region is assumed to be in the x direction, and given by,

$$J_n = q\mu_n nE + qD_n \frac{dn}{dx} \approx q\mu_n nE = q\mu_n N_d \frac{dV}{dx} \;,$$

where we have neglected the diffusion current, since $n \approx N_d \Rightarrow \dfrac{dn}{dx} = 0$.

Note that only the neutral part of the n-Si conducts since there are no carriers in the depletion regions.

JFET: derivation of I_D equation



Consider a slice of the device. The current density at any point in the neutral region is assumed to be in the x direction, and given by,

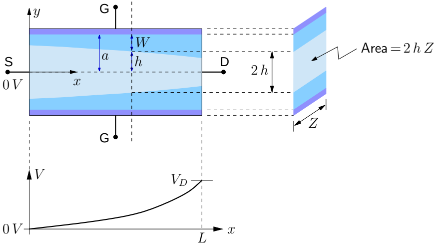
$$J_n = q\mu_n nE + qD_n\frac{dn}{dx} \approx q\mu_n nE = q\mu_n N_d\frac{dV}{dx}\ ,$$

where we have neglected the diffusion current, since $n \approx N_d \Rightarrow \dfrac{dn}{dx} = 0$.

Note that only the neutral part of the n-Si conducts since there are no carriers in the depletion regions.

At a given x, the current I_D is obtained by integrating J_n over the area of the neutral channel region (see figure on the right). Since J_n is constant over this area,

JFET: derivation of I_D equation



Consider a slice of the device. The current density at any point in the neutral region is assumed to be in the x direction, and given by,

$$J_n = q\mu_n nE + qD_n\frac{dn}{dx} \approx q\mu_n nE = q\mu_n N_d \frac{dV}{dx}\ ,$$

where we have neglected the diffusion current, since $n \approx N_d \Rightarrow \dfrac{dn}{dx} = 0$.

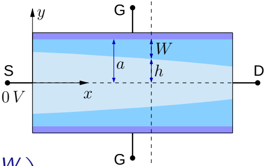
Note that only the neutral part of the n-Si conducts since there are no carriers in the depletion regions.

At a given x, the current I_D is obtained by integrating J_n over the area of the neutral channel region (see figure on the right). Since J_n is constant over this area,

$$I_D(x) = \int\!\!\int J_n dx\, dz = 2hZ \times \left(q\mu_n N_d \frac{dV}{dx}\right) = 2qZ\mu_n N_d a \frac{dV}{dx}\left(1 - \frac{W}{a}\right),$$

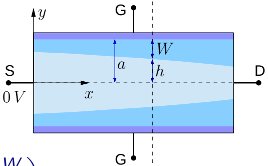
where we have used $h = a - W$, i.e., $h = a(1 - W/a)$.

JFET: derivation of I_D equation



$$I_D(x) = 2\,q\,Z\,\mu_n\,N_d\,a\frac{dV}{dx}\,\left(1-\frac{W}{a}\right).$$

JFET: derivation of I_D equation



$$I_D(x) = 2\,q\,Z\,\mu_n\,N_d\,a\,\frac{dV}{dx}\left(1-\frac{W}{a}\right).$$

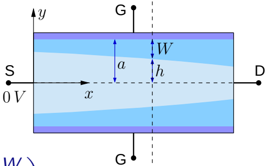
Since $I_D(x)$ is constant from $x=0$ to $x=L$, we get,

$$\int_0^L I_D\,dx = I_D\,L = 2qZ\mu_n N_d\,a\int_0^{V_D}\left(1-\sqrt{\frac{2\epsilon}{qN_d\,a^2}}\sqrt{V_{\mathrm{bi}}-(V_G-V)}\right)dV,$$

where we have used, for the depletion width W,

$$W(x) = \sqrt{\frac{2\epsilon}{qN_d}\left[V_{\mathrm{bi}}-(V_G-V)\right]}\,.$$

JFET: derivation of I_D equation



$$I_D(x) = 2\,q\,Z\,\mu_n\,N_d\,a\frac{dV}{dx}\left(1-\frac{W}{a}\right).$$

Since $I_D(x)$ is constant from $x=0$ to $x=L$, we get,

$$\int_0^L I_D\,dx = I_D L = 2qZ\mu_n N_d a\int_0^{V_D}\left(1-\sqrt{\frac{2\epsilon}{qN_d a^2}}\sqrt{V_{\rm bi}-(V_G-V)}\right)dV,$$

where we have used, for the depletion width W,

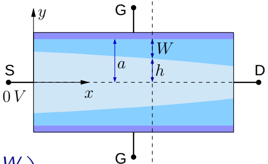
$$W(x) = \sqrt{\frac{2\epsilon}{qN_d}\left[V_{\rm bi}-(V_G-V)\right]}.$$

Evaluating the integral and using $V_{\rm bi}-V_P = \dfrac{qN_d a^2}{2\epsilon}$, we get (do this!)

$$I_D = G_0\left\{V_D-\frac{2}{3}(V_{\rm bi}-V_P)\left[\left(\frac{V_D+V_{\rm bi}-V_G}{V_{\rm bi}-V_P}\right)^{3/2}-\left(\frac{V_{\rm bi}-V_G}{V_{\rm bi}-V_P}\right)^{3/2}\right]\right\},$$

where $G_0 = 2qZ\mu_n N_d a/L$.

JFET: derivation of I_D equation



$$I_D(x) = 2\,q\,Z\,\mu_n\,N_d\,a\,\frac{dV}{dx}\,\left(1-\frac{W}{a}\right).$$

Since $I_D(x)$ is constant from $x=0$ to $x=L$, we get,

$$\int_0^L I_D\,dx = I_D L = 2qZ\mu_n N_d a \int_0^{V_D}\left(1-\sqrt{\frac{2\epsilon}{qN_d a^2}}\sqrt{V_{\rm bi}-(V_G-V)}\right)dV,$$

where we have used, for the depletion width W,

$$W(x) = \sqrt{\frac{2\epsilon}{qN_d}\left[V_{\rm bi}-(V_G-V)\right]}\,.$$

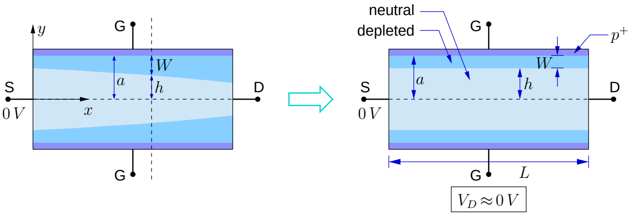
Evaluating the integral and using $V_{\rm bi}-V_P = \dfrac{qN_d a^2}{2\epsilon}$, we get (do this!)

$$I_D = G_0\left\{V_D - \frac{2}{3}\left(V_{\rm bi}-V_P\right)\left[\left(\frac{V_D+V_{\rm bi}-V_G}{V_{\rm bi}-V_P}\right)^{3/2} - \left(\frac{V_{\rm bi}-V_G}{V_{\rm bi}-V_P}\right)^{3/2}\right]\right\},$$

where $G_0 = 2qZ\mu_n N_d a/L$.

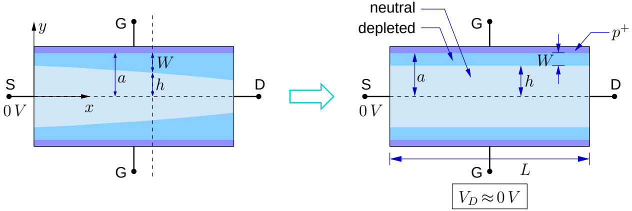
Note that G_0 is the channel conductance if there was no depletion, i.e., if $h(x)=a$ throughout the channel.

Special case: $V_D \approx 0\ V$



$$I_D \;=\; G_0 \left\{ V_D - \frac{2}{3}\,(V_{\text{bi}} - V_P) \left[\left(\frac{V_D + V_{\text{bi}} - V_G}{V_{\text{bi}} - V_P} \right)^{3/2} - \left(\frac{V_{\text{bi}} - V_G}{V_{\text{bi}} - V_P} \right)^{3/2} \right] \right\}$$

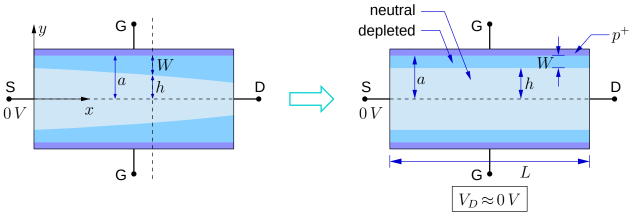
Special case: $V_D \approx 0\ V$



$$I_D = G_0 \left\{ V_D - \frac{2}{3}\,(V_{\text{bi}} - V_P) \left[\left(\frac{V_D + V_{\text{bi}} - V_G}{V_{\text{bi}} - V_P} \right)^{3/2} - \left(\frac{V_{\text{bi}} - V_G}{V_{\text{bi}} - V_P} \right)^{3/2} \right] \right\}$$

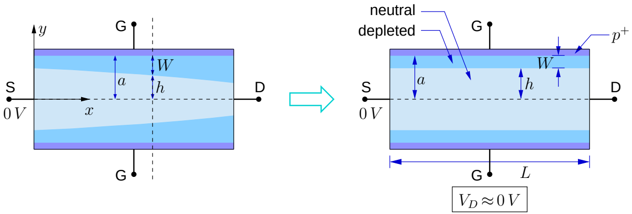
$$\approx G_0 \left\{ V_D - \frac{2}{3}\,(V_{\text{bi}} - V_P)^{-1/2} \left[\frac{3}{2}\, V_D\, (V_{\text{bi}} - V_G)^{1/2} \right] \right\} \quad \text{(using Taylor's series)}$$

Special case: $V_D \approx 0\ V$



$$
\begin{aligned}
I_D &= G_0 \left\{ V_D - \frac{2}{3}\,(V_{\text{bi}} - V_P) \left[\left(\frac{V_D + V_{\text{bi}} - V_G}{V_{\text{bi}} - V_P} \right)^{3/2} - \left(\frac{V_{\text{bi}} - V_G}{V_{\text{bi}} - V_P} \right)^{3/2} \right] \right\} \\
&\approx G_0 \left\{ V_D - \frac{2}{3}\,(V_{\text{bi}} - V_P)^{-1/2} \left[\frac{3}{2}\, V_D\, (V_{\text{bi}} - V_G)^{1/2} \right] \right\} \quad \text{(using Taylor's series)} \\
&= G_0\, V_D \left\{ 1 - \left(\frac{V_{\text{bi}} - V_G}{V_{\text{bi}} - V_P} \right)^{1/2} \right\}.
\end{aligned}
$$

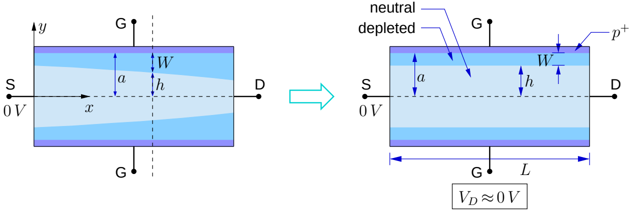
Special case: $V_D \approx 0\ V$



$$
\begin{aligned}
I_D &= G_0 \left\{ V_D - \frac{2}{3}\,(V_{\text{bi}} - V_P) \left[\left(\frac{V_D + V_{\text{bi}} - V_G}{V_{\text{bi}} - V_P} \right)^{3/2} - \left(\frac{V_{\text{bi}} - V_G}{V_{\text{bi}} - V_P} \right)^{3/2} \right] \right\} \\
&\approx G_0 \left\{ V_D - \frac{2}{3}\,(V_{\text{bi}} - V_P)^{-1/2} \left[\frac{3}{2}\, V_D\ (V_{\text{bi}} - V_G)^{1/2} \right] \right\} \quad \text{(using Taylor's series)} \\
&= G_0\, V_D \left\{ 1 - \left(\frac{V_{\text{bi}} - V_G}{V_{\text{bi}} - V_P} \right)^{1/2} \right\}.
\end{aligned}
$$

Since $W = \dfrac{2\epsilon}{qN_d}\,(V_{\text{bi}} - V_G)^{1/2}$, and $a = \dfrac{2\epsilon}{qN_d}\,(V_{\text{bi}} - V_P)^{1/2}$, we get

Special case: $V_D \approx 0\,V$



$$I_D = G_0 \left\{ V_D - \frac{2}{3}\,(V_{\text{bi}} - V_P) \left[\left(\frac{V_D + V_{\text{bi}} - V_G}{V_{\text{bi}} - V_P} \right)^{3/2} - \left(\frac{V_{\text{bi}} - V_G}{V_{\text{bi}} - V_P} \right)^{3/2} \right] \right\}$$

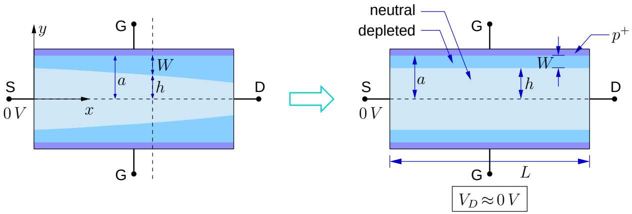
$$\approx G_0 \left\{ V_D - \frac{2}{3}\,(V_{\text{bi}} - V_P)^{-1/2} \left[\frac{3}{2}\, V_D\, (V_{\text{bi}} - V_G)^{1/2} \right] \right\} \quad \text{(using Taylor's series)}$$

$$= G_0\, V_D \left\{ 1 - \left(\frac{V_{\text{bi}} - V_G}{V_{\text{bi}} - V_P} \right)^{1/2} \right\}.$$

Since $W = \dfrac{2\epsilon}{qN_d}\,(V_{\text{bi}} - V_G)^{1/2}$, and $a = \dfrac{2\epsilon}{qN_d}\,(V_{\text{bi}} - V_P)^{1/2}$, we get

$$I_D = G_0\, V_D \left\{ 1 - \frac{W}{a} \right\}.$$

Special case: $V_D \approx 0\ V$



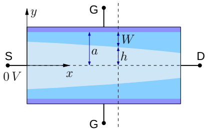
$$\begin{aligned}
I_D &= G_0 \left\{ V_D - \frac{2}{3}\,(V_{\text{bi}} - V_P) \left[\left(\frac{V_D + V_{\text{bi}} - V_G}{V_{\text{bi}} - V_P} \right)^{3/2} - \left(\frac{V_{\text{bi}} - V_G}{V_{\text{bi}} - V_P} \right)^{3/2} \right] \right\} \\
&\approx G_0 \left\{ V_D - \frac{2}{3}\,(V_{\text{bi}} - V_P)^{-1/2} \left[\frac{3}{2}\, V_D \, (V_{\text{bi}} - V_G)^{1/2} \right] \right\} \quad \text{(using Taylor's series)} \\
&= G_0 V_D \left\{ 1 - \left(\frac{V_{\text{bi}} - V_G}{V_{\text{bi}} - V_P} \right)^{1/2} \right\}.
\end{aligned}$$

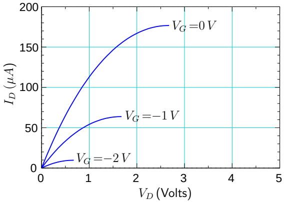
Since $W = \dfrac{2\epsilon}{qN_d}\,(V_{\text{bi}} - V_G)^{1/2}$, and $a = \dfrac{2\epsilon}{qN_d}\,(V_{\text{bi}} - V_P)^{1/2}$, we get

$$I_D = G_0 V_D \left\{ 1 - \frac{W}{a} \right\}.$$

This simply shows that the channel conductance reduces linearly with W (as seen before the $V_S = V_S = 0\ V$ condition), and for $V_G = V_P$ (i.e., $W = a$), the conductance becomes zero.

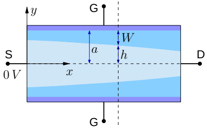
JFET: pinch-off near drain

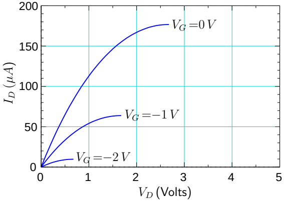




$$I_D = G_0 \left\{ V_D - \frac{2}{3}\,(V_{\mathrm{bi}} - V_P) \left[\left(\frac{V_D + V_{\mathrm{bi}} - V_G}{V_{\mathrm{bi}} - V_P} \right)^{3/2} - \left(\frac{V_{\mathrm{bi}} - V_G}{V_{\mathrm{bi}} - V_P} \right)^{3/2} \right] \right\}.$$

JFET: pinch-off near drain

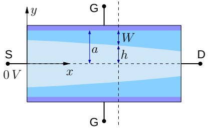


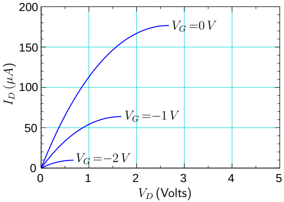


$$I_D = G_0 \left\{ V_D - \frac{2}{3}\left(V_{\text{bi}} - V_P\right) \left[\left(\frac{V_D + V_{\text{bi}} - V_G}{V_{\text{bi}} - V_P} \right)^{3/2} - \left(\frac{V_{\text{bi}} - V_G}{V_{\text{bi}} - V_P} \right)^{3/2} \right] \right\}.$$

For a given V_G, I_D reaches a maximum at $V_D = V_G - V_P$ (show this by differentiating the above equation).

JFET: pinch-off near drain



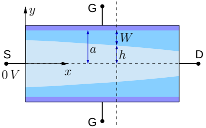


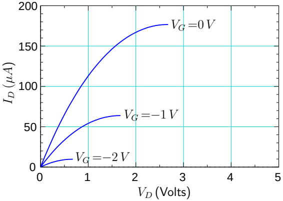
$$I_D = G_0 \left\{ V_D - \frac{2}{3}\left(V_{\text{bi}} - V_P\right)\left[\left(\frac{V_D + V_{\text{bi}} - V_G}{V_{\text{bi}} - V_P}\right)^{3/2} - \left(\frac{V_{\text{bi}} - V_G}{V_{\text{bi}} - V_P}\right)^{3/2}\right]\right\}.$$

For a given V_G, I_D reaches a maximum at $V_D = V_G - V_P$ (show this by differentiating the above equation).

At this value of V_D, the bias across the *p*-*n* junction at the drain end is $V_G - V_D = V_P$.

JFET: pinch-off near drain



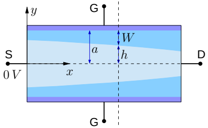


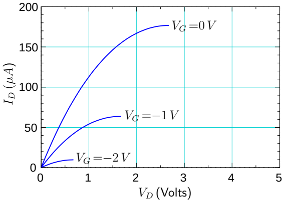
$$I_D = G_0 \left\{ V_D - \frac{2}{3}(V_{\text{bi}} - V_P) \left[\left(\frac{V_D + V_{\text{bi}} - V_G}{V_{\text{bi}} - V_P} \right)^{3/2} - \left(\frac{V_{\text{bi}} - V_G}{V_{\text{bi}} - V_P} \right)^{3/2} \right] \right\}.$$

For a given V_G, I_D reaches a maximum at $V_D = V_G - V_P$ (show this by differentiating the above equation).

At this value of V_D, the bias across the *p-n* junction at the drain end is $V_G - V_D = V_P$.
In other words, the drain end of the channel has *just* reached pinch-off.

JFET: pinch-off near drain

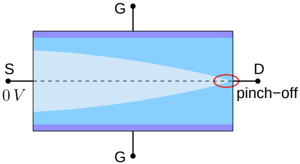




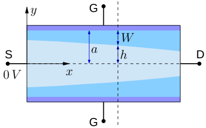
$$I_D = G_0 \left\{ V_D - \frac{2}{3}\left(V_{\text{bi}} - V_P\right) \left[\left(\frac{V_D + V_{\text{bi}} - V_G}{V_{\text{bi}} - V_P} \right)^{3/2} - \left(\frac{V_{\text{bi}} - V_G}{V_{\text{bi}} - V_P} \right)^{3/2} \right] \right\}.$$

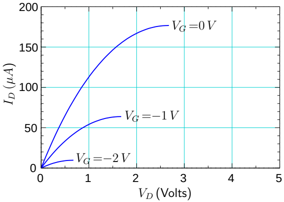
For a given V_G, I_D reaches a maximum at $V_D = V_G - V_P$ (show this by differentiating the above equation).

At this value of V_D, the bias across the *p*-*n* junction at the drain end is $V_G - V_D = V_P$.
In other words, the drain end of the channel has *just* reached pinch-off.



JFET: pinch-off near drain

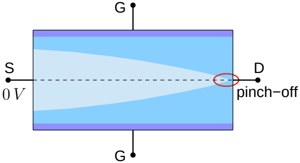




$$I_D = G_0 \left\{ V_D - \frac{2}{3}\left(V_{\text{bi}} - V_P\right)\left[\left(\frac{V_D + V_{\text{bi}} - V_G}{V_{\text{bi}} - V_P}\right)^{3/2} - \left(\frac{V_{\text{bi}} - V_G}{V_{\text{bi}} - V_P}\right)^{3/2}\right]\right\}.$$

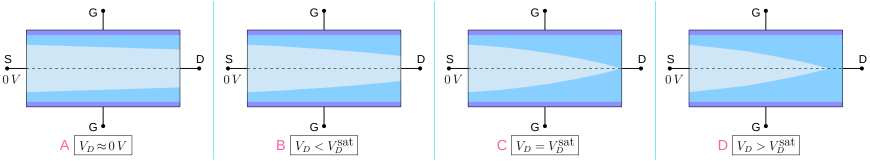
For a given V_G, I_D reaches a maximum at $V_D = V_G - V_P$ (show this by differentiating the above equation).

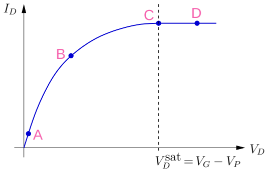
At this value of V_D, the bias across the *p*-*n* junction at the drain end is $V_G - V_D = V_P$.
In other words, the drain end of the channel has *just* reached pinch-off.



What happens if V_D is increased further?

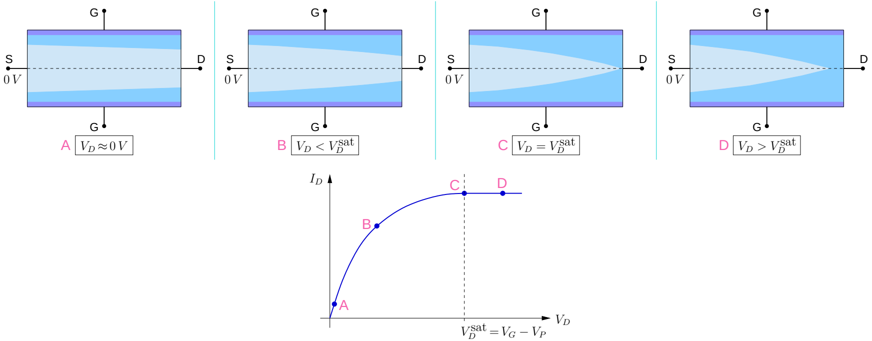
JFET: saturation





Consider a fixed V_G with V_D varying from $\sim 0\ V$ to a value beyond condition C.

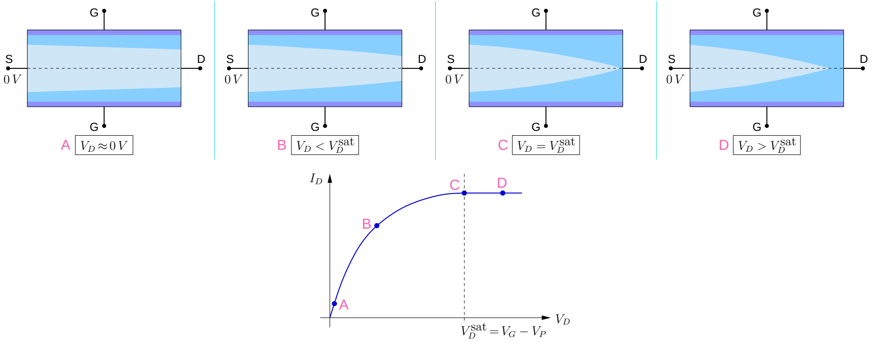
JFET: saturation



Consider a fixed V_G with V_D varying from $\sim 0\ V$ to a value beyond condition C.

In this situation, i.e., $V_D > V_D^{\text{sat}}$, a *short* high-field region develops near the drain end, and the "excess" voltage, $V_D - V_D^{\text{sat}}$ drops across this region.

JFET: saturation

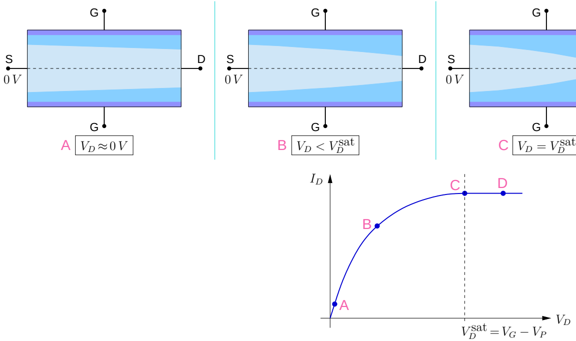


Consider a fixed V_G with V_D varying from $\sim 0\ V$ to a value beyond condition C.

In this situation, i.e., $V_D > V_D^{\text{sat}}$, a *short* high-field region develops near the drain end, and the "excess" voltage, $V_D - V_D^{\text{sat}}$ drops across this region.

Because the high-filed region is confined to a very small distance, the conditions in the device are almost identical in C and D.

JFET: saturation



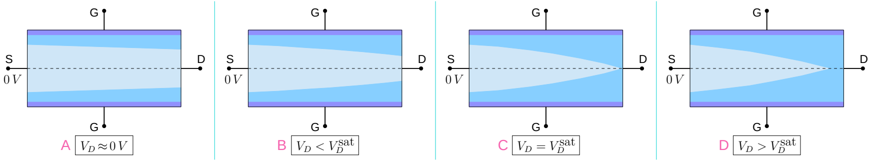
Consider a fixed V_G with V_D varying from $\sim 0\ V$ to a value beyond condition C.

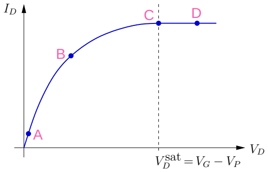
In this situation, i.e., $V_D > V_D^{\text{sat}}$, a *short* high-field region develops near the drain end, and the "excess" voltage, $V_D - V_D^{\text{sat}}$ drops across this region.

Because the high-filed region is confined to a very small distance, the conditions in the device are almost identical in C and D.

$\Rightarrow$ The current in case D is almost the same as that for case C.

JFET: saturation





Consider a fixed V_G with V_D varying from $\sim 0\ V$ to a value beyond condition C.

In this situation, i.e., $V_D > V_D^{\rm sat}$, a *short* high-field region develops near the drain end, and the "excess" voltage, $V_D - V_D^{\rm sat}$ drops across this region.

Because the high-filed region is confined to a very small distance, the conditions in the device are almost identical in C and D.

$\Rightarrow$ The current in case D is almost the same as that for case C.

The region $V_D > V_D^{\rm sat}$ is therefore called the "saturation region."

JFET: example

An n-channel silicon JFET has the following parameters (at $T=300\,K$): $a=1.5\,\mu$m, $L=5\,\mu$m, $Z=50\,\mu$m, $N_d=2\times10^{15}\,\text{cm}^{-3}$, $V_{\text{bi}}=0.8\,V$, $\mu_n=300\,\text{cm}^2/V$-sec.

(a) What is the pinch-off voltage?

(b) Write a program to generate I_D-V_D characteristics for $V_G=0\,V$, $-0.5\,V$, $-1\,V$, $-1.5\,V$, $-2\,V$.

(c) For each of the above V_G values, compute V_D^{sat}, and show it on the I_D-V_D plot. The part of an I_D-V_D corresponding to $V_D < V_D^{\text{sat}}$ is called the "linear" region, and that corresponding to $V_D > V_D^{\text{sat}}$ is called the "saturation" region.

JFET: example

An n-channel silicon JFET has the following parameters (at $T = 300\,K$): $a = 1.5\,\mu$m, $L = 5\,\mu$m, $Z = 50\,\mu$m, $N_d = 2 \times 10^{15}\,\text{cm}^{-3}$, $V_{\text{bi}} = 0.8\,V$, $\mu_n = 300\,\text{cm}^2/V$-sec.

(a) What is the pinch-off voltage?

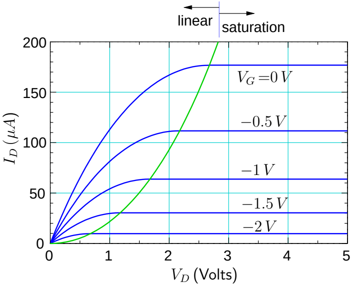
(b) Write a program to generate I_D-V_D characteristics for $V_G = 0\,V$, $-0.5\,V$, $-1\,V$, $-1.5\,V$, $-2\,V$.

(c) For each of the above V_G values, compute V_D^{sat}, and show it on the I_D-V_D plot. The part of an I_D-V_D corresponding to $V_D < V_D^{\text{sat}}$ is called the "linear" region, and that corresponding to $V_D > V_D^{\text{sat}}$ is called the "saturation" region.

Answer:

(a) $V_P = -2.68\,V$.

(b)



JFET: simplified model for saturation

$$I_D = G_0 \left\{ V_D - \frac{2}{3}\left(V_{\text{bi}} - V_P\right)\left[\left(\frac{V_D + V_{\text{bi}} - V_G}{V_{\text{bi}} - V_P}\right)^{3/2} - \left(\frac{V_{\text{bi}} - V_G}{V_{\text{bi}} - V_P}\right)^{3/2}\right]\right\}.$$

JFET: simplified model for saturation

$$I_D = G_0 \left\{ V_D - \frac{2}{3} \left(V_{\text{bi}} - V_P \right) \left[\left(\frac{V_D + V_{\text{bi}} - V_G}{V_{\text{bi}} - V_P} \right)^{3/2} - \left(\frac{V_{\text{bi}} - V_G}{V_{\text{bi}} - V_P} \right)^{3/2} \right] \right\}.$$

At saturtation, $V_D^{\text{sat}} = V_G - V_P$, giving

$$I_D^{\text{sat}} = G_0 \left\{ V_D - \frac{2}{3} \left(V_{\text{bi}} - V_P \right) \left[1 - \left(\frac{V_{\text{bi}} - V_G}{V_{\text{bi}} - V_P} \right)^{3/2} \right] \right\}.$$

JFET: simplified model for saturation

$$I_D = G_0 \left\{ V_D - \frac{2}{3}\left(V_{\rm bi} - V_P\right)\left[\left(\frac{V_D + V_{\rm bi} - V_G}{V_{\rm bi} - V_P}\right)^{3/2} - \left(\frac{V_{\rm bi} - V_G}{V_{\rm bi} - V_P}\right)^{3/2}\right]\right\}.$$

At saturtation, $V_D^{\rm sat} = V_G - V_P$, giving

$$I_D^{\rm sat} = G_0 \left\{ V_D - \frac{2}{3}\left(V_{\rm bi} - V_P\right)\left[1 - \left(\frac{V_{\rm bi} - V_G}{V_{\rm bi} - V_P}\right)^{3/2}\right]\right\}.$$

The following approximate model is found to be adequate in circuit design:

$I_D^{\rm sat}(V_G) = I_{DSS}\,(1 - V_G/V_P)^2$, where $I_{DSS} = I_D^{\rm sat}(V_G = 0\ V)$.

JFET: simplified model for saturation

$$I_D = G_0 \left\{ V_D - \frac{2}{3}\left(V_{\text{bi}} - V_P\right)\left[\left(\frac{V_D + V_{\text{bi}} - V_G}{V_{\text{bi}} - V_P}\right)^{3/2} - \left(\frac{V_{\text{bi}} - V_G}{V_{\text{bi}} - V_P}\right)^{3/2}\right]\right\}.$$

At saturtation, $V_D^{\text{sat}} = V_G - V_P$, giving

$$I_D^{\text{sat}} = G_0 \left\{ V_D - \frac{2}{3}\left(V_{\text{bi}} - V_P\right)\left[1 - \left(\frac{V_{\text{bi}} - V_G}{V_{\text{bi}} - V_P}\right)^{3/2}\right]\right\}.$$

The following approximate model is found to be adequate in circuit design:

$I_D^{\text{sat}}(V_G) = I_{DSS}\,(1 - V_G/V_P)^2$, where $I_{DSS} = I_D^{\text{sat}}(V_G = 0\ V)$.

In amplifier design, we are interested in $g_m = \left.\frac{\partial I_D}{\partial V_G}\right|_{V_D=\text{constant}}$, which is obtained as:

JFET: simplified model for saturation

$$I_D = G_0 \left\{ V_D - \frac{2}{3}\,(V_{\text{bi}} - V_P) \left[\left(\frac{V_D + V_{\text{bi}} - V_G}{V_{\text{bi}} - V_P} \right)^{3/2} - \left(\frac{V_{\text{bi}} - V_G}{V_{\text{bi}} - V_P} \right)^{3/2} \right] \right\}.$$

At saturtation, $V_D^{\text{sat}} = V_G - V_P$, giving

$$I_D^{\text{sat}} = G_0 \left\{ V_D - \frac{2}{3}\,(V_{\text{bi}} - V_P) \left[1 - \left(\frac{V_{\text{bi}} - V_G}{V_{\text{bi}} - V_P} \right)^{3/2} \right] \right\}.$$

The following approximate model is found to be adequate in circuit design:

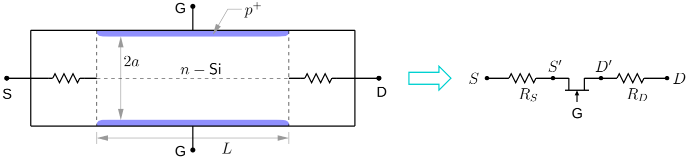
$I_D^{\text{sat}}(V_G) = I_{DSS}\,(1 - V_G/V_P)^2$, where $I_{DSS} = I_D^{\text{sat}}(V_G = 0\ V)$.

In amplifier design, we are interested in $g_m = \left.\dfrac{\partial I_D}{\partial V_G}\right|_{V_D=\text{constant}}$, which is obtained as:

$g_m = g_{m0}\,(1 - V_G/V_P)$,

where $g_{m0} = -2I_{DSS}/V_P = g_m(V_G = 0\ V)$.

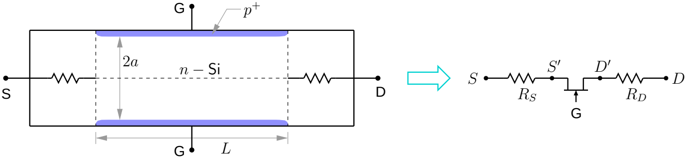
JFET: source/drain resistances



(Not drawn to scale. Typically, $L \gg 2a$.)

Cross−sectional view

JFET: source/drain resistances



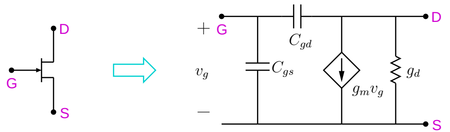
(Not drawn to scale. Typically, $L \gg 2a$.)

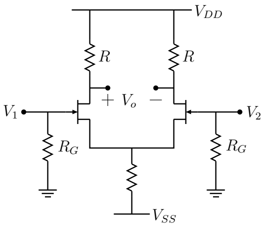
Cross−sectional view

In real JFETs, there is a separation between the source/drain contacts and the active channel.

The *n*-type semiconductor regions between the active channel and the source/drain contacts can be modelled by resistances R_S and R_D.

JFET: small-signal model

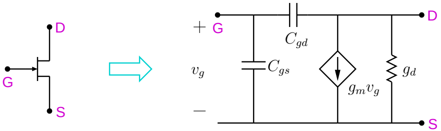


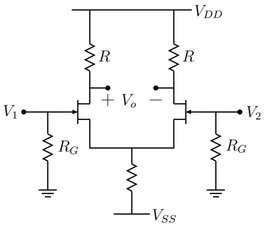


Amplifier example

- A small-signal model of a JFET is required in analysis of an amplifier.

JFET: small-signal model

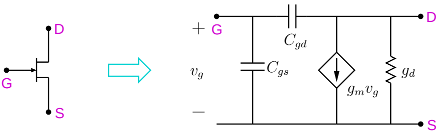


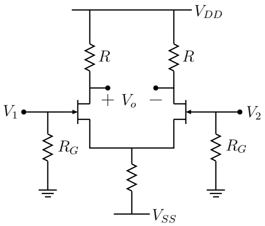


Amplifier example

- A small-signal model of a JFET is required in analysis of an amplifier.
- The DC gate current, which is the reverse current of a *p*-*n* junction, is generally insignificant and is therefore ignored.

JFET: small-signal model

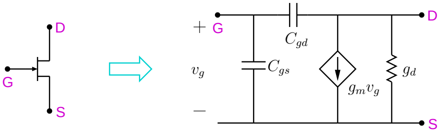


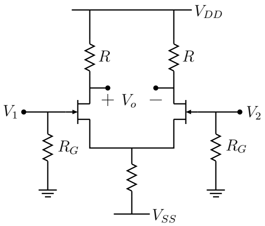


Amplifier example

- A small-signal model of a JFET is required in analysis of an amplifier.
- The DC gate current, which is the reverse current of a *p*-*n* junction, is generally insignificant and is therefore ignored.
- $g_m = \dfrac{\partial I_D}{\partial V_G}$ with $V_D =$ constant.

JFET: small-signal model

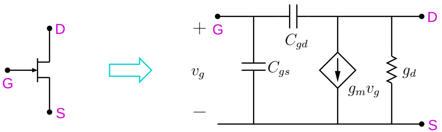


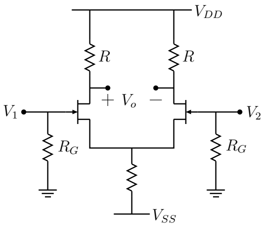


Amplifier example

- A small-signal model of a JFET is required in analysis of an amplifier.
- The DC gate current, which is the reverse current of a *p*-*n* junction, is generally insignificant and is therefore ignored.
- $g_m = \dfrac{\partial I_D}{\partial V_G}$ with $V_D =$ constant.
- $g_d = \dfrac{\partial I_D}{\partial V_D}$ with $V_G =$ constant.

JFET: small-signal model

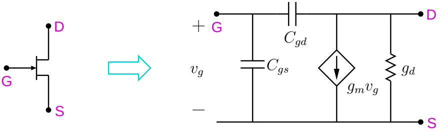


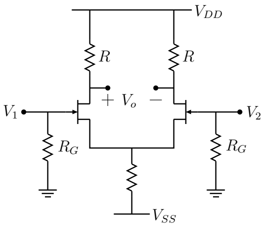


Amplifier example

- ∗ A small-signal model of a JFET is required in analysis of an amplifier.
- ∗ The DC gate current, which is the reverse current of a *p*-*n* junction, is generally insignificant and is therefore ignored.
- ∗ $g_m = \dfrac{\partial I_D}{\partial V_G}$ with $V_D =$ constant.
- ∗ $g_d = \dfrac{\partial I_D}{\partial V_D}$ with $V_G =$ constant.
- ∗ g_m and g_d can be obtained by differentiating $I_D(V_G, V_D)$. Note that, in our simple model, short-channel effects have not been included; we would therefore obtain $g_d = 0\,\mho$ in saturation. However, a real device would show a small increase in I_D with an increase in V_D in saturation, giving rise to a non-zero g_d.

JFET: small-signal model





Amplifier example

- A small-signal model of a JFET is required in analysis of an amplifier.
- The DC gate current, which is the reverse current of a *p*-*n* junction, is generally insignificant and is therefore ignored.
- $g_m = \dfrac{\partial I_D}{\partial V_G}$ with $V_D =$ constant.
- $g_d = \dfrac{\partial I_D}{\partial V_D}$ with $V_G =$ constant.
- g_m and g_d can be obtained by differentiating $I_D(V_G, V_D)$. Note that, in our simple model, short-channel effects have not been included; we would therefore obtain $g_d = 0\,\mho$ in saturation. However, a real device would show a small increase in I_D with an increase in V_D in saturation, giving rise to a non-zero g_d.
- The capacitances C_{gs} and C_{gd} are depletion capacitances of the *p*-*n* junction.