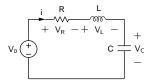


#### M. B. Patil

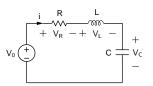
mbpatil@ee.iitb.ac.in
www.ee.iitb.ac.in/~sequel

Department of Electrical Engineering Indian Institute of Technology Bombay

イロト イロト イヨト イヨ

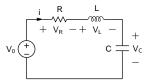






KVL:  $V_R + V_L + V_C = V_0 \Rightarrow i R + L \frac{di}{dt} + \frac{1}{C} \int i dt = V_0$ 



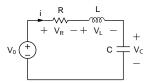


KVL: 
$$V_R + V_L + V_C = V_0 \Rightarrow i R + L \frac{di}{dt} + \frac{1}{C} \int i dt = V_0$$

Differentiating w. r. t. t, we get,

$$R\frac{di}{dt} + L\frac{d^2i}{dt^2} + \frac{1}{C}i = 0.$$

M. B. Patil, IIT Bombay



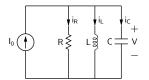
KVL: 
$$V_R + V_L + V_C = V_0 \Rightarrow iR + L\frac{di}{dt} + \frac{1}{C}\int i\,dt = V_0$$

Differentiating w. r. t. t, we get,

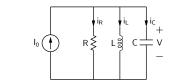
$$R \frac{di}{dt} + L \frac{d^2i}{dt^2} + \frac{1}{C}i = 0.$$
  
i.e., 
$$\frac{d^2i}{dt^2} + \frac{R}{L}\frac{di}{dt} + \frac{1}{LC}i = 0.$$

a second-order ODE with constant coefficients.

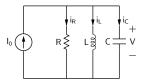
M. B. Patil, IIT Bombay







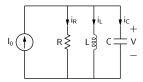
KCL: 
$$i_R + i_L + i_C = I_0 \Rightarrow \frac{1}{R} V + \frac{1}{L} \int V dt + C \frac{dV}{dt} = I_0$$



KCL: 
$$i_R + i_L + i_C = I_0 \Rightarrow \frac{1}{R}V + \frac{1}{L}\int V dt + C \frac{dV}{dt} = I_0$$

Differentiating w. r. t. t, we get,

$$\frac{1}{R}\frac{dV}{dt} + \frac{1}{L}V + C\frac{d^2V}{dt^2} = 0.$$



KCL: 
$$i_R + i_L + i_C = I_0 \Rightarrow \frac{1}{R} V + \frac{1}{L} \int V dt + C \frac{dV}{dt} = I_0$$

Differentiating w. r. t. t, we get,

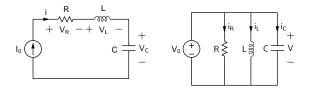
$$\frac{1}{R}\frac{dV}{dt} + \frac{1}{L}V + C\frac{d^2V}{dt^2} = 0.$$
  
i.e.,  $\frac{d^2V}{dt^2} + \frac{1}{RC}\frac{dV}{dt} + \frac{1}{LC}V = 0$ 

a second-order ODE with constant coefficients.

(≧▶ ≧ ∽) Q (? M. B. Patil, IIT Bombay

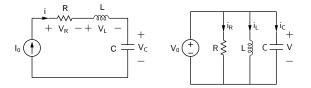
・ロト ・回 ト ・ヨト ・ヨト

# Series/Parallel RLC circuits



< □ > < 部 > < 書 > < 書 > こ 少 < C M. B. Patil, IIT Bombay

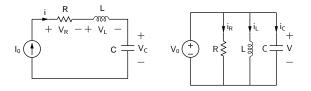
# Series/Parallel RLC circuits



\* A series RLC circuit driven by a constant current source is trivial to analyze.



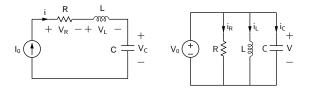
# Series/Parallel RLC circuits



\* A series RLC circuit driven by a constant current source is trivial to analyze. Since the current through each element is known, the voltage can be found in a straightforward manner.

・ロト ・日下・ ・ ヨト

$$V_R = i R, V_L = L \frac{di}{dt}, V_C = \frac{1}{C} \int i dt.$$

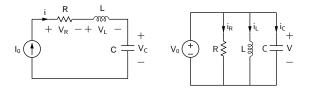


\* A series RLC circuit driven by a constant current source is trivial to analyze. Since the current through each element is known, the voltage can be found in a straightforward manner.

$$V_R = i R, \ V_L = L \frac{di}{dt}, \ V_C = \frac{1}{C} \int i \, dt$$

\* A parallel RLC circuit driven by a constant voltage source is trivial to analyze.

・ロト ・回ト ・ヨト



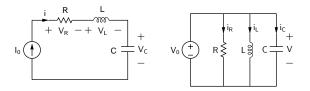
\* A series RLC circuit driven by a constant current source is trivial to analyze. Since the current through each element is known, the voltage can be found in a straightforward manner.

$$V_R = i R, V_L = L \frac{di}{dt}, V_C = \frac{1}{C} \int i dt.$$

\* A parallel RLC circuit driven by a constant voltage source is trivial to analyze. Since the voltage across each element is known, the current can be found in a straightforward manner.

・ロト ・回ト ・ヨト

$$i_R = V/R, \ i_C = C \frac{dV}{dt}, \ i_L = \frac{1}{L} \int V \, dt \, .$$



\* A series RLC circuit driven by a constant current source is trivial to analyze. Since the current through each element is known, the voltage can be found in a straightforward manner.

$$V_R = i R, V_L = L \frac{di}{dt}, V_C = \frac{1}{C} \int i dt.$$

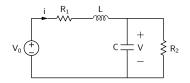
\* A parallel RLC circuit driven by a constant voltage source is trivial to analyze. Since the voltage across each element is known, the current can be found in a straightforward manner.

$$i_R = V/R, \ i_C = C \frac{dV}{dt}, \ i_L = \frac{1}{L} \int V dt$$

\* The above equations hold even if the applied voltage or current is not constant, and the variables of interest can still be easily obtained without solving a differential equation.

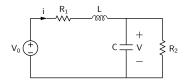
イロト イヨト イヨト イヨト





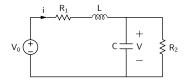


・ロト ・日下・ ・ ヨト



$$V_0 = R_1 i + L \frac{di}{dt} + V$$
(1)  
$$i = C \frac{dV}{dt} + \frac{1}{R_2} V$$
(2)

・ロト ・日下・ ・ ヨト



$$V_0 = R_1 i + L \frac{di}{dt} + V \tag{1}$$

$$i = C \frac{dV}{dt} + \frac{1}{R_2} V \tag{2}$$

・ロト ・日下・ ・ ヨト

Substituting (2) in (1), we get

$$V_0 = R_1 \left[ CV' + V/R_2 \right] + L \left[ CV'' + V'/R_2 \right] + V, \qquad (3)$$

$$V''[LC] + V'[R_1C + L/R_2] + V[1 + R_1/R_2] = V_0.$$
(4)

$$\frac{d^2y}{dt^2} + a \frac{dy}{dt} + b y = K \text{ (constant)}.$$



$$\frac{d^2y}{dt^2} + a \frac{dy}{dt} + b y = K \text{ (constant)}.$$

The general solution y(t) can be written as,

$$y(t) = y^{(h)}(t) + y^{(p)}(t)$$

where  $y^{(h)}(t)$  is the solution of the homogeneous equation,

$$\frac{d^2y}{dt^2} + a\frac{dy}{dt} + by = 0$$

and  $y^{(p)}(t)$  is a particular solution.

< □ > < 部 > < 書 > < 書 > こ き < つ < @ M. B. Patil, IIT Bombay

$$\frac{d^2y}{dt^2} + a \frac{dy}{dt} + b y = K \text{ (constant)}.$$

The general solution y(t) can be written as,

$$y(t) = y^{(h)}(t) + y^{(p)}(t)$$

where  $y^{(h)}(t)$  is the solution of the homogeneous equation,

$$\frac{d^2y}{dt^2} + a\frac{dy}{dt} + by = 0$$

and  $y^{(p)}(t)$  is a particular solution.

Since K = constant, a particular solution is simply  $y^{(p)}(t) = K/b$ .

M. B. Patil, IIT Bombay

・ロン ・四 と ・ 正 と ・ 正 と

$$\frac{d^2y}{dt^2} + a \frac{dy}{dt} + b y = K \text{ (constant)}.$$

The general solution y(t) can be written as,

$$y(t) = y^{(h)}(t) + y^{(p)}(t)$$

where  $y^{(h)}(t)$  is the solution of the homogeneous equation,

$$\frac{d^2y}{dt^2} + a\frac{dy}{dt} + by = 0$$

and  $y^{(p)}(t)$  is a particular solution.

Since K = constant, a particular solution is simply  $y^{(p)}(t) = K/b$ .

In the context of *RLC* circuits,  $y^{(p)}(t)$  is the steady-state value of the variable of interest, i.e.,

$$y^{(p)} = \lim_{t \to \infty} y(t),$$

M. B. Patil, IIT Bombay

which can be often found by inspection.

$$\frac{d^2y}{dt^2} + a\frac{dy}{dt} + by = 0,$$

we first find the roots of the associated characteristic equation,

$$r^2 + a r + b = 0.$$

Let the roots be  $r_1$  and  $r_2$ . We have the following possibilities:



$$\frac{d^2y}{dt^2} + a\frac{dy}{dt} + by = 0,$$

we first find the roots of the associated characteristic equation,

$$r^2 + a r + b = 0.$$

Let the roots be  $r_1$  and  $r_2$ . We have the following possibilities:

\*  $r_1$ ,  $r_2$  are real,  $r_1 \neq r_2$  ("overdamped")  $y^{(h)}(t) = C_1 \exp(r_1 t) + C_2 \exp(r_2 t)$ .

$$\frac{d^2y}{dt^2} + a\frac{dy}{dt} + by = 0$$

we first find the roots of the associated characteristic equation,

$$r^2 + a r + b = 0.$$

Let the roots be  $r_1$  and  $r_2$ . We have the following possibilities:

- \*  $r_1, r_2$  are real,  $r_1 \neq r_2$  ("overdamped")  $y^{(h)}(t) = C_1 \exp(r_1 t) + C_2 \exp(r_2 t)$ .
- \*  $r_1$ ,  $r_2$  are complex,  $r_{1,2} = \alpha \pm j\omega$  ("underdamped")  $y^{(h)}(t) = \exp(\alpha t) [C_1 \cos(\omega t) + C_2 \sin(\omega t)].$

M. B. Patil, IIT Bombay

・ロト ・回 ト ・ヨト ・ヨト

$$\frac{d^2y}{dt^2} + a\frac{dy}{dt} + by = 0$$

we first find the roots of the associated characteristic equation,

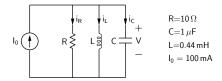
$$r^2 + ar + b = 0.$$

・ロト ・ 日 ・ ・ ヨ ・ ・ ヨ ・ ・

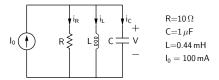
M. B. Patil, IIT Bombay

Let the roots be  $r_1$  and  $r_2$ . We have the following possibilities:

- \*  $r_1, r_2$  are real,  $r_1 \neq r_2$  ("overdamped")  $y^{(h)}(t) = C_1 \exp(r_1 t) + C_2 \exp(r_2 t)$ .
- \*  $r_1$ ,  $r_2$  are complex,  $r_{1,2} = \alpha \pm j\omega$  ("underdamped")  $y^{(h)}(t) = \exp(\alpha t) [C_1 \cos(\omega t) + C_2 \sin(\omega t)].$
- \*  $r_1 = r_2 = \alpha$  ("critically damped")  $y^{(h)}(t) = \exp(\alpha t) [C_1 t + C_2].$



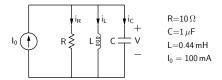




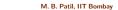
$$i_L(0^-) = 0 A \Rightarrow i_L(0^+) = 0 A.$$
  

$$V(0^-) = 0 V \Rightarrow V(0^+) = 0 V.$$

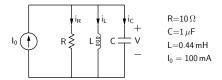
(■) ■ ∽ののC M. B. Patil, IIT Bombay



$$\begin{split} i_L(0^-) &= 0 \ A \Rightarrow i_L(0^+) = 0 \ A. \\ V(0^-) &= 0 \ V \Rightarrow V(0^+) = 0 \ V. \\ \frac{d^2 V}{dt^2} + \frac{1}{RC} \ \frac{dV}{dt} + \frac{1}{LC} \ V = 0 \ \text{ (as derived earlier)} \end{split}$$



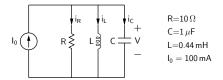
E



$$\begin{split} i_L(0^-) &= 0 \ A \Rightarrow i_L(0^+) = 0 \ A. \\ V(0^-) &= 0 \ V \Rightarrow V(0^+) = 0 \ V. \\ \frac{d^2 V}{dt^2} + \frac{1}{RC} \ \frac{dV}{dt} + \frac{1}{LC} \ V = 0 \ \text{ (as derived earlier)} \\ \end{split}$$
The roots of the characteristic equation are (show this):

 $r_1 = -0.65 imes 10^5 \, s^{-1}$  ,  $r_2 = -0.35 imes 10^5 \, s^{-1}$  .

M. B. Patil, IIT Bombay



$$i_{L}(0^{-}) = 0 A \Rightarrow i_{L}(0^{+}) = 0 A.$$

$$V(0^{-}) = 0 V \Rightarrow V(0^{+}) = 0 V.$$

$$\frac{d^{2}V}{dt^{2}} + \frac{1}{RC} \frac{dV}{dt} + \frac{1}{LC} V = 0 \text{ (as derived earlier)}$$

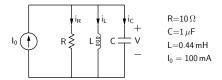
The roots of the characteristic equation are (show this):

$$r_1 = -0.65 imes 10^5 \, s^{-1}$$
 ,  $r_2 = -0.35 imes 10^5 \, s^{-1}$  .

The general expression for V(t) is,  $V(t) = A \exp(r_1 t) + B \exp(r_2 t) + V(\infty)$ ,

M. B. Patil, IIT Bombay

(ロ) (四) (目) (日) (日)



・ロン ・部 と ・ ヨ と ・ ヨ と

M. B. Patil, IIT Bombay

$$\begin{split} i_L(0^-) &= 0 A \Rightarrow i_L(0^+) = 0 A. \\ V(0^-) &= 0 V \Rightarrow V(0^+) = 0 V. \\ \frac{d^2 V}{dt^2} + \frac{1}{RC} \frac{dV}{dt} + \frac{1}{LC} V = 0 \quad \text{(as derived earlier)} \end{split}$$

The roots of the characteristic equation are (show this):

$$r_1 = -0.65 imes 10^5 \, s^{-1}$$
 ,  $r_2 = -0.35 imes 10^5 \, s^{-1}$  .

The general expression for V(t) is,  $V(t) = A \exp(r_1 t) + B \exp(r_2 t) + V(\infty)$ , i.e.,  $V(t) = A \exp(-t/\tau_1) + B \exp(-t/\tau_2) + V(\infty)$ , where  $\tau_1 = -1/r_1 = 15.4 \,\mu s$ ,  $\tau_2 = -1/r_1 = 28.6 \,\mu s$ .

As 
$$t \to \infty$$
,  $V = L \frac{di_L}{dt} = 0$   $V \Rightarrow V(\infty) = 0$   $V$ .

▲□▶ ▲□▶ ▲□▶ ▲□▶ ▲□▶ ▲□

As 
$$t \to \infty$$
,  $V = L \frac{di_L}{dt} = 0$   $V \Rightarrow V(\infty) = 0$   $V$ .  
 $\Rightarrow V(t) = A \exp(-t/\tau_1) + B \exp(-t/\tau_2)$ ,

▲□▶ ▲□▶ ▲□▶ ▲□▶ ▲□▶ ▲□

As 
$$t \to \infty$$
,  $V = L \frac{di_L}{dt} = 0 V \Rightarrow V(\infty) = 0 V$ .  
 $\Rightarrow V(t) = A \exp(-t/\tau_1) + B \exp(-t/\tau_2)$ ,

Since  $V(0^+) = 0$  V, we have,

$$A+B=0. (1)$$

< □ > < 部 > < 臣 > < 臣 > < 臣 > ○ < ↔ M. B. Patil, IIT Bombay

As 
$$t \to \infty$$
,  $V = L \frac{di_L}{dt} = 0$   $V \Rightarrow V(\infty) = 0$   $V$ .  
 $\Rightarrow V(t) = A \exp(-t/\tau_1) + B \exp(-t/\tau_2)$ ,  
Since  $V(0^+) = 0$   $V$ , we have,  
 $A + B = 0$ . (1)

Our other initial condition is  $i_L(0^+) = 0$  A, which can be used to obtain  $\frac{dV}{dt}(0^+)$ .



As 
$$t \to \infty$$
,  $V = L \frac{di_L}{dt} = 0 V \Rightarrow V(\infty) = 0 V$ .  
 $\Rightarrow V(t) = A \exp(-t/\tau_1) + B \exp(-t/\tau_2)$ ,  
Since  $V(0^+) = 0 V$ , we have,  
 $A + B = 0$ . (1)

Our other initial condition is  $i_L(0^+) = 0$  A, which can be used to obtain  $\frac{dV}{dt}(0^+)$ .  $i_L(0^+) = I_0 - \frac{1}{R} V(0^+) - C \frac{dV}{dt}(0^+) = 0$  A, which gives



As  $t \to \infty$ ,  $V = L \frac{di_L}{dt} = 0$   $V \Rightarrow V(\infty) = 0$  V.  $\Rightarrow V(t) = A \exp(-t/\tau_1) + B \exp(-t/\tau_2)$ , Since  $V(0^+) = 0$  V, we have, A + B = 0. (1) Our other initial condition is  $i_L(0^+) = 0$  A, which can be used to obtain  $\frac{dV}{dt}(0^+)$ .  $i_L(0^+) = I_0 - \frac{1}{R} V(0^+) - C \frac{dV}{dt}(0^+) = 0$  A, which gives

 $(A/\tau_1) + (B/\tau_2) = -I_0/C.$  (2)



As  $t \to \infty$ ,  $V = L \frac{di_L}{dt} = 0$   $V \Rightarrow V(\infty) = 0$  V.  $\Rightarrow V(t) = A \exp(-t/\tau_1) + B \exp(-t/\tau_2)$ , Since  $V(0^+) = 0$  V, we have, A + B = 0. (1)

Our other initial condition is  $i_{L}(0^{+}) = 0$  A, which can be used to obtain  $\frac{dV}{dt}(0^{+})$ .  $i_{L}(0^{+}) = I_{0} - \frac{1}{R} V(0^{+}) - C \frac{dV}{dt}(0^{+}) = 0$  A, which gives  $(A/\tau_{1}) + (B/\tau_{2}) = -I_{0}/C.$  (2)

From (1) and (2), we get the values of A and B, and

$$V(t) = -3.3 \left[ \exp(-t/\tau_1) - \exp(-t/\tau_2) \right] V.$$
(3)

(SEQUEL file: ee101\_rlc\_1.sqproj)

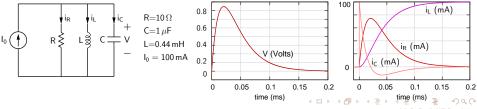
As  $t \to \infty$ ,  $V = L \frac{di_L}{dt} = 0$   $V \Rightarrow V(\infty) = 0$  V.  $\Rightarrow V(t) = A \exp(-t/\tau_1) + B \exp(-t/\tau_2)$ , Since  $V(0^+) = 0$  V, we have, A + B = 0.

Our other initial condition is  $i_L(0^+) = 0$  A, which can be used to obtain  $\frac{dV}{dt}(0^+)$ .  $i_L(0^+) = I_0 - \frac{1}{R} V(0^+) - C \frac{dV}{dt}(0^+) = 0$  A, which gives  $(A/\tau_1) + (B/\tau_2) = -I_0/C.$  (2)

From (1) and (2), we get the values of A and B, and

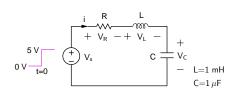
$$V(t) = -3.3 \left[ \exp(-t/\tau_1) - \exp(-t/\tau_2) \right] V.$$
(3)

(SEQUEL file: ee101\_rlc\_1.sqproj)

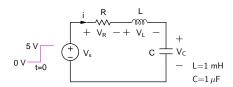


M. B. Patil, IIT Bombay

(1)

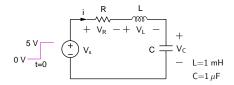






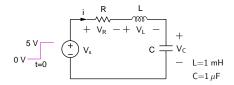
(a) Show that the condition for critically damped response is  $R = 63.2 \Omega$ .





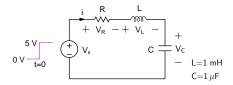
- (a) Show that the condition for critically damped response is  $R = 63.2 \Omega$ .
- (b) For  $R = 20 \Omega$ , derive expressions for i(t) and  $V_L(t)$  for t > 0 (Assume that  $V_C(0^-) = 0 V$  and  $i_L(0^-) = 0 A$ ). Plot them versus time.

< □ > < @ > < 注 > < 注 > ... 注

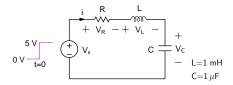


- (a) Show that the condition for critically damped response is  $R = 63.2 \Omega$ .
- (b) For  $R = 20 \Omega$ , derive expressions for i(t) and  $V_L(t)$  for t > 0 (Assume that  $V_C(0^-) = 0 V$  and  $i_L(0^-) = 0 A$ ). Plot them versus time.
- (c) Repeat (b) for  $R = 100 \Omega$ .





- (a) Show that the condition for critically damped response is  $R = 63.2 \Omega$ .
- (b) For  $R = 20 \Omega$ , derive expressions for i(t) and  $V_L(t)$  for t > 0 (Assume that  $V_C(0^-) = 0 V$  and  $i_L(0^-) = 0 A$ ). Plot them versus time.
- (c) Repeat (b) for  $R = 100 \Omega$ .
- (d) Compare your results with the following plots. (SEQUEL file: ee101\_rlc\_2.sqproj)



- (a) Show that the condition for critically damped response is  $R = 63.2 \Omega$ .
- (b) For  $R = 20 \Omega$ , derive expressions for i(t) and  $V_L(t)$  for t > 0 (Assume that  $V_C(0^-) = 0 V$  and  $i_L(0^-) = 0 A$ ). Plot them versus time.
- (c) Repeat (b) for  $R = 100 \Omega$ .
- (d) Compare your results with the following plots. (SEQUEL file: ee101\_rlc\_2.sqproj)

