

Tutorial sheet 5, EE302-S1, 11th March 2025.

Q-1: Consider $G(s) = \frac{ds+b}{s+a}$, $d \neq 0$.

- (a) Find the underlying differential equation between u & y .
 (b) Rewrite $y(t) = y_1(t) + y_2(t)$ such that the input $u(t)$ would not need to be differentiated. (Get $G(s) = \frac{d}{s+a} + G_2(s)$ Hint. constant strictly proper.)
 (c) Conclude that (more generally), for proper, transfer function, one never needs to differentiate input. (Solve for real distinct roots of $d(s)$ with $G(s) = \frac{n(s)}{d(s)}$.)

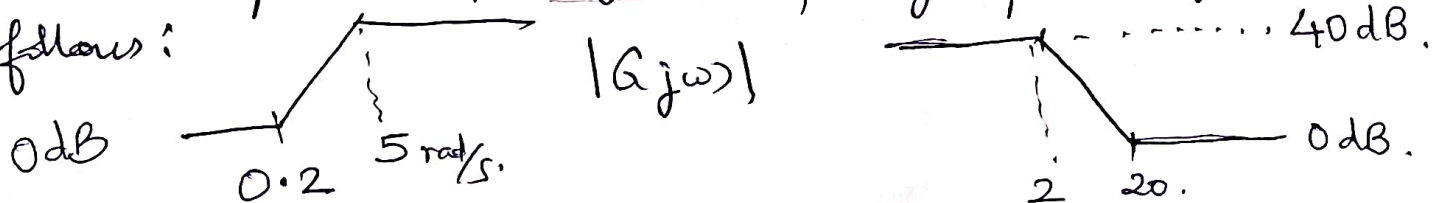
Q-2: Consider $G(s) = \frac{1}{s+3}$ with standard negative unity feedback configuration but with k increasing from $-\infty$ to 0 . Draw root locus.

- (b) Draw: complete root locus $-\infty \rightarrow 0 \rightarrow +\infty$.
 (c) Guess/get rules for $k < 0$ (for strictly proper G & biproper G).
 (d) Consider cases: $k < 0$, $k > 0$, and -ve feedback & +ve feedback, and $G(s) = \frac{n(s)}{d(s)}$: leading coefficients of n, d : same sign / opposite sign. Explain why we have not 2³ but just 2 cases to study for closed loop pole locus.

Q-3: Draw asymptotic Bode plot for $\frac{1}{s+1}$,

$\frac{1}{(s+1)(s+2)}$: Both phase & magnitude.

Q-4: Design low pass filter & high pass filter as follows:



Q-5 (a) Verify that $\sin \omega t$ input gives output $|G(j\omega)| \sin(\omega t + ?)$

(Verify using linearity & consider complex valued signals $e^{j\omega t}$.)
(b) What about $\cos \omega t$ input?

Q-6: If relative degree of a $G(s) = 0$, can G be low-pass? high-pass?

(Q-7) If $G(s)$ is high-pass, can $G(s)$ be relative degree = 1 or 2, ...? What should relative degree be?

Q-8: If magnitude plot is given, (like in Q-4), how much non-uniqueness is possible in $G(s)$? (Answer for both magnitude plots.)

Q-9: Consider  (a) Find impedance $Z(s)$ of this circuit.

(b) For one period, find active power absorbed by the circuit. (get $\int_0^T v(z) i(z) dz$ for $T = \frac{2\pi}{\omega}$.)

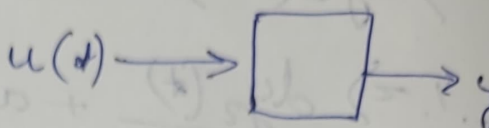
(c) Relate active power w.r.t. $\operatorname{Re}(Z(j\omega))$

Q-10: Plot complete root locus ($k: -\infty \rightarrow +\infty$)

for $G(s) = \frac{1}{(s+1)(s+2)(s+3)}$, $\frac{1}{(s+1)(s+2)}$, $\frac{s}{s^2 + \omega^2}$

Tutorial-4

Q1: a) $G(s) = \frac{ds+b}{s+a}$, $d \neq 0$

$$\frac{y(s)}{u(s)} = \frac{ds+b}{s+a}$$


$$\Rightarrow sy(s) + ay(s) = dsu(s) + bu(s)$$

~~Q~~ Taking inverse Laplace:

$$\frac{dy}{dt} + ay = d \frac{du}{dt} + bu$$

$$\begin{aligned} \text{(b)} \quad G(s) &= \frac{ds+b}{s+a} = \frac{ds+da-da+b}{s+a} \\ &= d \frac{(s+a)}{(s+a)} + \frac{b-da}{s+a} \\ &= d + \frac{b-da}{s+a} \end{aligned}$$

$$\Rightarrow \frac{y(s)}{u(s)} = d + \frac{b-da}{s+a}$$

Taking inverse Laplace after rearranging $G(s)$

$$y(s) = \underbrace{du(s)}_{y_1(s)} + \underbrace{\left(\frac{b-da}{s+a}\right)u(s)}_{y_2(s)}$$

$$y_1(s) = du(s) \xrightarrow{\text{I.L.T.}} y_1(t) = du(t)$$

$$y_2(s) = \left(\frac{b-da}{s+a} \right) u(s)$$

$$\Rightarrow y_2(s)(s+a) = (b-da)u(s)$$

$$\text{I.L.T.} \Rightarrow \frac{dy_2(t)}{dt} + ay(t) = (b-da)u(t)$$

(C) Suppose we have $G(s) = \frac{N(s)}{D(s)}$ where $\text{degree}(N(s)) \leq \text{degree}(D(s))$ then we can perform partial fraction expansion (decomposition) as:

$$G(s) = \frac{N(s)}{D(s)} = k + \frac{C_1}{s+p_1} + \dots + \frac{C_n}{s+p_n}$$

$$\Rightarrow \frac{y(s)}{u(s)} = k + \frac{C_1}{s+p_1} + \dots + \frac{C_n}{s+p_n}$$

and each term will correspond to its respective

$$y_i(s)(s+p_i) = C_i u(s)$$

$$\text{I.L.T.} \Rightarrow \frac{dy_i(t)}{dt} + p_i y_i(t) = C_i u(t)$$

$$\text{and } y(t) = k u(t) + \sum_{i=1}^n y_i$$

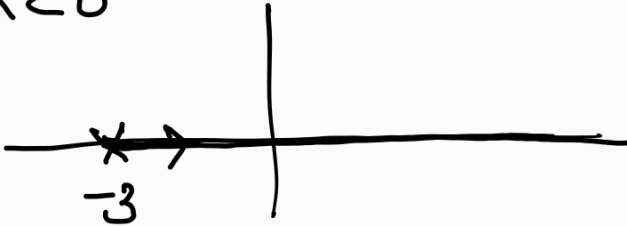
None of this analysis involved derivative of $u(t)$

Q2) $G(s) = \frac{1}{s+3}$

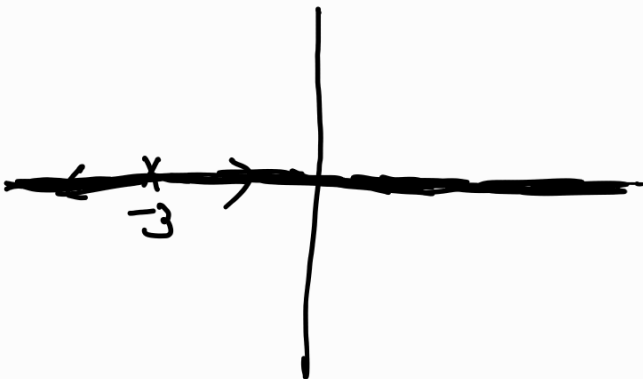
$1 + KGH$

$1 + \frac{K}{s+3} = 0 \quad s+3+k=0 \Rightarrow s = -(3+k)$

(a) $K < 0$



b) $K \in \mathbb{R}$



c) $K < 0$

- i) A point on the real axis lies on the root locus if the total number of poles & zeroes to the right of it is even.
- ii) No. of branches of the RL equals no. of open poles.
- iii) RL starts at $k=0$ & ends at open-loop zeroes ($k = -\infty$)
- iv) Angle of asymptotes = $\frac{2n\pi}{\text{Poles} - \text{Zeroes}}$

d) $1 + GH = 0$ (-ve unity feedback)

$K > 0 \rightarrow$ Direct Root Locus

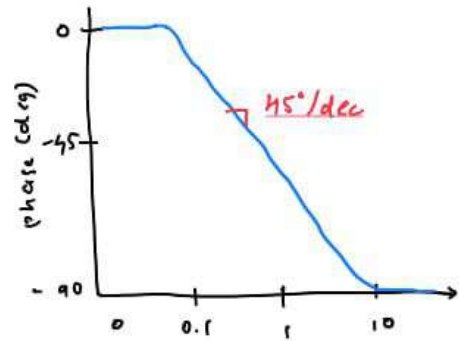
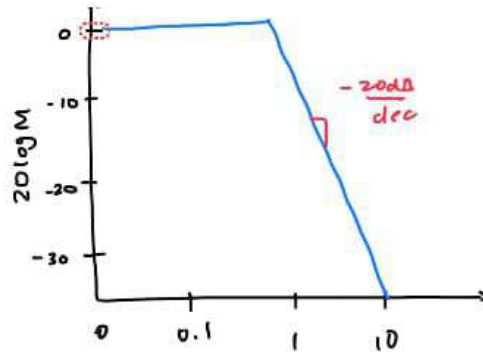
$K < 0 \rightarrow$ Inverse RL

the Unity feedback $\begin{cases} K > 0 & \text{IRL} \\ K < 0 & \text{DRL} \end{cases}$

So, to study closed loop pole locus, Only 2 cases are

enough. $\begin{matrix} \text{-ve unity, } K > 0 \\ \text{+ve unity, } K < 0 \end{matrix} \} \text{DRL} \quad \begin{matrix} \text{+ve unity, } K > 0 \\ \text{-ve unity, } K < 0 \end{matrix} \} \text{IRL}$

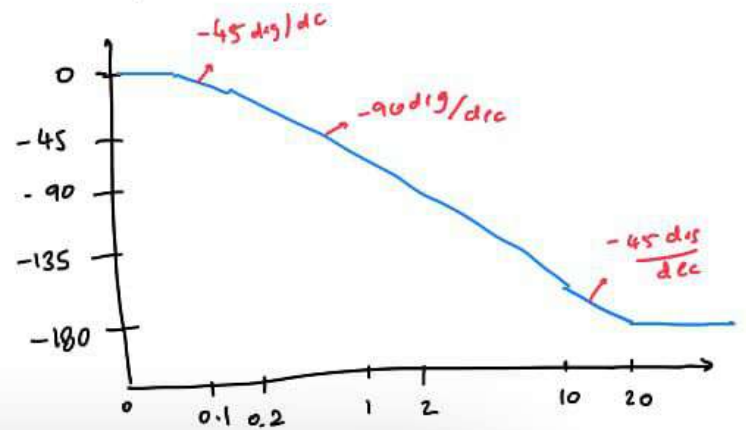
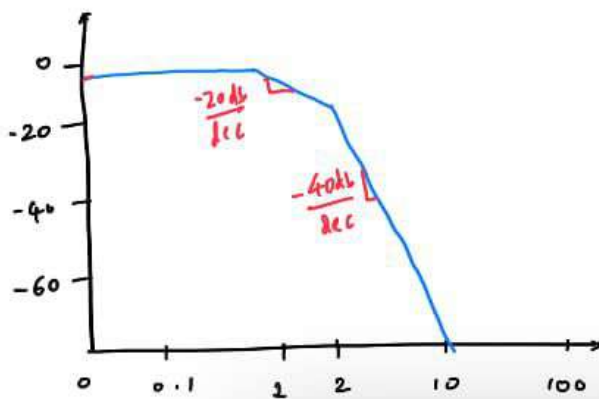
→ $\frac{1}{s+1}$



→ $\frac{1}{(s+1)(s+2)}$

	Freq.	
	1	2
pole at -1	-20	-20
pole at -2	0	-20
	-20	-40

	Freq.			
	0.1	0.2	10	20
pole at -1	-45	-45	0	0
pole at -2	0	-45	-45	0
	-45	-90	-45	0

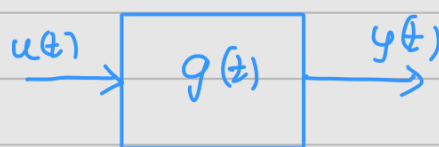


Tut 4 Q5

$$a) \sin \omega t = \frac{e^{j\omega t} - e^{-j\omega t}}{2j}$$

Let $u(t) = \sin \omega t$ and $g(t)$ be transfer function

$$\therefore y(t) = u(t) * g(t)$$



$$= \sin \omega t * g(t)$$

$$= \frac{e^{j\omega t} - e^{-j\omega t}}{2j} * g(t)$$

By using linearity property of convolution.

$$y(t) = \frac{1}{2j} (e^{j\omega t} * g(t) - e^{-j\omega t} * g(t))$$

But we know that when input is exponential signal, the o/p follows

$$y(t) = e^{j\omega t} * g(t); y(t) = |G(j\omega)| e^{j(\omega t + \angle \phi)} \quad \text{where } \phi = \angle G(j\omega)$$

$\therefore$ Using this property, we can write.

$$y(t) = \frac{1}{2j} (|G(j\omega)| e^{j(\omega t + \angle \phi)} - |G(j\omega)| e^{-j(\omega t + \angle \phi)})$$

$$\therefore y(t) = |G(j\omega)| \left(\frac{e^{j(\omega t + \angle \phi)} - e^{-j(\omega t + \angle \phi)}}{2j} \right)$$

$$y(t) = |G(j\omega)| \sin(\omega t + \angle \phi) \quad \text{where } \phi = \angle G(j\omega)$$

Consider $\cos \omega t = \frac{e^{j\omega t} + e^{-j\omega t}}{2}$ and do same analysis.

Q6) If relative degree is 0, by Bode magnitude plots, we can say that the magnitude at higher frequencies doesn't decay. So, Transfer function cannot certainly be a LPF.

$$G(s) = \frac{a_0 s^0 + a_1 s^{-1} + \dots + a_n}{b_0 s^0 + b_1 s^{-1} + \dots + b_n}$$

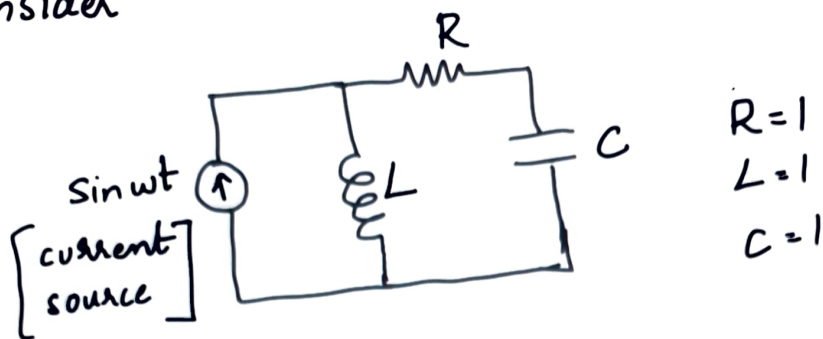
As $\omega \rightarrow 0$, magnitude of $G(s) \rightarrow a_n/b_n$ & as $\omega \rightarrow \infty$, $\text{mag} \rightarrow \frac{a_0}{b_0}$. It can be a Band pass / stop filter.

$\Rightarrow$ Zeros at $s=0$ force the gain to rise at low frequencies, creating HPF characteristics.

Eg: $\frac{s}{s+a}$, $\frac{s^2}{s^2+\dots}$

Q7) If $G(s)$ is a HPF, it should attenuate the low frequencies and pass the high f . If the relative degree is 1 or 2, then by Bode Magnitude plots at high f there is a decay in magnitude response. So, if $G(s)$ is HPF, its relative degree cannot be 1 or 2, it should be equal to zero.

Q9: Consider



a) Find impedance $Z(s)$ of the circuit.

$$Z(s) = \frac{Ls \left[R + \frac{1}{Cs} \right]}{Ls + \left(R + \frac{1}{Cs} \right)} = \frac{s(s+1)}{s^2 + s + 1}$$

b) For one period find active power absorbed by circuit.

$$\int_0^T v(t) i(t) dt =$$

$$Z(j\omega) = \frac{j\omega [j\omega + 1]}{(j\omega)^2 + j\omega + 1} = \frac{-\omega^2 + j\omega}{(1 - \omega^2) + j\omega} = \frac{\omega^4 + \omega j}{1 - \omega^2 + \omega^4}$$

$$Z = Z_0 \angle \phi$$

$$V = IZ = Z_0 \sin(\omega t - \phi)$$

$$P_{act} = \int_0^T Z_0 \sin(\omega t - \phi) \sin \omega t dt, \quad T = \frac{2\pi}{\omega}$$

expanding $\sin(\omega t - \phi) = \sin \omega t \cos \phi - \cos \omega t \sin \phi$

$$P_{act} = \int_0^T Z_0 \sin^2 \omega t \cos \phi dt - \int_0^T Z_0 \sin \omega t \cos \omega t \sin \phi dt$$

$$\Rightarrow \frac{Z_0 \cos \phi}{2} \int_0^T (1 - \cos 2\omega t) dt - \frac{Z_0 \sin \phi}{2} \int_0^T \sin 2\omega t dt$$

$$\Rightarrow \frac{Z_0 \cos \phi}{2} \left[t - \frac{\sin 2\omega t}{2\omega} \right]_0^T - \frac{Z_0 \sin \phi}{2} \left[-\frac{\cos 2\omega t}{2\omega} \right]_0^T$$

$$\Rightarrow \frac{Z_0 \cos \phi}{2} [T] - \frac{Z_0 \sin \phi}{2} \left[\frac{-1}{2\omega} (1-1) \right]$$

$$\Rightarrow \frac{Z_0 \cos \phi}{2}$$

∴ Relate active power w.r.t $\text{Re}[Z(j\omega)]$

$$P_{act} = \frac{Z_0 \cos \phi}{2} = \frac{\text{Re}[Z(j\omega)]}{2}$$

$$n(s) = \frac{1}{(s+1)(s+2)(s+3)}$$

angle of asymptote

$$= \frac{180(2q+1)}{p-z}$$

$$\left(\begin{array}{l} p = \text{no of poles} \\ z = \text{no of zeros} \end{array} \right)$$

$$= \frac{180(2q+1)}{3-0}$$

$$= 60(2q+1)$$

$$q = 0, 1, 2, \dots, |p|-|z|-1$$

$$= 0, 1, 2$$

$$= 60, 180, 300$$

$$\text{centroid} = \frac{\text{sum of poles} - \text{sum of zeros}}{p-z}$$

$$= \frac{(-1-2-3) - 0}{3}$$

$$= -2$$

Break-away and Break-in points:

$$k + (s+1)(s+2)(s+3) = 0$$

get the closed-loop transfer function and equate the denominator to 0.

$$\frac{dk}{ds} = 0$$

such s values will give you the break-away and break-in points

$$(s^2 + 3s + 2)(s+3) + k = 0$$

$$(s^2 + 3s + 2)(s+3) + k = 0$$

$$s^3 + 6s^2 + 11s + 6 + k = 0$$

$$s^3 + 6s^2 + 11s + 6 + k = 0$$

Imaginary axis crossing

Routh Table:

s^3	1	11
s^2	6	$6+k$
s^1	$60-k$	
s^0	6	

$$\rightarrow 60 - k = 0$$

$$k = 60$$

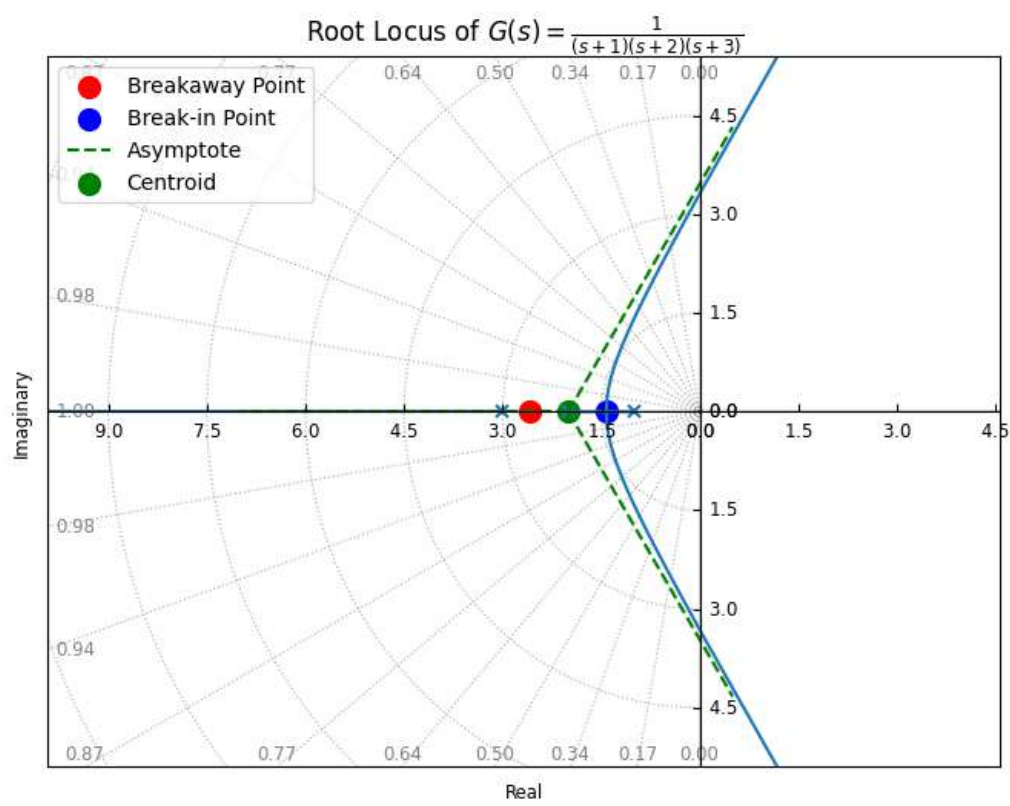
Auxiliary eq: $6s^2 + 6 + k = 0$

$$6s^2 + 66 = 0$$

$$s^2 = -11$$

$$s = \pm j\sqrt{11}$$

Root locus plot for sys[16]



$$\omega(8) = \frac{1}{(s+1)(s+2)}$$

Angle of asymptote

$$= \frac{180(2z+1)}{p-2}$$

$$= \frac{180(2z+1)}{2}$$

$$= 90(2z+1)$$

$$= 5+31 \text{ } z=8 \text{ } 2.50, 1, \text{ } p=2-1$$

$$\cancel{2.50}$$

$$p-2-1=1$$

$$\Rightarrow z \in \{0, 1\}$$

$$\Rightarrow 180(1), 180(3)$$

$$180, 540$$

$$\text{centroid} = \frac{\text{sum of poles} - \text{sum of zeros}}{p-2}$$

$$= \frac{-3}{2}$$

Break away / Break-in points:

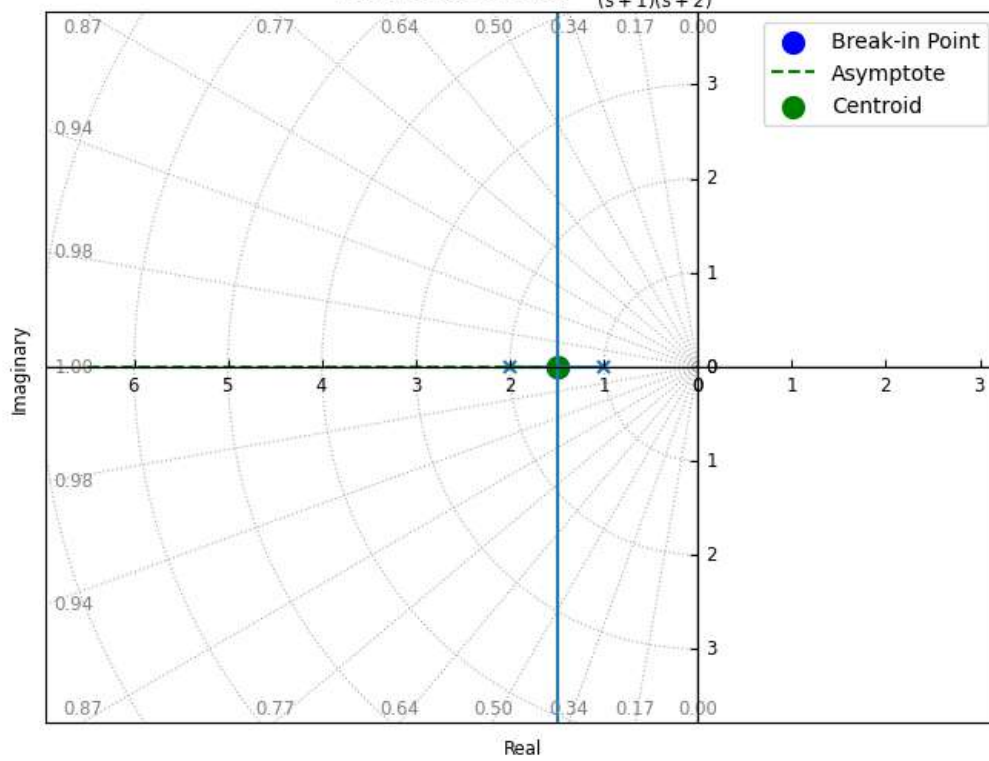
$$K + (s+1)(s+2) = 0$$

$$dK = 0$$

$$ds$$

Root locus plot for sys[18]

Root Locus of $G(s) = \frac{1}{(s+1)(s+2)}$



$$\phi(8) = \frac{8}{s^2 + \omega^2}$$

angle of asymptotes:

$$\theta = \frac{180(2z + 1)}{1p1 - 1z1}$$

$$= \frac{180(2z + 1)}{1}$$

$$= 180(2z + 1)$$

$$\Rightarrow 180$$

$$\text{Centroid} = \frac{+5\omega - 5\omega + 0}{1}$$

$$= 0$$

Break-away / Break-in points:

~~Root locus~~

~~Root locus~~

$$K \phi(s) = 0$$

$$1 + K \phi(s)$$

$$\frac{K 8}{s^2 + \omega^2}$$

$$\Rightarrow \frac{K 8}{s^2 + \omega^2}$$

$$\frac{4K 8}{s^2 + \omega^2}$$

8

~~solve~~ $ks + s^2 + \omega^2 = 0 \rightarrow$ denominator of CLTF

solve for $\frac{dk}{ds} = 0$

Imag. axis crossing:

RH Table =

s^2	1	ω^2
s^1	k	0

Auxiliary eq:

$$s^2 + \omega^2 = 0$$

$$s = \pm j\omega$$

~

Root locus plot for sys[21]

Root Locus of $G(s) = \frac{s}{s^2 + \omega^2}$ (Assuming $\omega = 1$)

