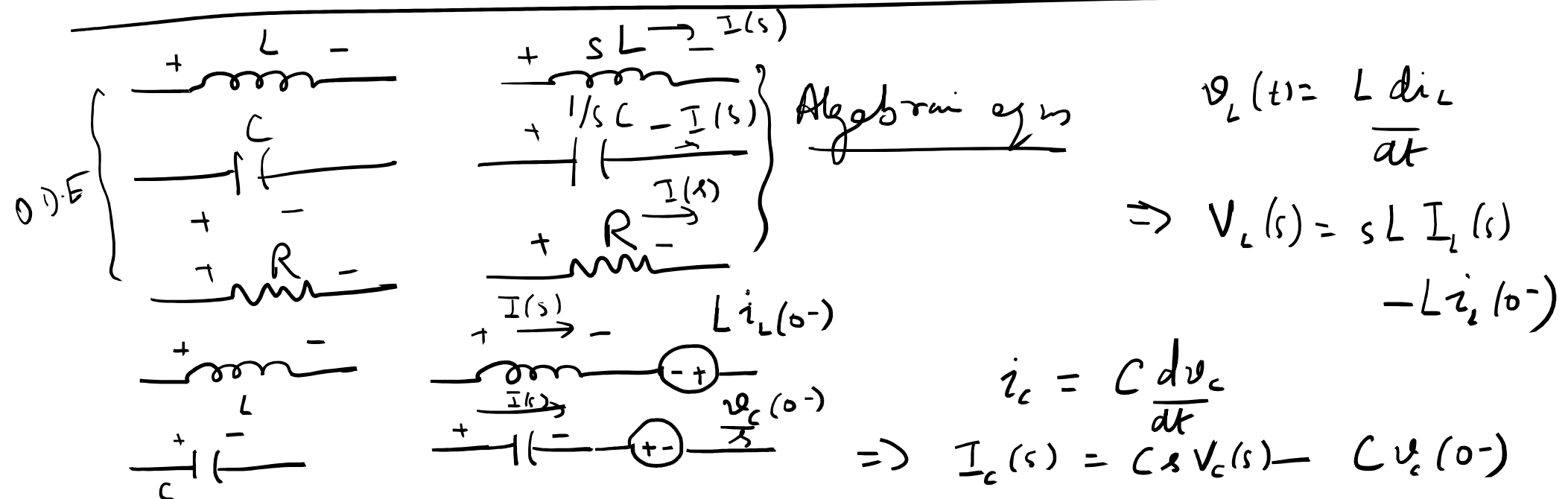
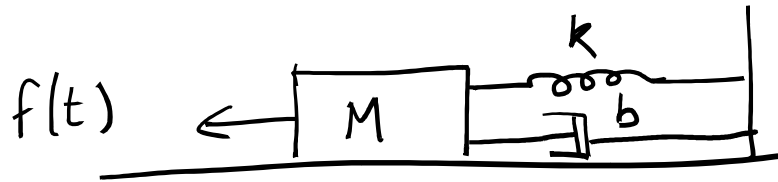


Lecture 3 Module 1

Modelling of mechanical systems

- translational dynamics
- rotational dynamics





$$M\ddot{x} + b\dot{x} + kx = f(t)$$

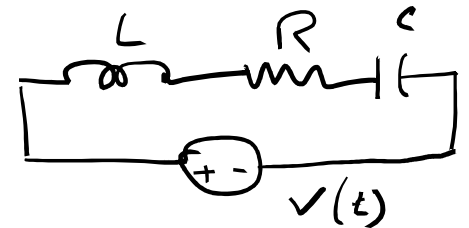
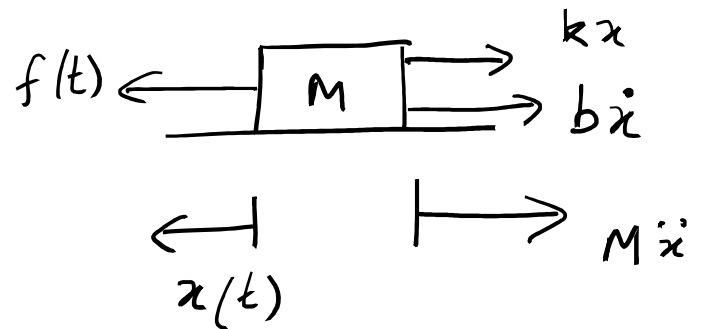
$$\Rightarrow (Ms^2 + bs + k)X(s) = F(s)$$



$$\Rightarrow \left(Ms + b + \frac{k}{s}\right) \underbrace{SX(s)}_{\substack{\text{L.T.} \\ \updownarrow \\ \text{velocity}}} = F(s)$$

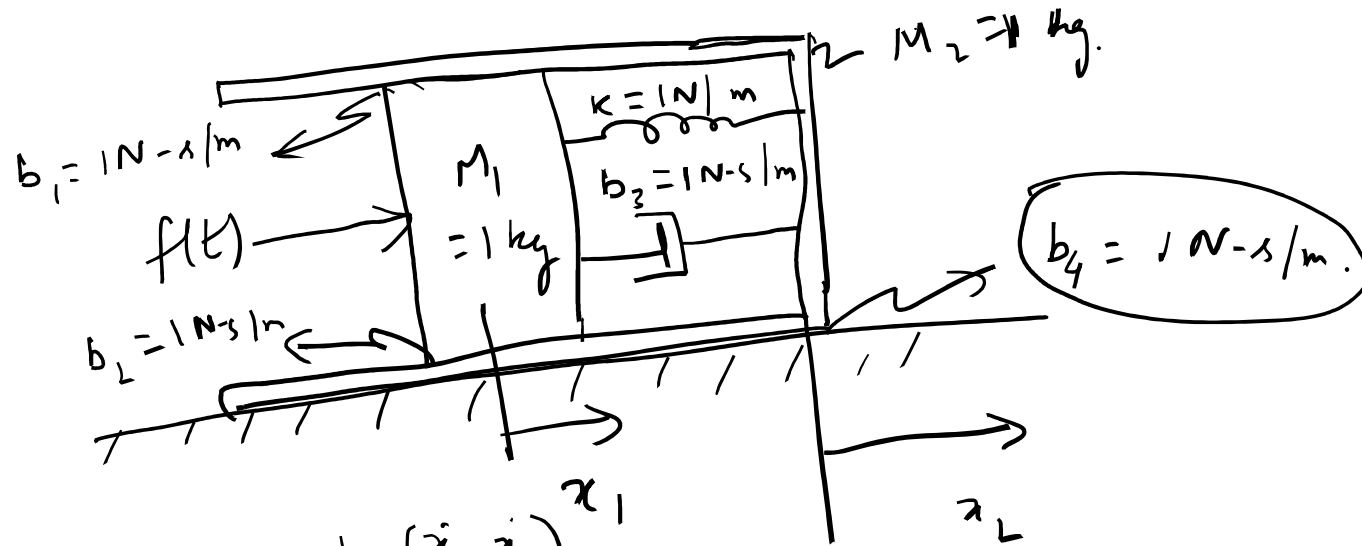
$$\left(Ls + R + \frac{1}{sC}\right) \underline{I(s)} = \underline{V(s)}$$

velocity



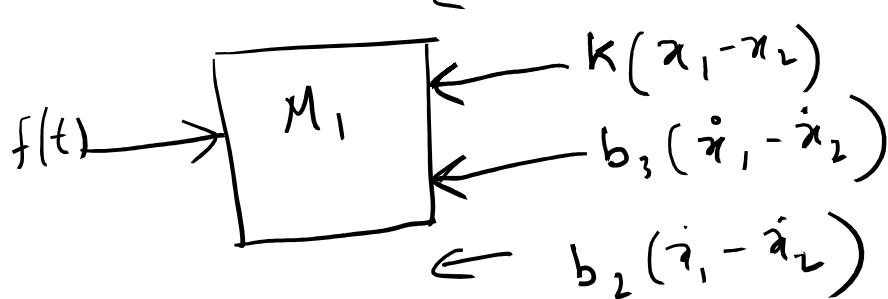
Series Analogy

$$\begin{aligned} k &\rightarrow \frac{1}{C} \\ R &\rightarrow b \\ L &\rightarrow M \end{aligned}$$



Goal:
obtain $\frac{x_2(s)}{F(s)}$
 $G(s) = \frac{x_2(s)}{F(s)}$

$b_4 = 1 \text{ N-s/m}$



$$F(s) = s^2 X_1(s) + 3s X_1(s) + X_1(s) - 3s X_2(s) - X_2(s) \quad (i)$$

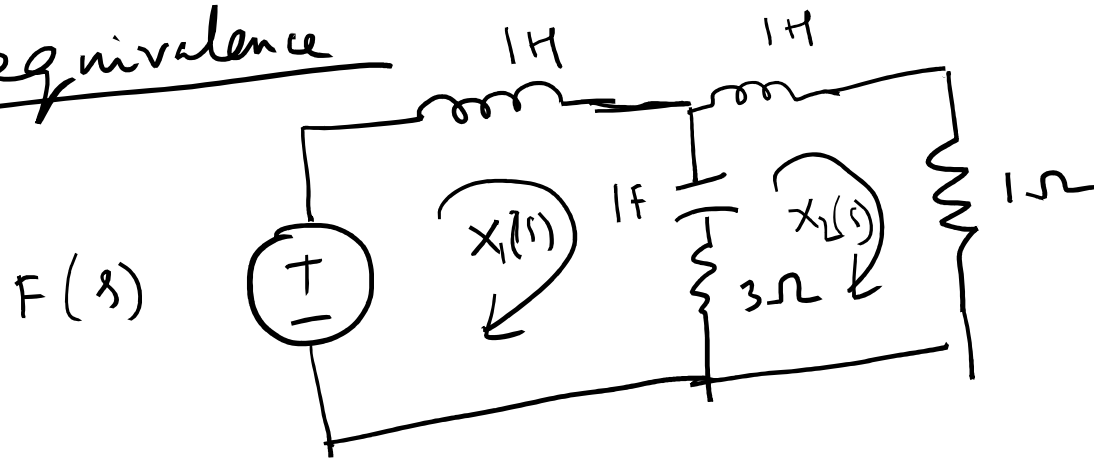
$$0 = -(3s+1) X_1(s) + (s^2 + 3s + 1) X_2(s) + s X_2(s) \quad (ii)$$

Ex

$$\frac{3s+1}{s^4 + 7s^3 + 5s^2 + s} = G(s)$$

Equivalent circuit

Series equivalence



Parallel equivalence

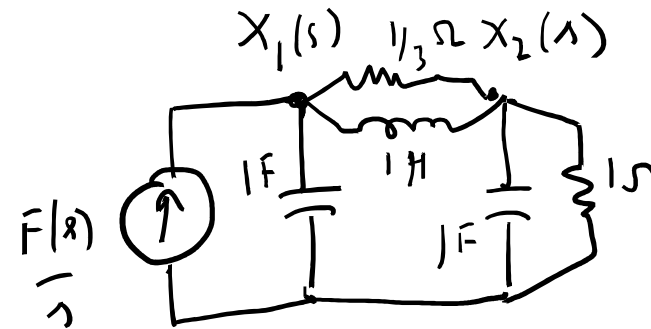
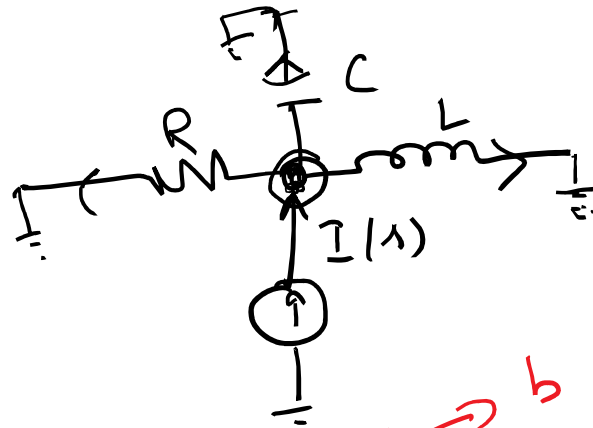
"through" variables: current, force, torque, etc.

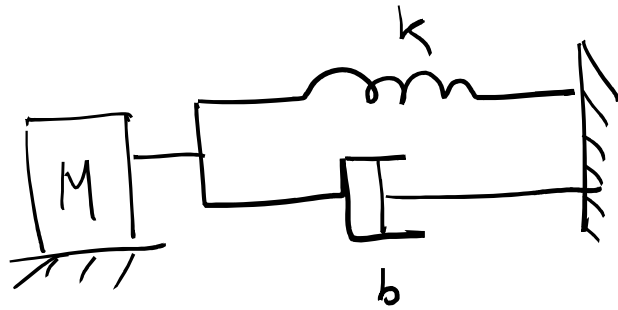
"across" variables: volt/displ/
ang. displ.

$$I(s) = V(s) \cdot \frac{1}{sL} + v(s) \cdot Cs + \frac{V(s)}{R}$$

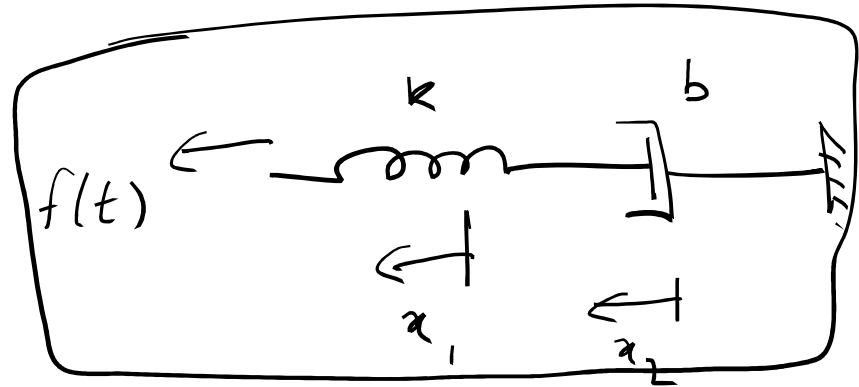
$$I(s) = V(s) \left[\frac{1}{sL} + Cs + \frac{1}{R} \right]$$

Red annotations: A red circle around $\frac{1}{sL}$ with an arrow pointing to 'K'. A red arrow points from 'Cs' to 'M'. A red circle around $\frac{1}{R}$ with an arrow pointing to 'b'.





$$F(s) = k x_1(s) \\ = s b x_2(s)$$



$$f(t) = k x_1 \quad (i)$$

$$f(t) = b \dot{x}_2 \quad (ii)$$

Total disp

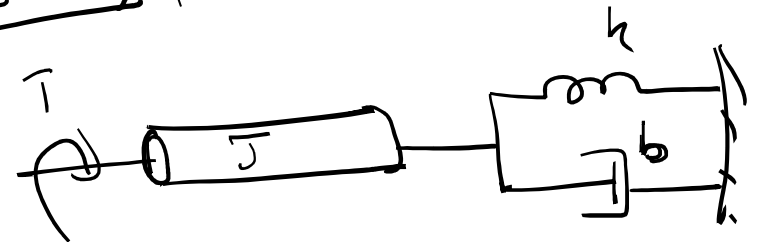
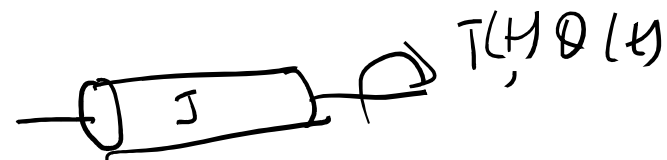
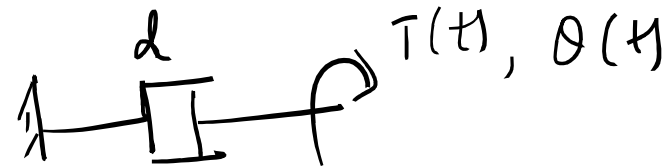
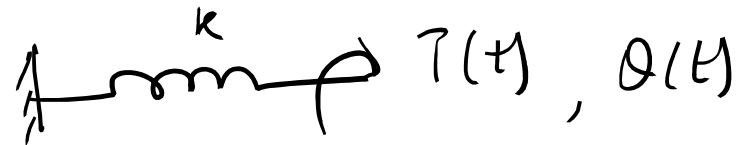
$$X(s) = x_1(s) + x_2(s) \Rightarrow \frac{F(s)}{k} + \frac{F(s)}{b s}$$

$$\Rightarrow \frac{X(s)}{F(s)} = \frac{1}{k} + \frac{1}{b s}$$

$$T(t) = k \theta(t)$$

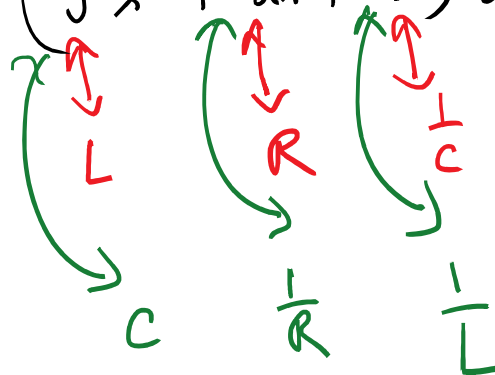
$$T(t) = d \dot{\theta}(t)$$

$$T(t) = J \ddot{\theta}(t)$$



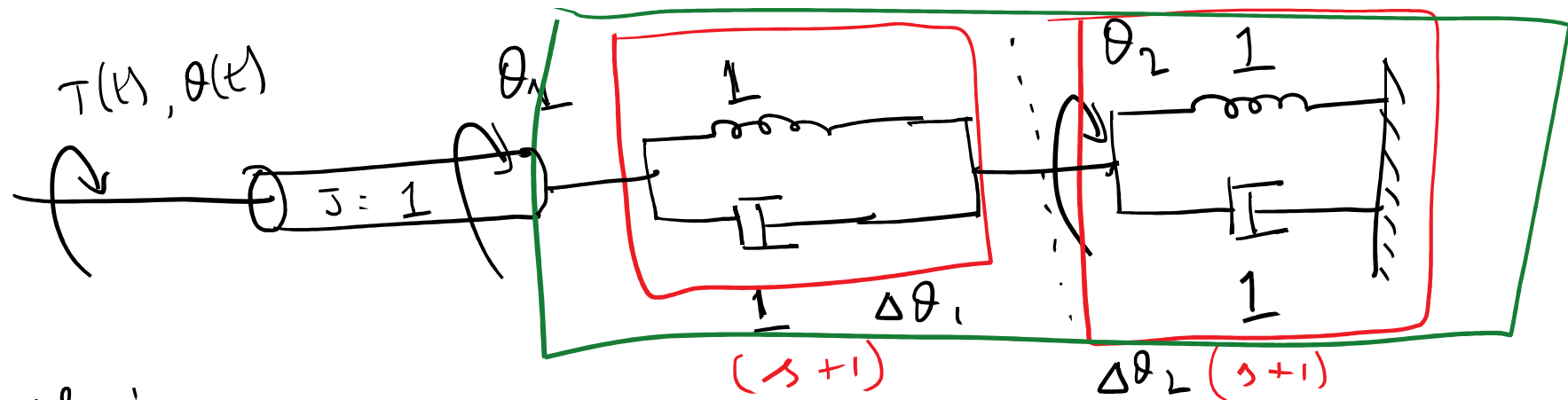
$$T(t) = J \ddot{\theta} + d \dot{\theta} + k \theta$$

$$\Rightarrow T(s) = (J s^2 + d s + k) \theta$$



→ Series Analog.

→ Parallel analog.



Obtain
 $\theta_2(s)/T(s)$

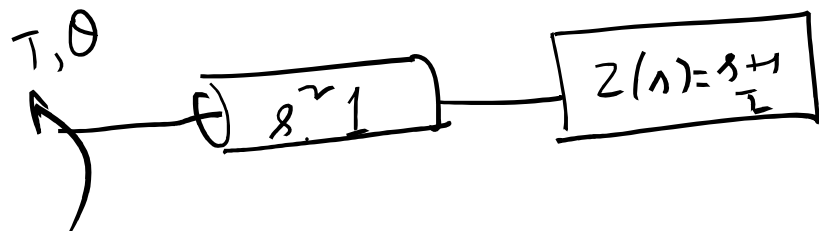
$$T = (s^2 + s + 1) \theta_1(s) + (s + 1) \theta_2(s) \quad \text{--- (1)}$$

$$0 = (\theta_2 - \theta_1) + (\dot{\theta}_2 - \dot{\theta}_1) + \theta_2 + \dot{\theta}_2$$

$$\Rightarrow 0 = -(s + 1) \theta_1(s) + 2(s + 1) \theta_2(s) \quad \text{--- (2)}$$

$$G(s) = \frac{1}{2s^2 + s + 1}$$

$$\frac{(s+1)(s+1)}{(s+1) + (s+1)} = \frac{s+1}{2}$$



$$\frac{T}{s+1} = \Delta\theta_1$$

$$\frac{T}{s+1} = \Delta\theta_2$$

$$\Rightarrow \Delta\theta_1 = \Delta\theta_2$$

$$T(s) = \left(s^2 + \frac{s+1}{2}\right) \theta(s)$$

$$\Rightarrow \frac{\theta(s)}{T(s)} = \frac{2}{2s^2 + s + 1}$$

Now,

$$\theta = \Delta\theta_1 + \Delta\theta_2$$

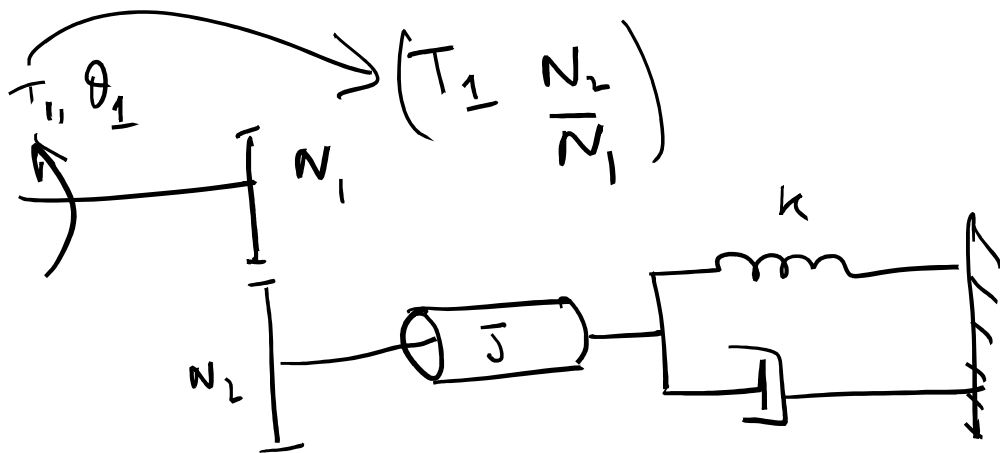
$$= 2\Delta\theta_2 = \theta_1$$

$$\Delta\theta_2 = \theta_2$$

$$\Delta\theta_1 = \theta_1 - \theta_2$$

$$\boxed{\frac{\theta_2}{T} = \frac{1}{2s^2 + s + 1}}$$

Gears



$$r_1 \theta_1 = r_2 \theta_2 \quad (1)$$

$$r_1 \theta_1 = r_2 \theta_2 \quad (2)$$

$$N_1 \theta_1 = N_2 \theta_2 \quad (3)$$

$$T_1 \theta_1 = T_2 \theta_2 \quad (4)$$

Combining (3) & (4) $\rightarrow$

$$\frac{\theta_1}{\theta_2} = \frac{N_2}{N_1} = \frac{T_2}{T_1}$$

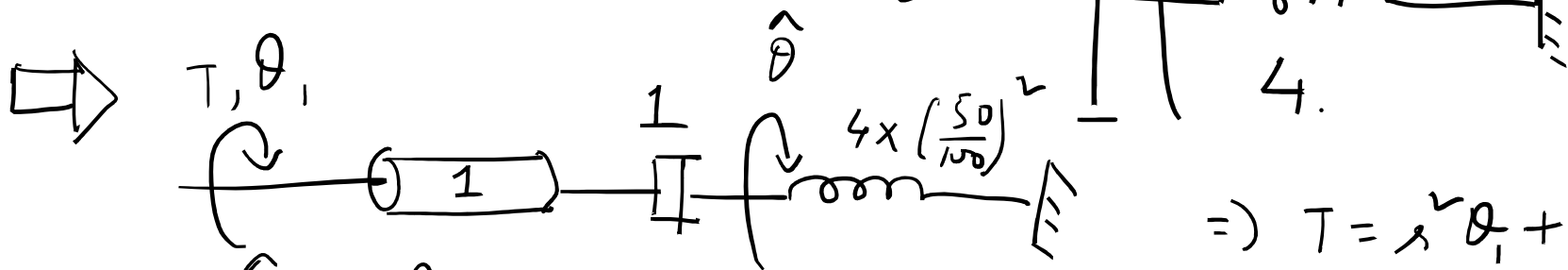
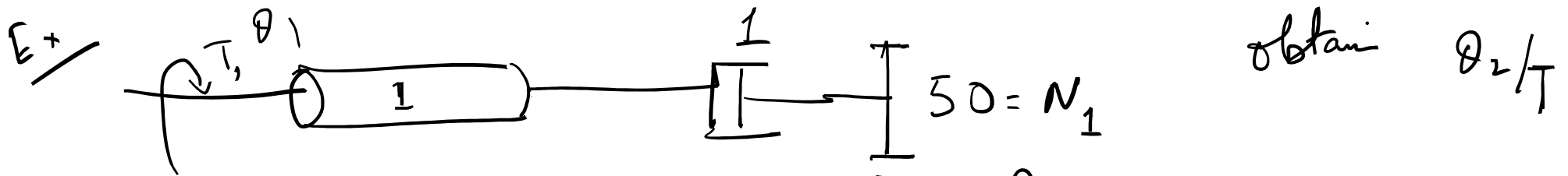
$$T_1\left(\frac{N_2}{N_1}\right) = (Js^2 + ds + k)\theta_2 = (Js^2 + ds + k)\theta_1\left(\frac{N_1}{N_2}\right)$$

$$\Rightarrow \frac{\theta_1}{T_1} = \frac{\frac{N_2}{N_1}}{\left(\frac{N_1}{N_2}\right)(Js^2 + ds + k)} = \frac{1}{J_{eq}s^2 + d_{eq}s + k_{eq}}$$

$$J_{eq} = J \cdot \left(\frac{N_1}{N_2}\right)^2$$

$$k_{eq} = k \cdot \left(\frac{N_1}{N_2}\right)^2$$

$$d_{eq} = d \cdot \left(\frac{N_1}{N_2}\right)^2$$



Note: $\hat{\theta} = 2\theta_2$

$$\frac{\theta_2}{T} = \frac{1/2}{s^2 + s + 1}$$

$$\Rightarrow T = s^2 \theta_1 + s(\theta_1 - \hat{\theta}) \quad (i)$$

$$\Delta D = s(\hat{\theta} - \theta_1) + \hat{\theta} \quad (ii)$$

$$\Rightarrow \theta_1 = \frac{(s+1)}{s} \hat{\theta}$$

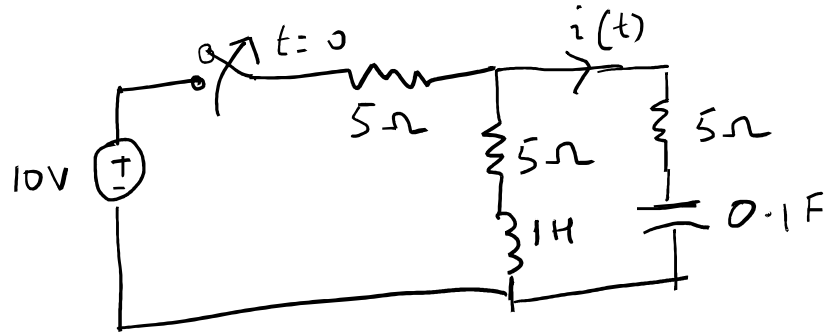
$$\Rightarrow T = s(s+1) \hat{\theta} + (s+1) \hat{\theta} - s \hat{\theta}$$

$$= (s^2 + s + 1) \hat{\theta}$$

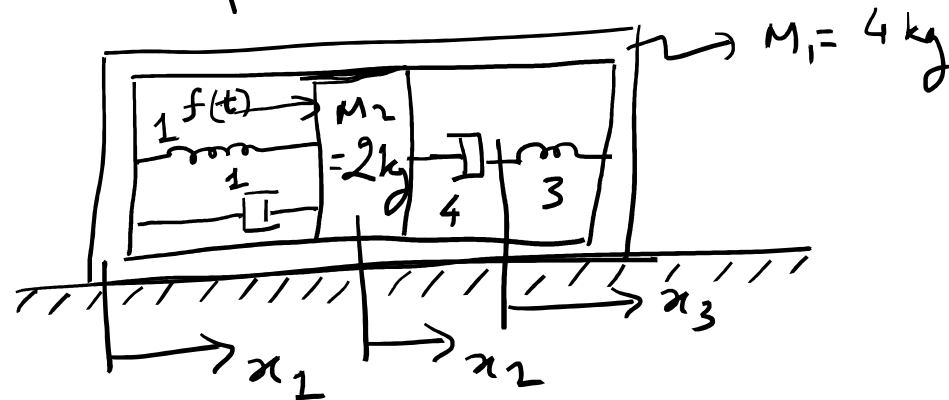
$$\Rightarrow \frac{\hat{\theta}}{T} = \frac{1}{s^2 + s + 1}$$

Exercises

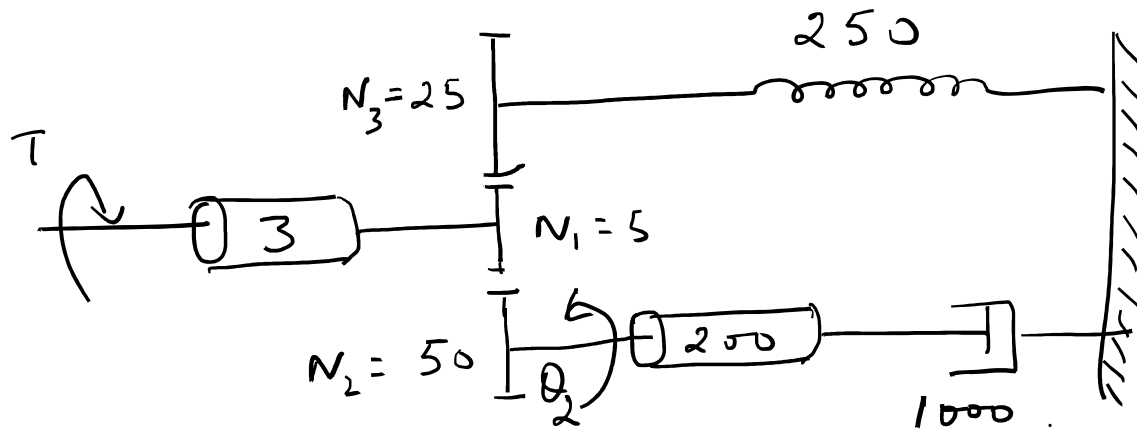
- Solve for $i(t)$, $t > 0$, using Laplace transform.



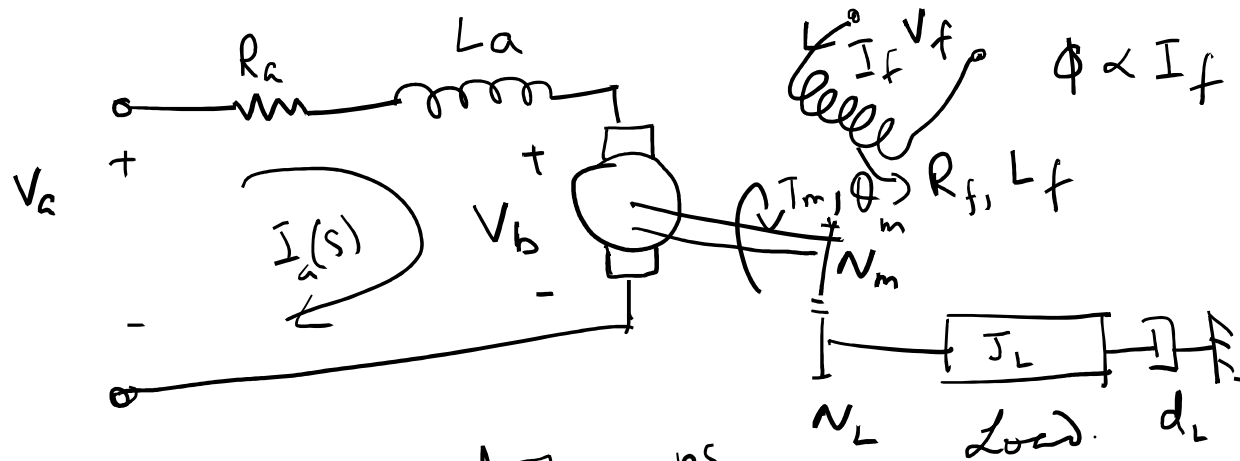
- Obtain $X_3(s)/F(s)$ for the following system. (units are consistent)
Assume all surfaces to be frictionless



- Obtain $\frac{\theta_2(s)}{T(s)}$ for the following system. (All units are consistent)



Module 2 : Modelling electromechanical systems



Armature
Control

obtain $\frac{\Theta_m(s)}{V_a(s)}$

$$V_b = \frac{p \Phi N_m}{\omega} \text{ rps}$$

$\frac{p}{2} \frac{N_m}{N_L} \frac{\omega_m}{2}$

Elect.

$$V_b(s) = k_b \cdot s \Theta_m(s) \quad \text{--- (1)} \quad V_b = k_b \cdot \omega_m, \quad \omega_m = \frac{d\Theta_m}{dt}$$

$$V_a(s) - V_b(s) = (R_a + sL_a) I_a(s) \quad \text{--- (2)}$$

Mech.

$$T_m(s) = \left[J_m + J_L \left(\frac{N_m}{N_L} \right)^2 \right] s^2 + \left[d_m + d_L \left(\frac{N_m}{N_L} \right)^2 \right] s \Theta_m(s)$$

$$T \propto \phi,$$

$$T \propto I_c$$

$$T = k_m I_c(s)$$

Electromechanical part.

• Obtain $\frac{\theta_m(s)}{T(s)} = \frac{1}{J_e s^2 + d_e s} \rightarrow \textcircled{I}$

• $V_c(s) = k_b s \theta_m(s) + (R_c + sL_c) I_c(s).$

$$= k_b s \theta_m(s) + (R_c + sL_c) \frac{T(s)}{k_m}$$

$$= \left[k_b s \frac{1}{J_e s^2 + d_e s} + \frac{(R_c + sL_c)}{k_m} \right] T(s)$$

$$\Rightarrow \frac{T(s)}{V_c(s)} = \frac{1}{\frac{R_c + sL_c}{k_m} + \frac{k_b}{J_e s + d_e}}$$

$$\textcircled{II}$$

(22)

$$\frac{\theta_m(s)}{V_a(s)} = \frac{k_m}{s [k_b k_m + (R_c + s L_c) (J_e s + d_e)]}$$

$$L_c \ll R_c$$

$$= \frac{k_m}{s [k_b k_m + R_c (1 + \frac{s L_c}{R_c}) (J_e s + d_e)]}$$

$$= \frac{k_m}{s [J_e R_c s + R_c d_e + k_b k_m]}$$

$$= \frac{\frac{k_m}{J_e R_c}}{s \left[s + \frac{d_e}{J_e} + \frac{k_b k_m}{J_e R_c} \right]} = \frac{k}{s(s + \alpha)}$$

$$\frac{k_m}{J_e R_c}, k_b$$

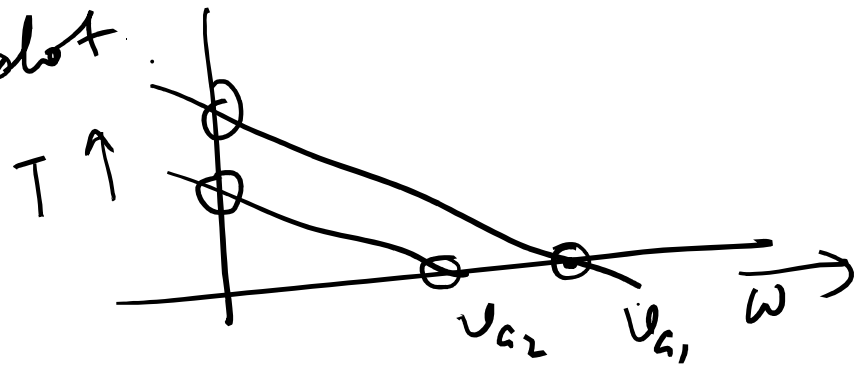
$$\Omega(s) = s \theta(s)$$

$$V_a(s) = k_b \Omega(s) + (R_a + s \frac{J_e}{k_m}) \frac{T(s)}{k_m}$$

$$V_a(s) = k_b \Omega(s) + \frac{R_a}{k_m} T(s)$$

$$v_a(t) = k_b \omega(t) + \frac{R}{k_m} T(t)$$

For a given $v_a(t)$, we have a straight line plotted in the $T-\omega$ plot.



$$T_{stall} = e_a \cdot \frac{k_m}{R_a} \cdot \frac{v_{a2}}{k_b}$$

Ex Derive the t.f. betw $\theta_m(s)$ and $V_f(s)$ (field control)

Module 3 : Transient response

$$G(s) = \frac{s^3 + s^2 + 3s + 4}{s^4 + 5s^3 + 7s^2 + 8s + 5}$$

$$u = e^{\alpha t}$$

$$U(s) = \frac{1}{s - \alpha}$$

$$Y(s) = G(s) \boxed{U(s)}$$

$$y(t) = \mathcal{L}^{-1}[G(s)U(s)]$$

$$y^{(4)} + 5y^{(3)} + 7y'' + 8y' + 5y = u^{(3)} + u'' + 3u' + 4u.$$

$$y = \underbrace{y_f}_{\text{particular}} + \underbrace{y_n}_{\text{homogeneous}}$$

$\boxed{e^{\alpha t}}$ $\rightarrow$ y_f
 $\boxed{\sum_{i=1,2,3,4} C_i e^{p_i t}}$ $\rightarrow$ y_n

$$s^4 + 5s^3 + 7s^2 + 8s + 5 = 0$$

$$p_1, p_2, p_3, p_4$$

$$Y(s) = \sum_{i=1}^{d_i} \frac{a_i}{(s + p_i)^{r_i}}$$

$$\frac{a}{s + a}$$

$$\frac{as + b}{cs^2 + ds + b}$$

First order systems

$$G(s) = \frac{a}{s + a}$$

$$Y(s) = \frac{1}{s} \cdot \frac{a}{s + a}$$

$$\lim_{s \rightarrow 0} s \cdot Y(s) = \lim_{s \rightarrow 0} \frac{a}{s + a} = \frac{1}{1} = \lim_{t \rightarrow \infty} y(t)$$

$$\underline{\text{d.c. gain} = 1}$$

(E)

$$y(t) = [1 - e^{-at}] \underline{1(t)}$$

- time constant: the time at which the op reaches 63% of its s.s. value

$$1 - e^{-a \frac{1}{a}} = 1 - e^{-1} = 0.63$$

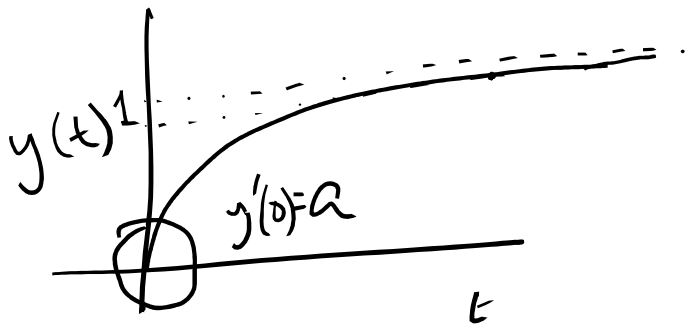
$$\frac{a}{s+a} = \frac{1}{1+s\tau} \quad \tau = \frac{1}{a}$$

- rise time: time taken by y to go from 10% to 90% of its s.s. value.

$$\begin{aligned} 1 - e^{-at_1} &= 0.1 \Rightarrow e^{-at_1} = 0.9 \Rightarrow \\ 1 - e^{-at_2} &= 0.9 \Rightarrow e^{-at_2} = 0.1 \Rightarrow \end{aligned} \quad \left. \begin{aligned} & \\ & \end{aligned} \right\} t_2 - t_1 = \frac{1}{a} \ln 9$$

(E) $\approx \frac{2.2}{a}$

settling time : time taken by $y(t)$ to reach within 2% of its s.s value.



$$1 - e^{-a t_s} = 0.98$$

$$t_s = \frac{1}{a} \boxed{\ln 50} = \frac{3.9}{a} \approx \frac{4}{a}$$

Step response of second order systems

$$G(s) = \frac{\omega_n^2}{s^2 + 2\zeta\omega_n s + \omega_n^2}$$

$$s = -\zeta\omega_n \pm \sqrt{\zeta^2 - 1} \omega_n$$

ζ → damping ratio

- $\zeta > 1 \longrightarrow$ Overdamped.

$$G(s) = \frac{p_1 p_2}{(s + p_1)(s + p_2)}$$

p_1, p_2 are
distinct

$$Y(s) = \frac{1}{s} \cdot G(s)$$

(*) $y(t) = \left[1 - \frac{1}{p_1 - p_2} \left[p_1 e^{p_2 t} - p_2 e^{p_1 t} \right] \right]$



$$p_1, p_2 < 0$$

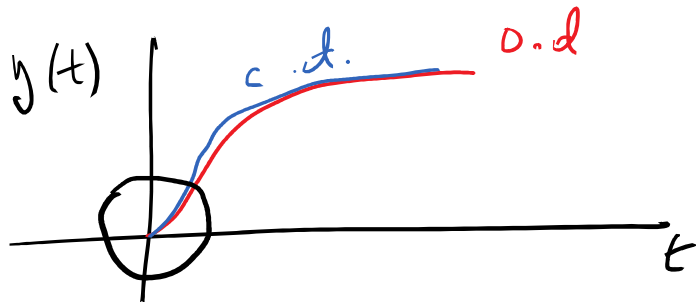
• $\zeta = 1 \rightarrow$ critically damped

$$G(s) = \frac{p^2}{(s+p)^2} \quad p \in \mathbb{R}_-$$

$$Y(s) = \frac{1}{s} \cdot \frac{p^2}{(s+p)^2}$$

(C)

$$y(t) = 1 - e^{-pt} - pte^{-pt}$$



$$y'(0) = 0$$

- Suppose you look at the step responses for a 1st order system & a second order system. Is there a way to distinguish between the two if ζ (for 2nd order system) is ≥ 1 ?

Ans : Look for $y'(0)$. Ex Hint: Apply
 I.V.T to $y'(t)$.

• Undamped system : $\zeta = 0$

$$G(s) = \frac{\omega_n^2}{s^2 + \omega_n^2}$$

$$U(s) = 1/s$$

⑤ $y(t) = 1 - \cos \omega_n t.$

• Underdamped system ($0 < \zeta < 1$)

$\omega_n \rightarrow$ natural freq. $\zeta \rightarrow$ damping ratio.

$$Y(s) = \frac{1}{s} \cdot \frac{\omega_n^2}{s^2 + 2\zeta\omega_n s + \omega_n^2}$$

$$U(s) = 1/s$$

$$Y(s) = \frac{A}{s} + \frac{Bs + C}{s^2 + 2\zeta\omega_n s + \omega_n^2}$$

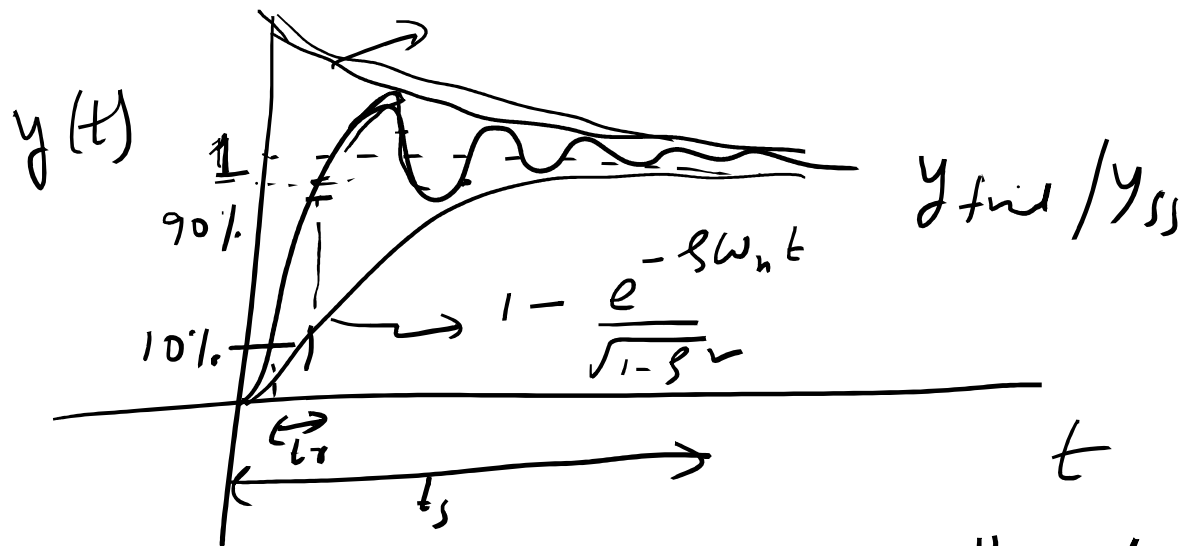
(5*) $A = 1 ; B = -1 ; C = -2\zeta\omega_n$

$$Y(s) = \frac{1}{s} - \frac{(s + \zeta\omega_n)}{(s + \zeta\omega_n)^2 + (\underbrace{\omega_n \sqrt{1-\zeta^2}}_{\omega_d})^2} - \frac{\zeta\omega_n}{(s + \zeta\omega_n)^2 + (\omega_n \sqrt{1-\zeta^2})^2}$$

$$\begin{aligned} y(t) &= 1 - e^{-\zeta\omega_n t} \cos \omega_d t - \frac{\zeta}{\sqrt{1-\zeta^2}} \int \left[\frac{\omega_n \sqrt{1-\zeta^2}}{(s + \zeta\omega_n)^2 + \omega_d^2} \right] \\ &= 1 - \frac{e^{-\zeta\omega_n t}}{\sqrt{1-\zeta^2}} \left[\sqrt{1-\zeta^2} \cos \omega_d t + \zeta \sin \omega_d t \right] \\ &\quad \text{Suppose } \tan \phi = \frac{\zeta}{\sqrt{1-\zeta^2}} \end{aligned}$$

$$y(t) = 1 - \frac{e^{-\zeta \omega_n t}}{\sqrt{1-\zeta^2}} \cos(\omega_d t - \phi)$$

- t_s
- t_r
- % O.S.
- t_p



- it enters the 2% band of s.s value and "continues to remain within the band thereafter"

$$\frac{y_{max} - y_{ss}}{y_{ss}} \times 100 = \% O.S.$$

- time at which y_{max} is attained by $y(t)$. $\rightarrow$ $(\forall t > t_s)$

- $t_r \approx \frac{1.8}{\omega_n}$ ✓
- $t_p = \frac{\pi}{\omega_n \sqrt{1-\zeta^2}} = \frac{\pi}{\omega_d}$

• 0.05 ✓

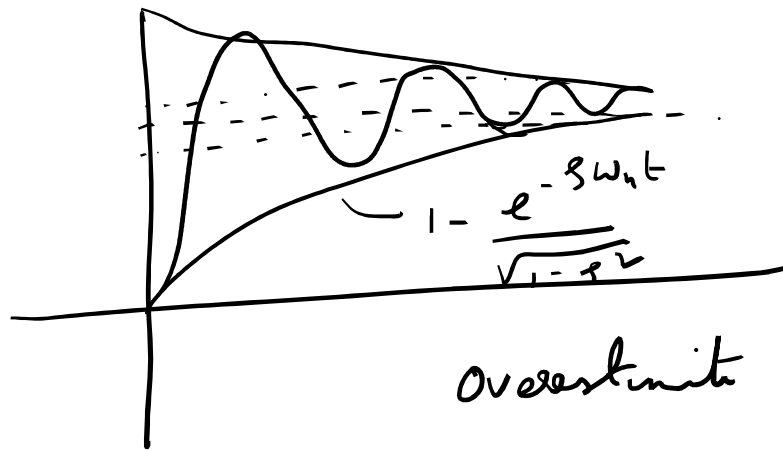
$$y(t_p) = 1 - \frac{e^{-\zeta \omega_n t_p}}{\sqrt{1-\zeta^2}} \cos\left(\omega_n \sqrt{1-\zeta^2} t_p - \phi\right) = \frac{\omega_n}{\sqrt{1-\zeta^2}} e^{-\zeta \omega_n t} \sin \omega_d t = 0$$

$$= 1 + e^{-\frac{\zeta \pi}{\sqrt{1-\zeta^2}}}$$

$$\% \text{ OS} = \frac{y(t_p) - y_{ss}}{y_{ss}} = \boxed{e^{-\frac{\pi \zeta}{\sqrt{1-\zeta^2}}}} \Rightarrow \omega_d t = n\pi$$

$$n = 0, 1, 2, \dots$$

$$n = 1 \rightarrow \text{maxima.}$$

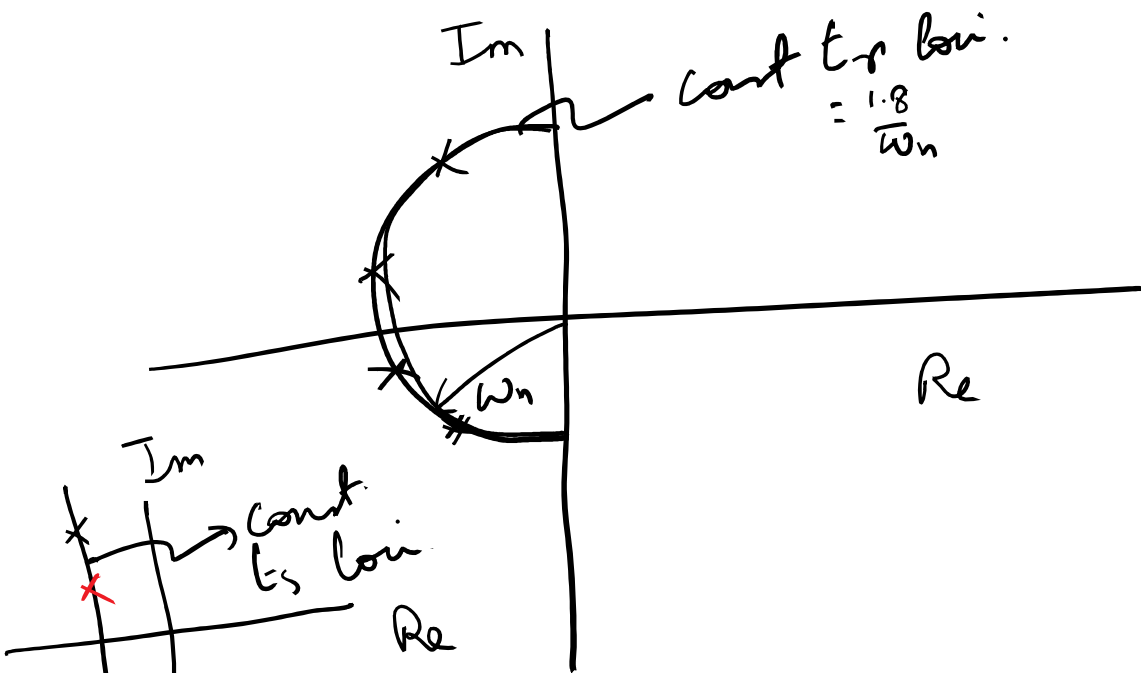


$$t_s = \frac{4}{\zeta \omega_n}$$

$$1 - \frac{e^{-\zeta \omega_n t_s}}{\sqrt{1 - \zeta^2}} = 0.98$$

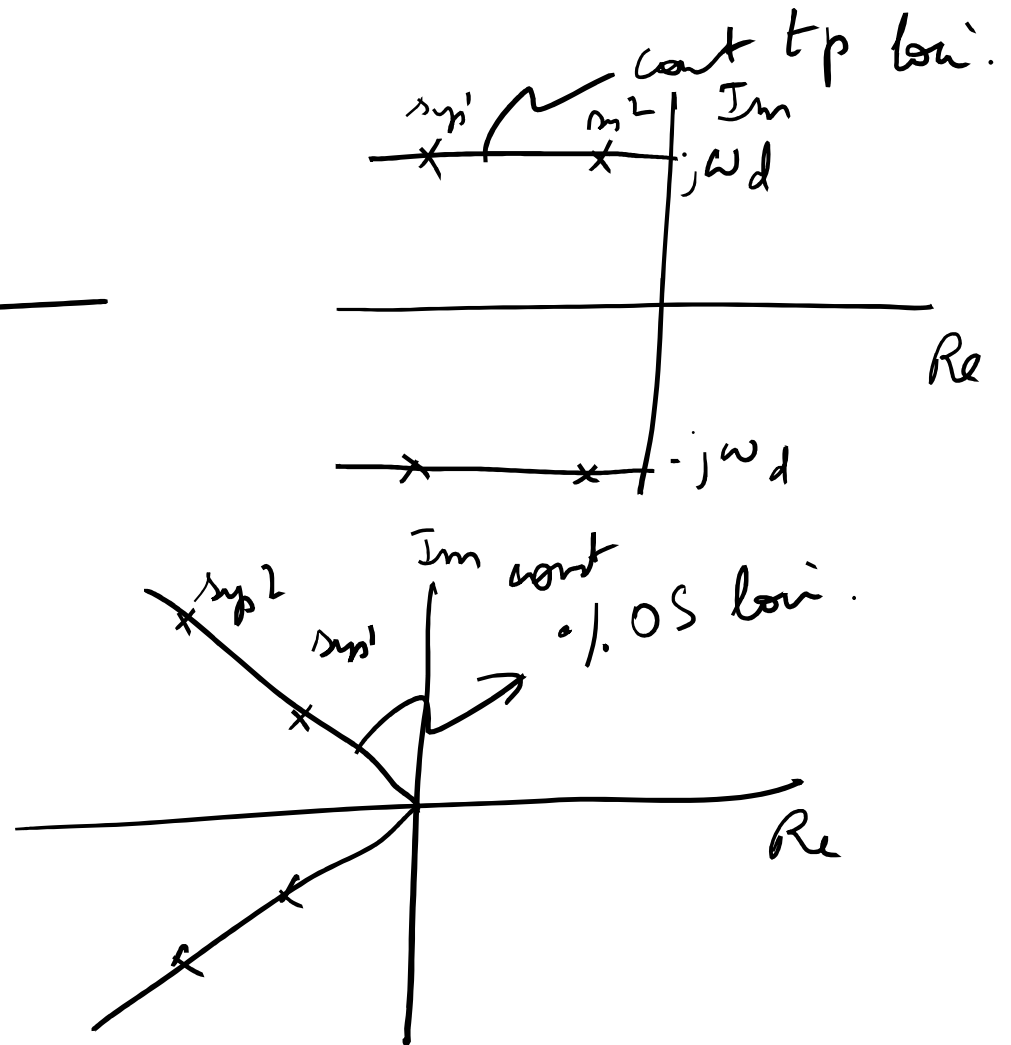
$$\Rightarrow t_s = - \frac{1}{\zeta \omega_n} \boxed{\ln(0.02 \sqrt{1 - \zeta^2})}$$

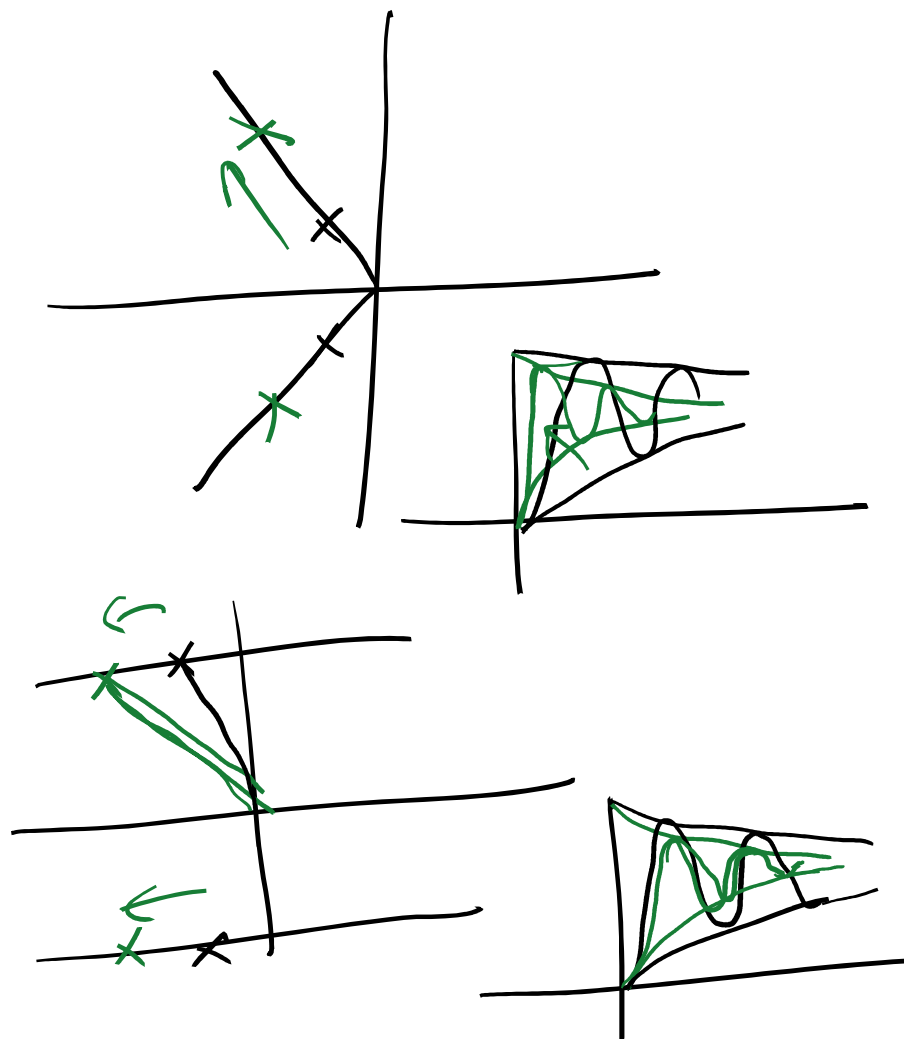
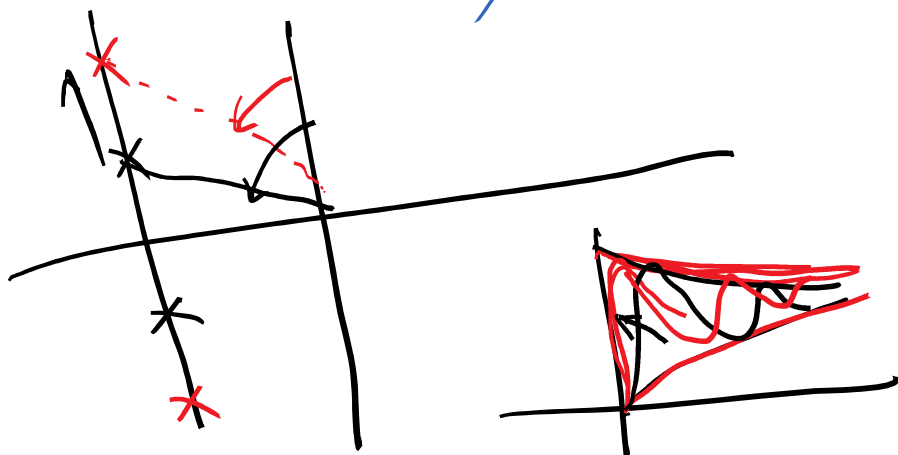
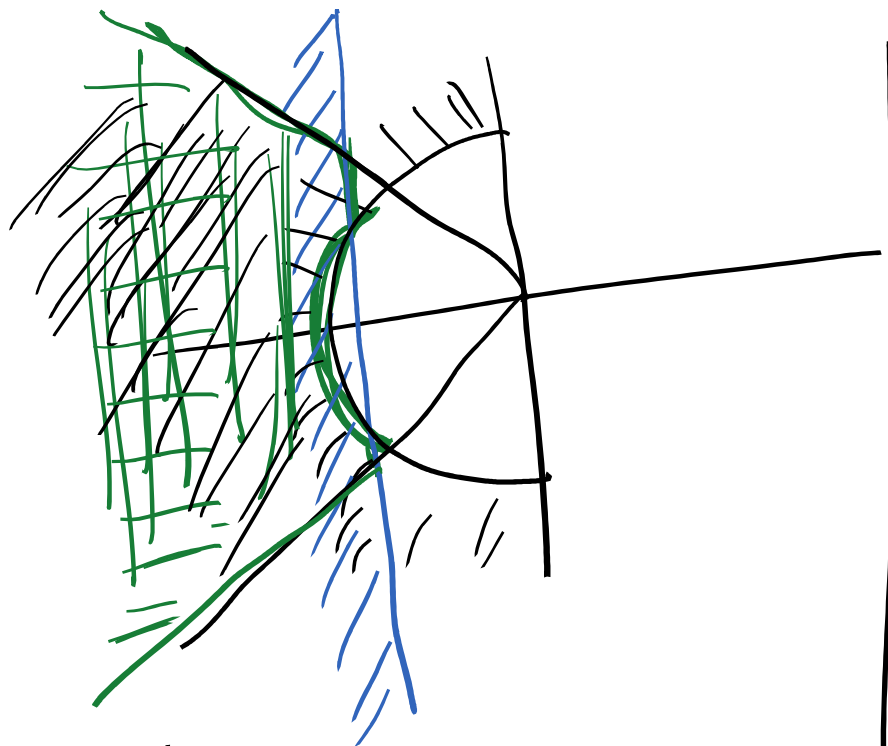
$$\approx \frac{4}{\zeta \omega_n} \quad \begin{matrix} 0 < \zeta < 0.9 \\ 3.91 - 4.7 \end{matrix}$$



$$s = -\xi\omega_n \pm j \underbrace{\omega_n \sqrt{1-\xi^2}}_{\omega_d}$$

$$|s| = \omega_n$$





Effects of additional poles & zeros.

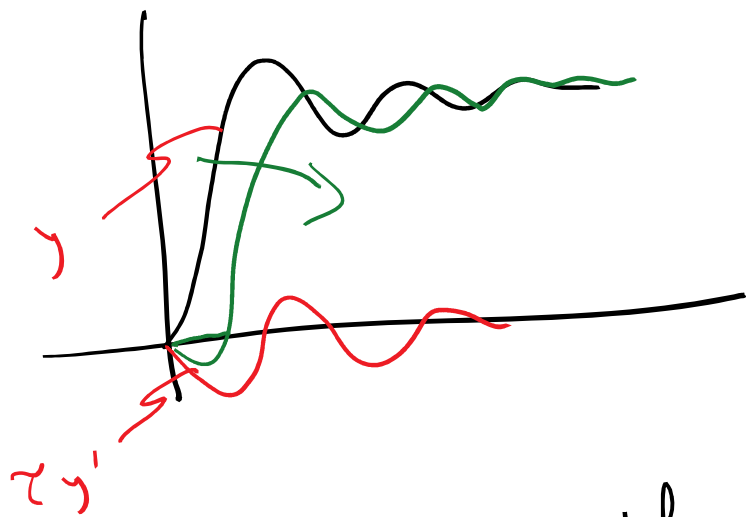
$$G_1(s) = \frac{\omega_n^2 (1 + s\tau)}{s^2 + 2\zeta\omega_n s + \omega_n^2} \quad \tau > 0$$

$$G_2(s) = \frac{\omega_n^2}{(s^2 + 2\zeta\omega_n s + \omega_n^2)(1 + s\tau)} \quad \tau > 0$$

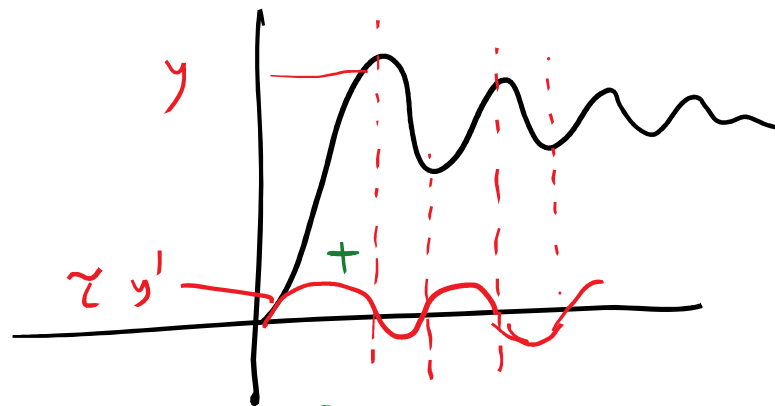
$$\boxed{-1/\tau \approx -\zeta\omega_n}$$

→ All the analysis we have carried out does not help!

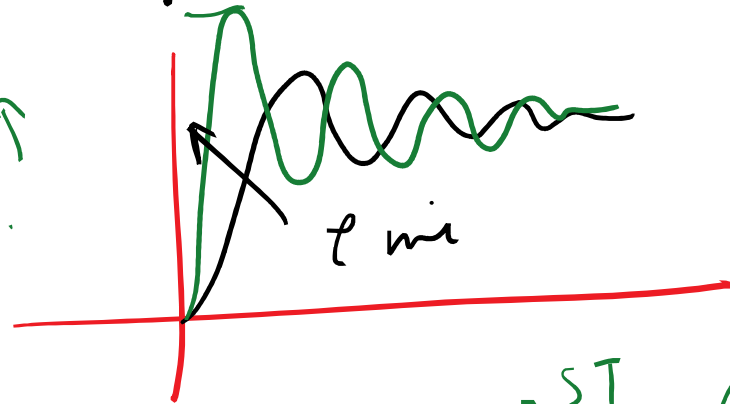
Suppose $0 < \tau \ll \xi \omega_n$



Non-minimum phase systems ($\tau < 0$)



$\cdot 1.65 \uparrow$
var.
 $t_p \downarrow$

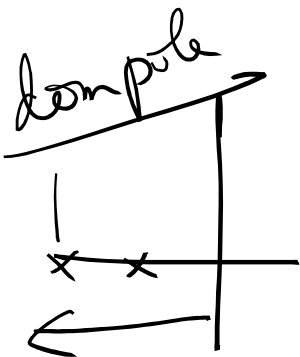


Pade approx

$$e^{-sT} \approx \frac{1 - sT/2}{1 + sT/2}$$

Effect of additional poles

$$G(s) = \frac{\omega_n^2}{(s^2 + 2\zeta\omega_n s + \omega_n^2)(1+s\tau)}$$



$$\text{Re}(p_1) = -\zeta\omega_n$$

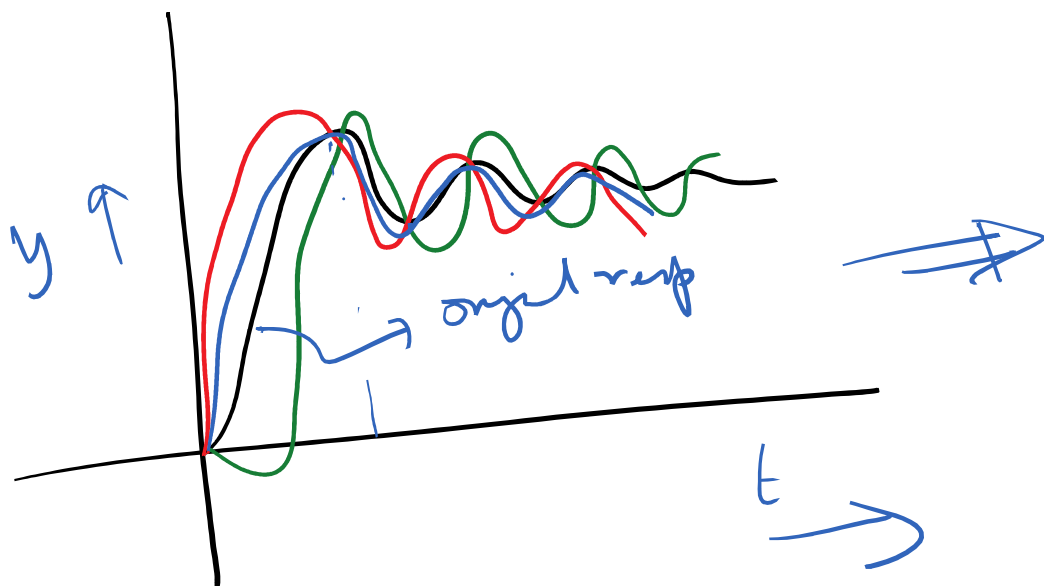
Dominant pole

$$|1/\tau| > 5 \left| \text{Re}(\text{dom pole}) \right|$$

$$G_3 = \frac{\omega_n^2(1+s\tau_1)^{\frac{1}{5}}}{(s^2 + 2\zeta\omega_n s + \omega_n^2)(1+s\tau_2)} \quad \tau_1 \rightarrow \tau_2$$

Let $\tau \rightarrow 0$

$$G > G_2 > G_3 \quad [C] e^{-t/\tau}$$



$$\boxed{\tau y'} + \boxed{y}$$