

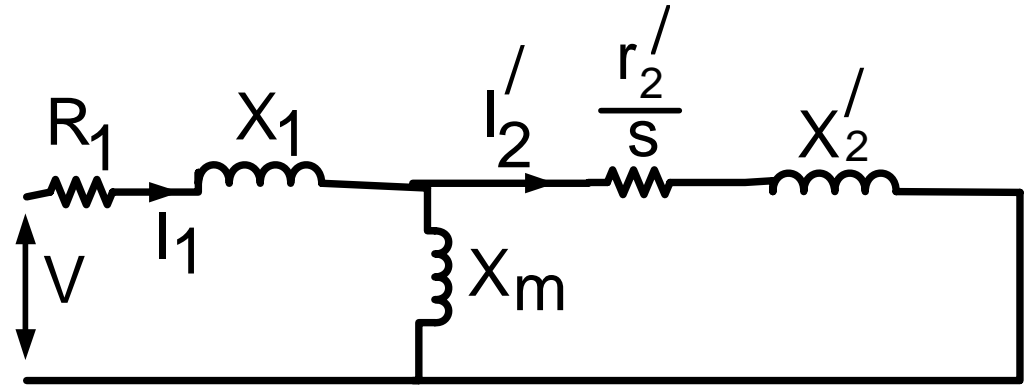
EE 111

# Introduction to Electrical Systems

Lecture - 34

# Performance features

I/M never runs at  
synch. speed =  
Asynchronous Motor



Starting Current

Starting Torque

Power Factor

Efficiency

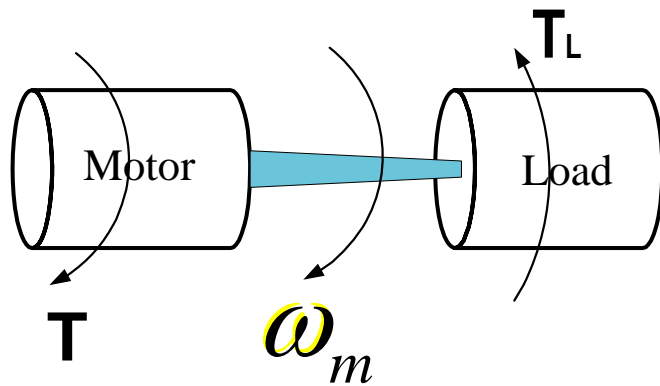
## Name Plate Rating:

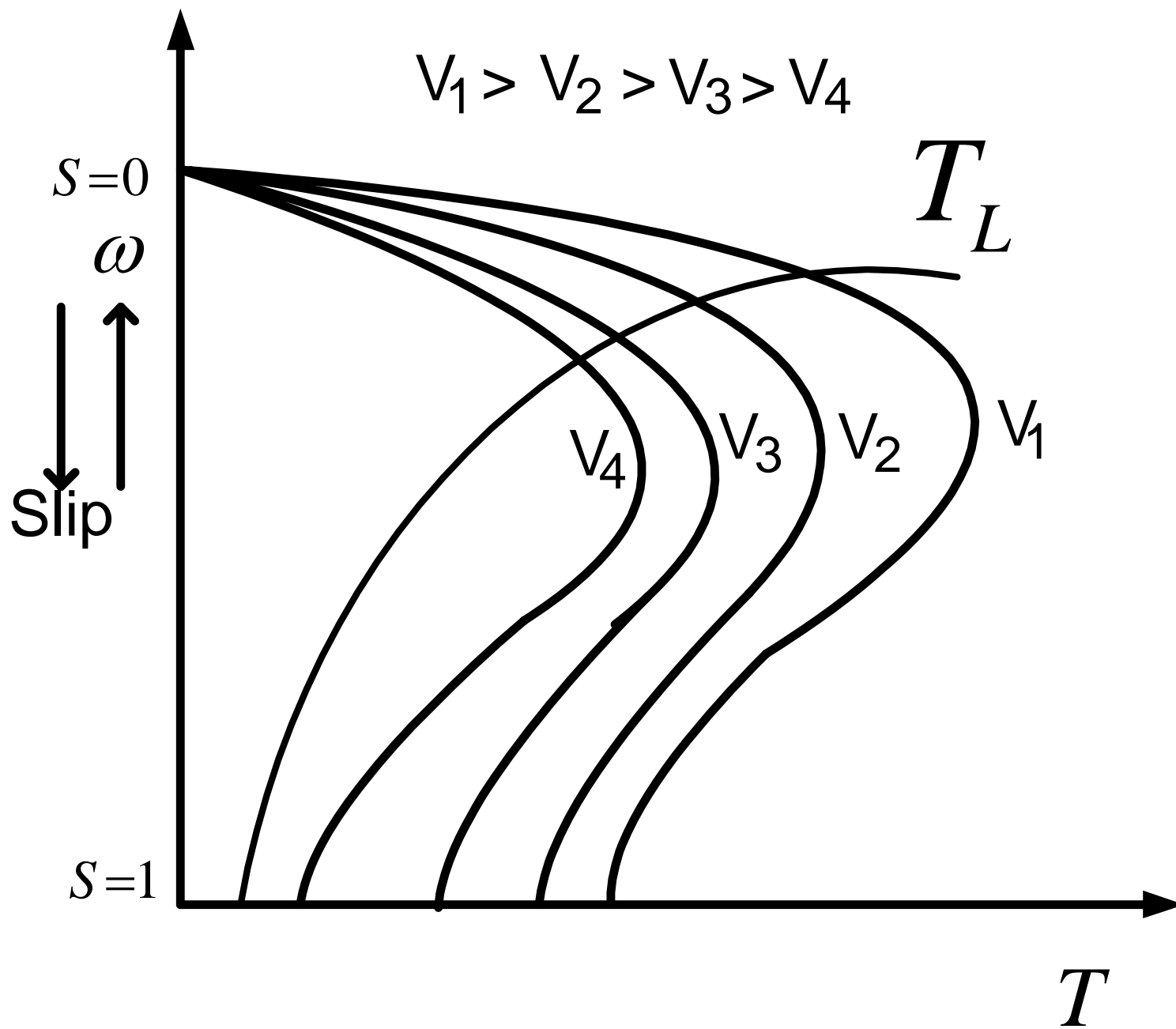
12 kW, 3- $\phi$ , 50 Hz, 25 A, 400 V, 1440 rpm  
delta connected, 0.8 pf (lag) squirrel cage  
induction motor

## Generating Mode of operation

# Variable terminal voltage control

$$T = \frac{3}{\omega_s} \left[ \frac{V_t^2 \frac{r_2'}{s}}{\left(R_t + \frac{r_2'}{s}\right)^2 + (X_t + X_2')^2} \right] \approx \frac{3}{\omega_s} \frac{V_t^2}{r_2'} s$$





# Variable terminal voltage control

- Poor efficiency

Neglecting stator losses and rotational losses:

$$P_m = (1 - s)P_g$$

$$\eta = \frac{P_m}{P_g} = (1 - s)$$

# Rotor resistance Control: Wound rotor Motors

$$T = \frac{3}{\omega_s} \left[ \frac{V_t^2 \frac{r_2'}{s}}{(R_t + \frac{r_2'}{s})^2 + (X_t + X_2')^2} \right] \approx \frac{3}{\omega_s} \frac{V_t^2}{r_2'} s$$

# Variable frequency Control

In order to maintain air gap flux at its rated value:

Assuming,  $V \simeq E$

$$f = kf_{rated}$$

$$E \simeq V = kV_{rated}$$

Therefore,

$$\frac{V}{f} = \frac{V_{rated}}{f_{rated}}$$

$$N_s = \frac{120f}{P}$$

$$E_{rated} = 4.44k_{sw}N_{st}f_{rated}\phi_p$$

$$\phi_p = \frac{E_{rated}}{4.44k_{sw}N_{st}f_{rated}}$$

**V / f Controlled induction motor drive**



# DC Machine

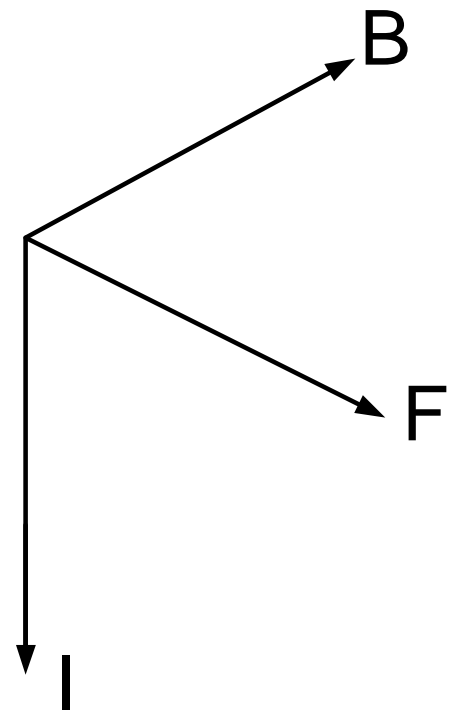
**DC Machine:**

**DC Motor**

**DC Generator**

Conductor carrying current when placed  
in a magnetic field experience  
Mechanical force.

Fleming's Left hand Rule

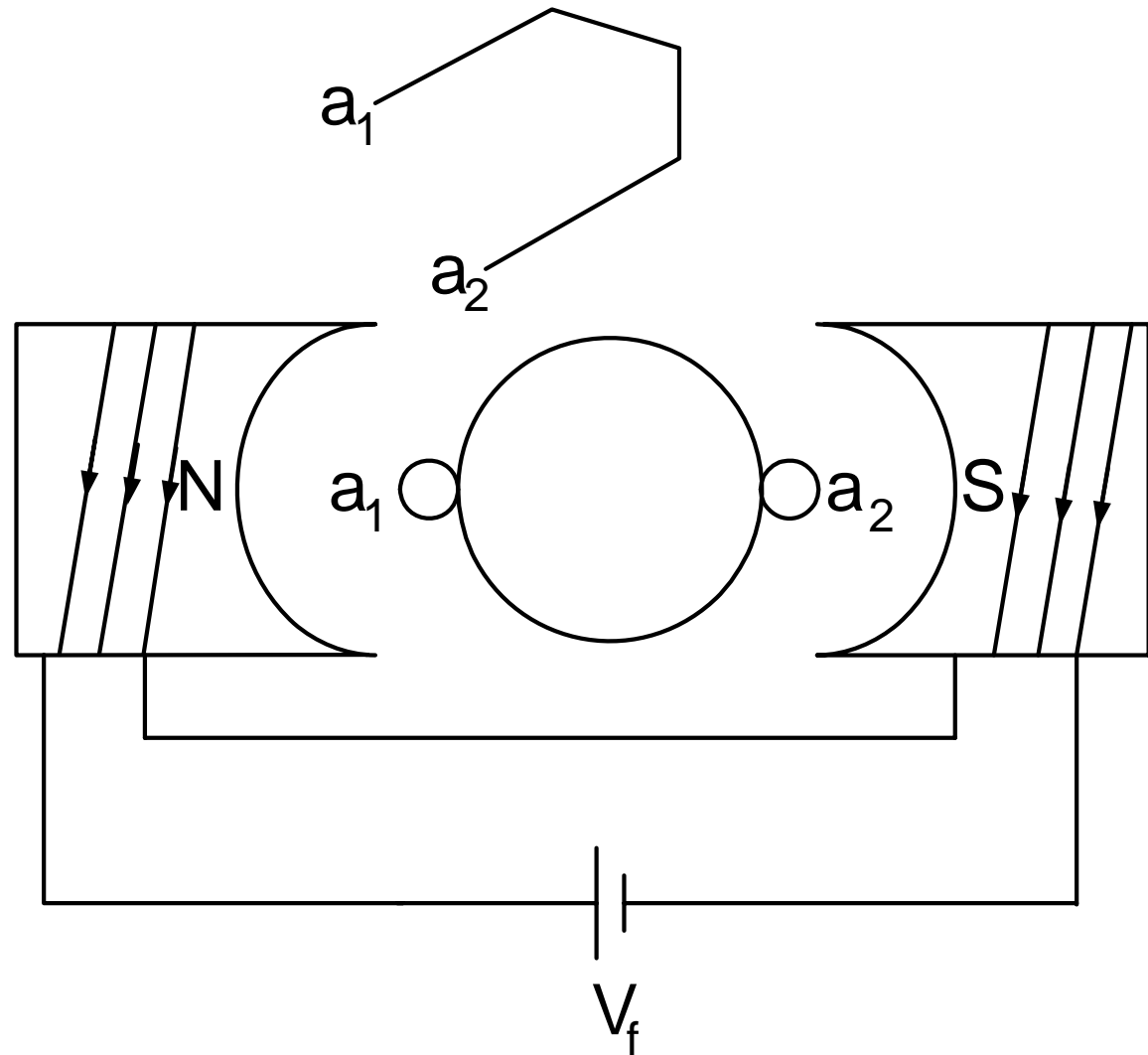


# DC M/C : Principle of Operation

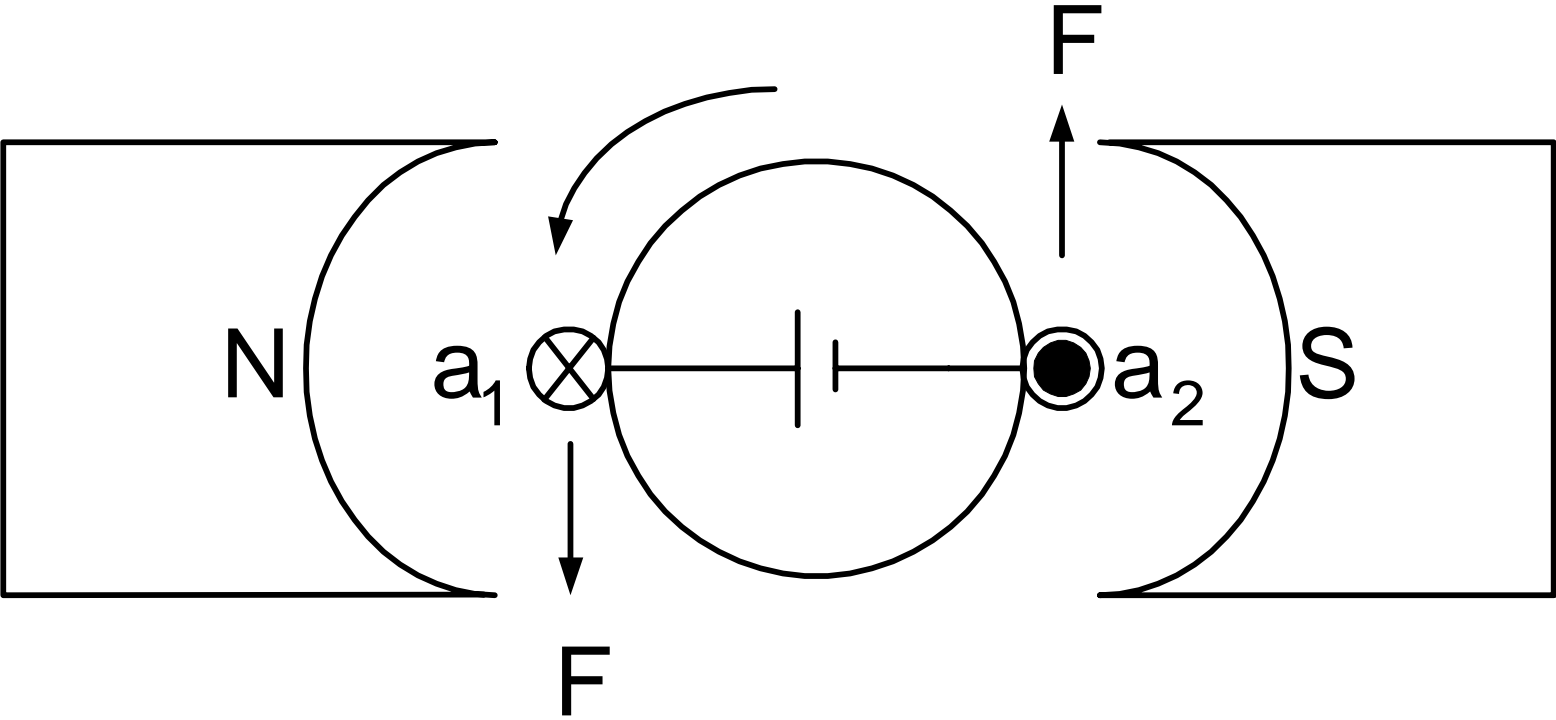
Field winding

Armature

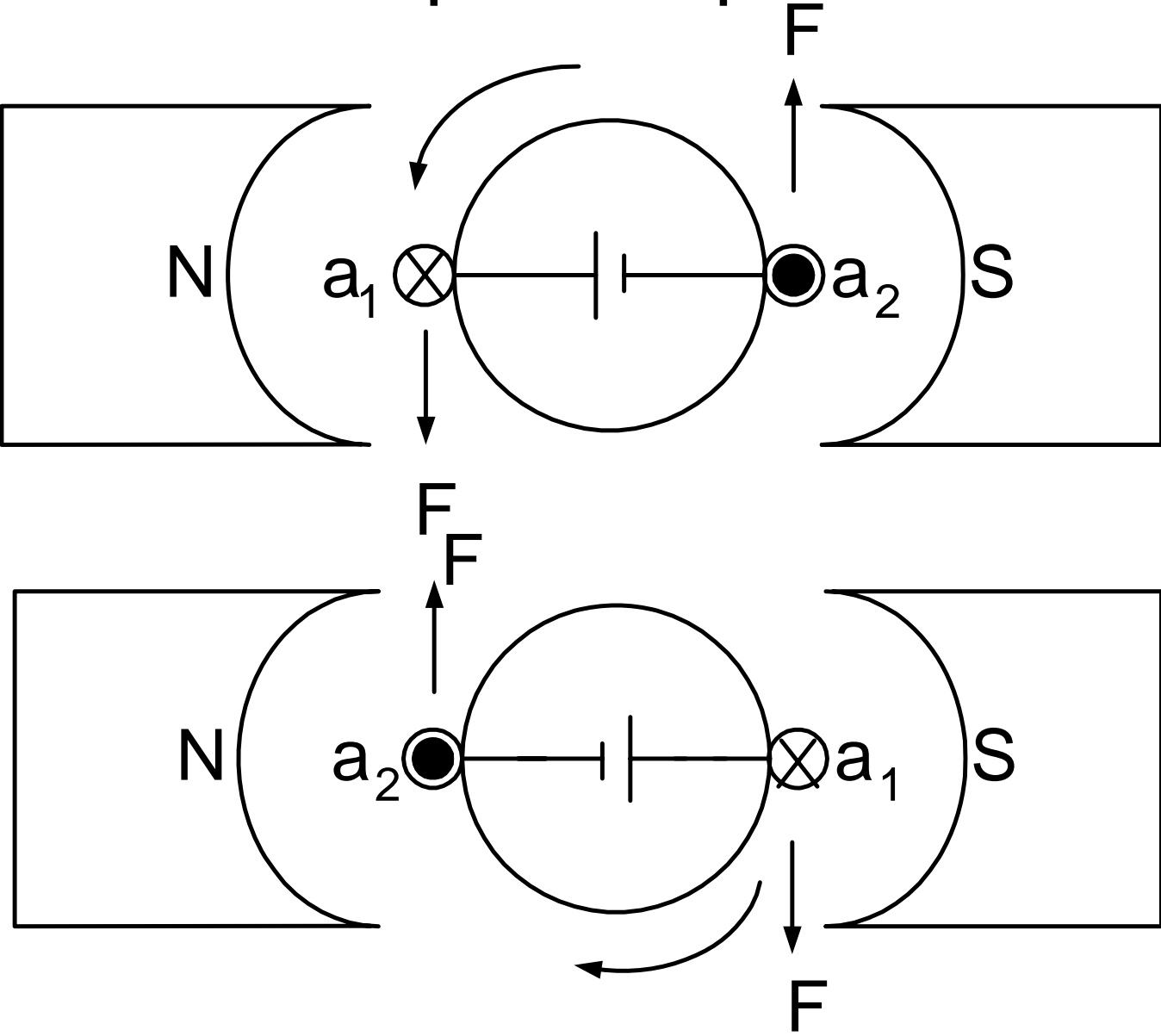
Armature Conductor



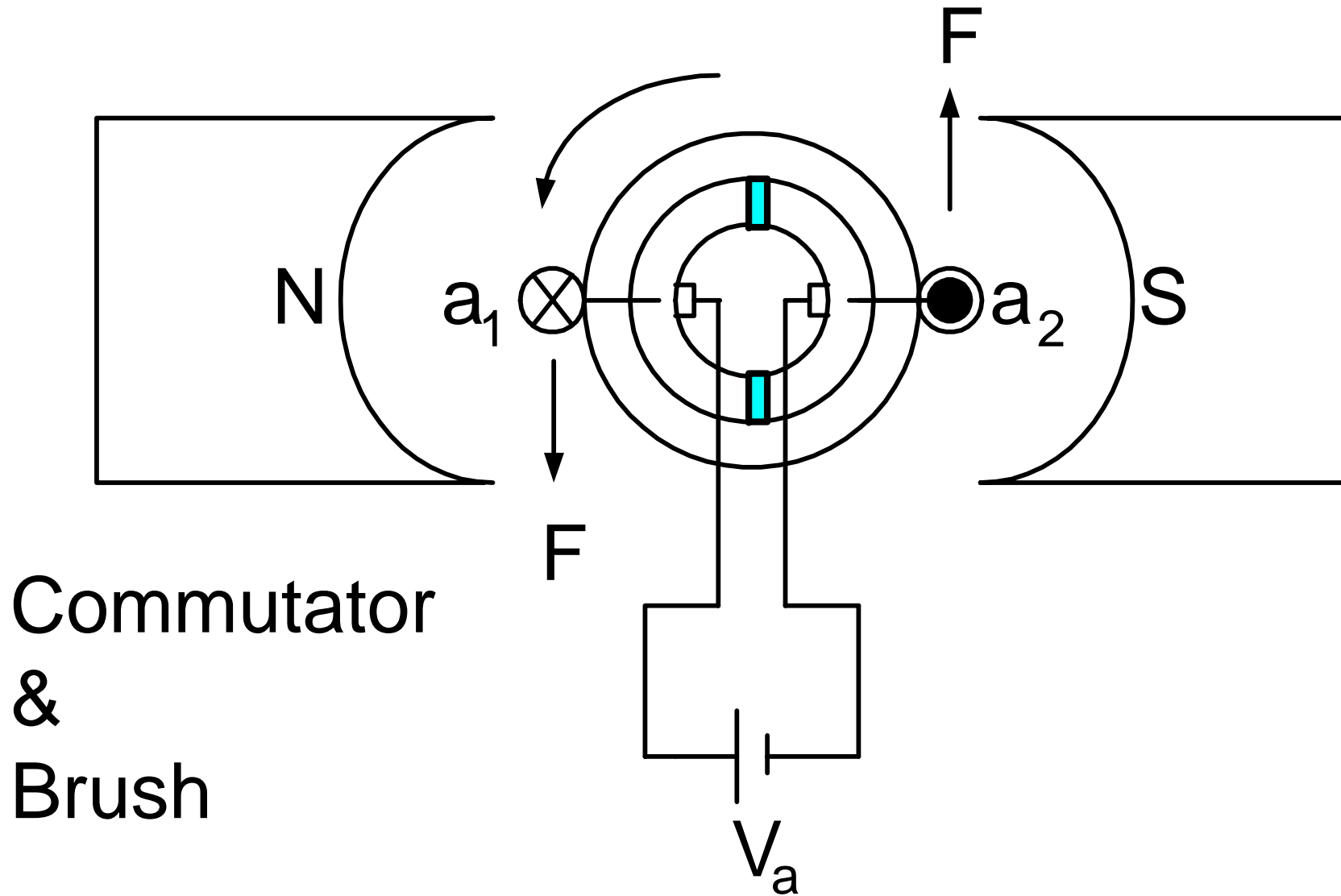
# DC M/C : Principle of Operation



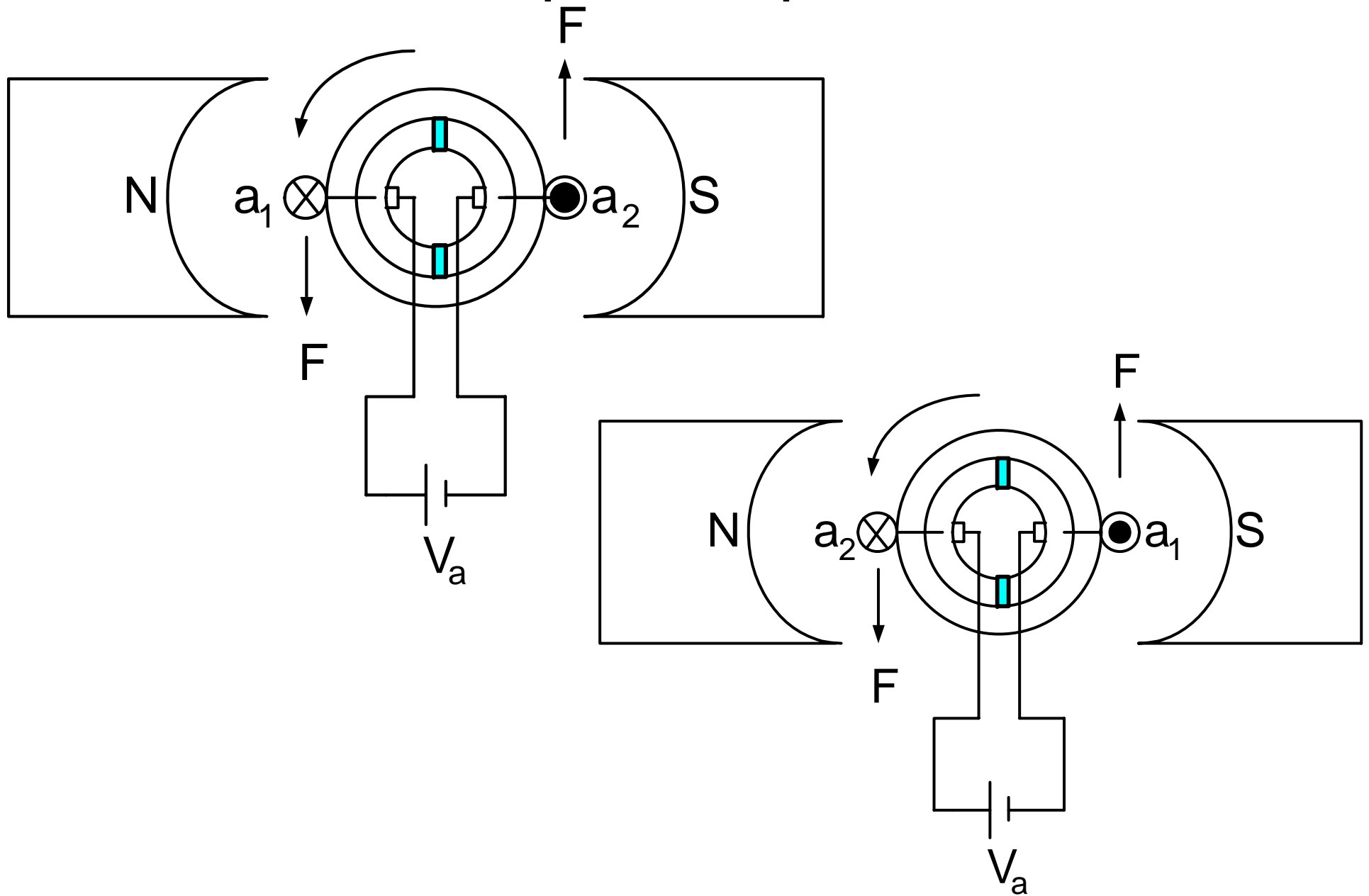
# DC M/C : Principle of Operation



# DC M/C : Principle of Operation

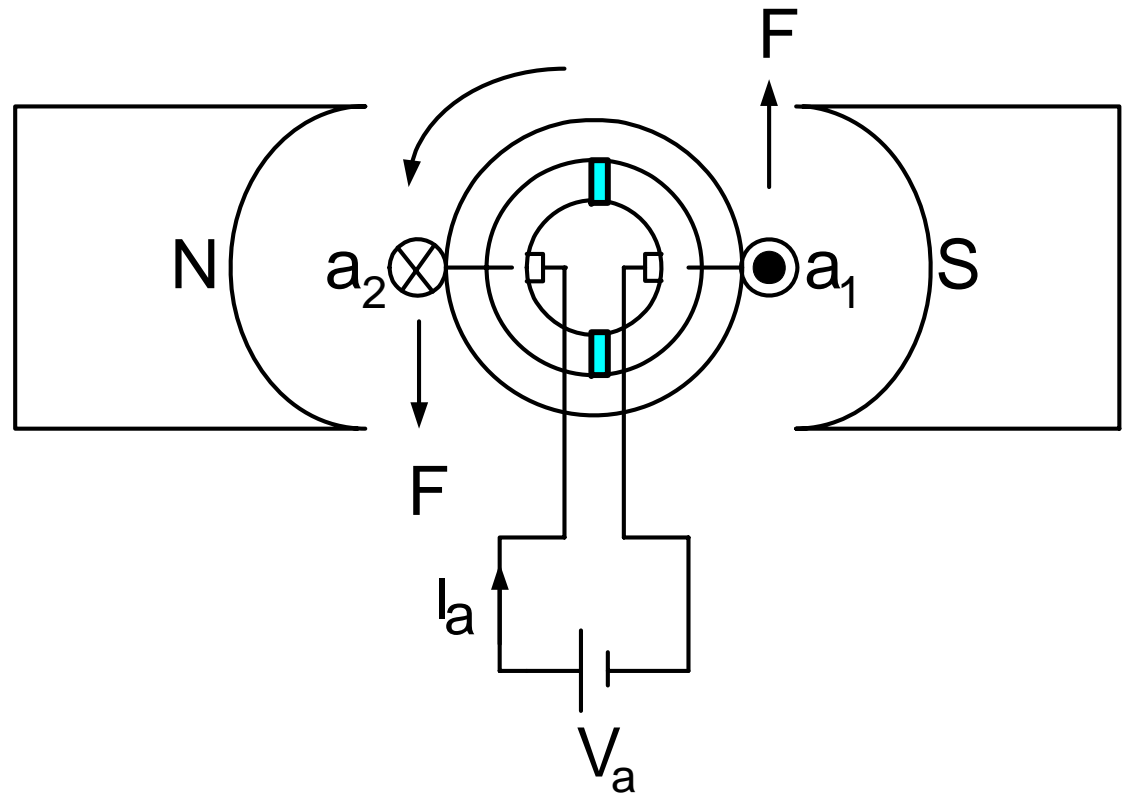


# DC M/C : Principle of Operation





# DC M/C : Principle of Operation



$$F = BIL \sin \theta$$

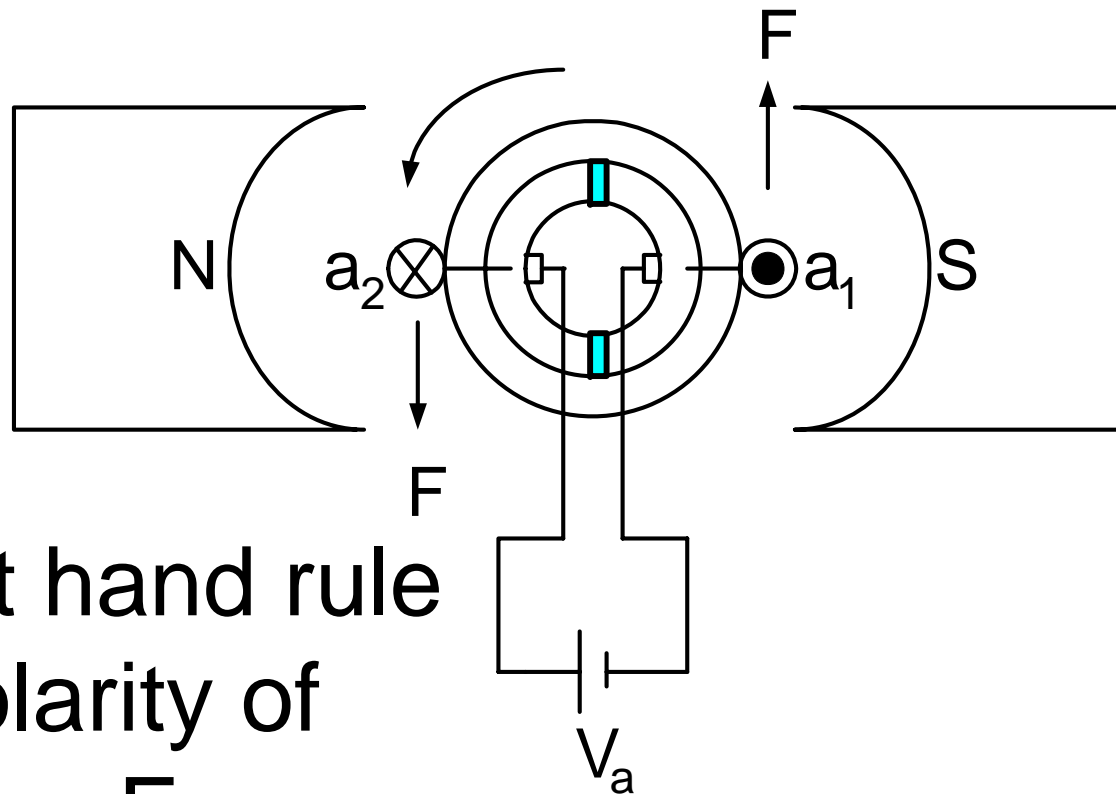
$$\theta \approx 90^\circ$$

$$T \propto \phi I_a$$

# Contradiction from Faraday's Law

$$E_b = 2BLv \sin \theta$$

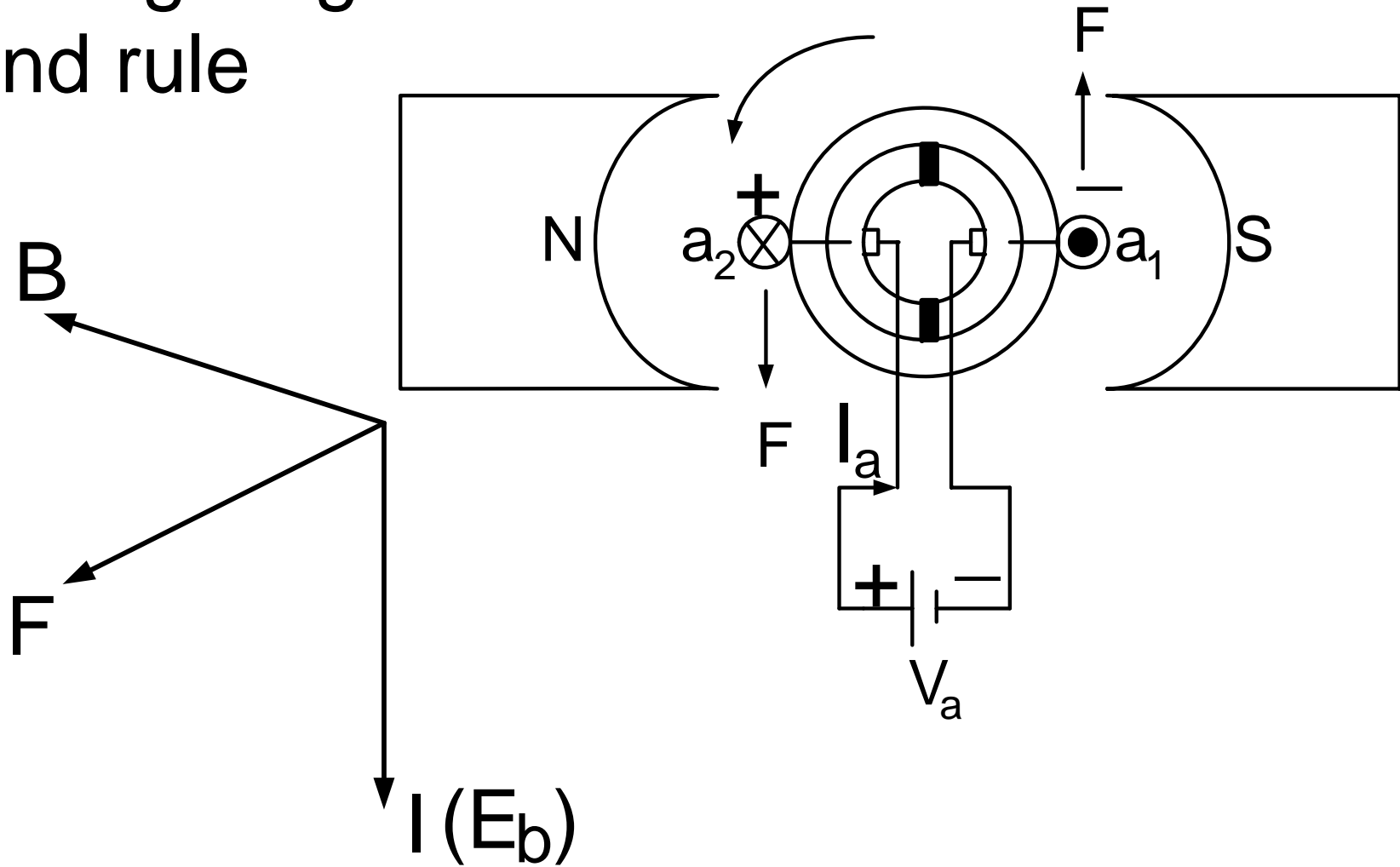
$$E_b \propto \phi \omega$$



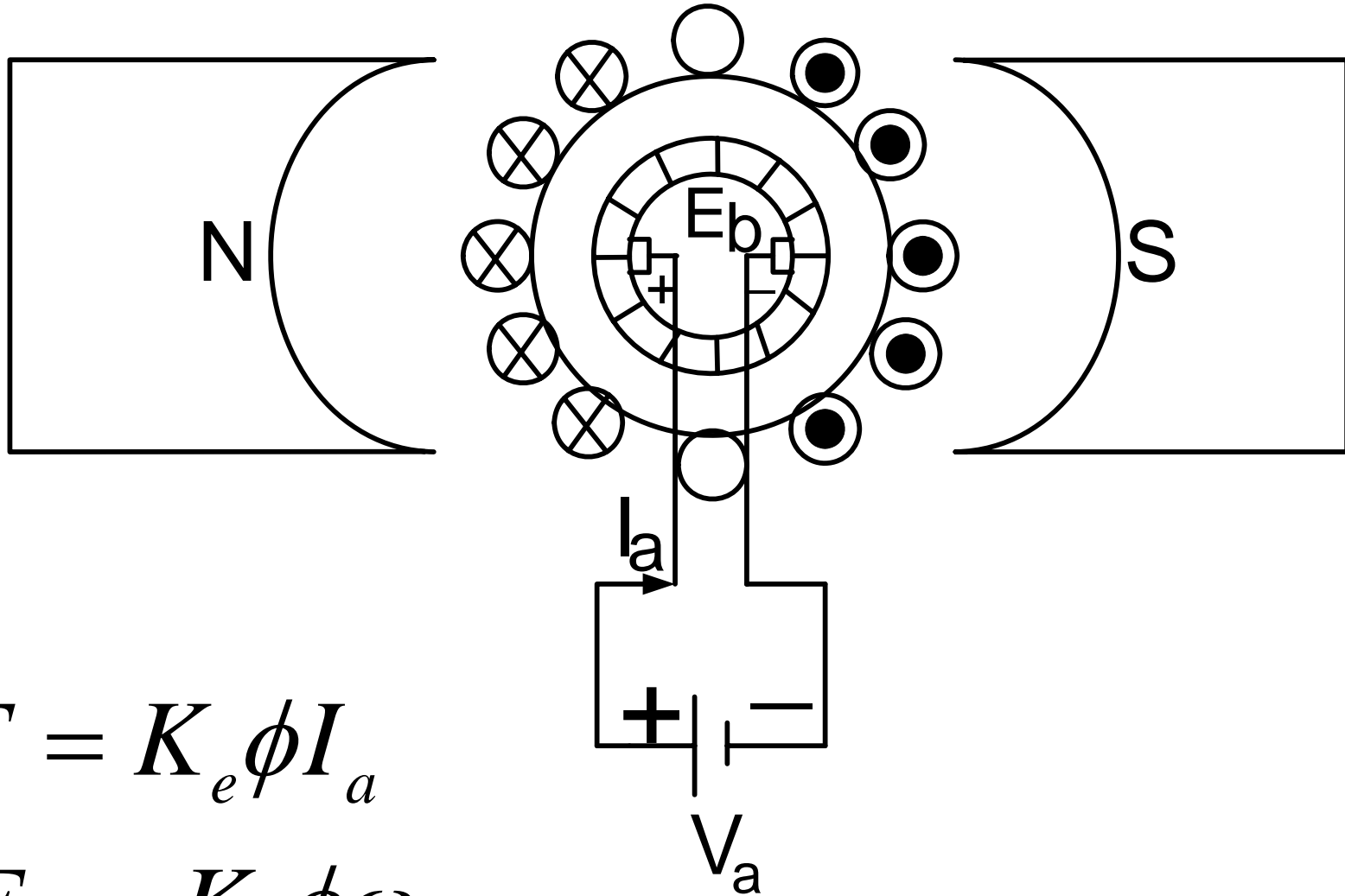
Fleming's right hand rule assigns the polarity of induced voltage, E

# DC M/C : Principle of Operation

Fleming's right  
Hand rule



# A Realistic DC Machine



$$T = K_e \phi I_a$$

$$E_b = K_e \phi \omega$$

# DC Machine: Steady state model and behaviour

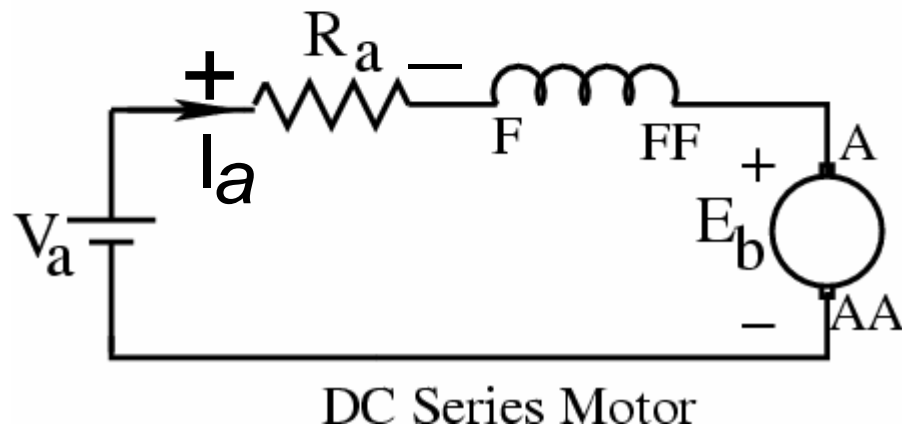
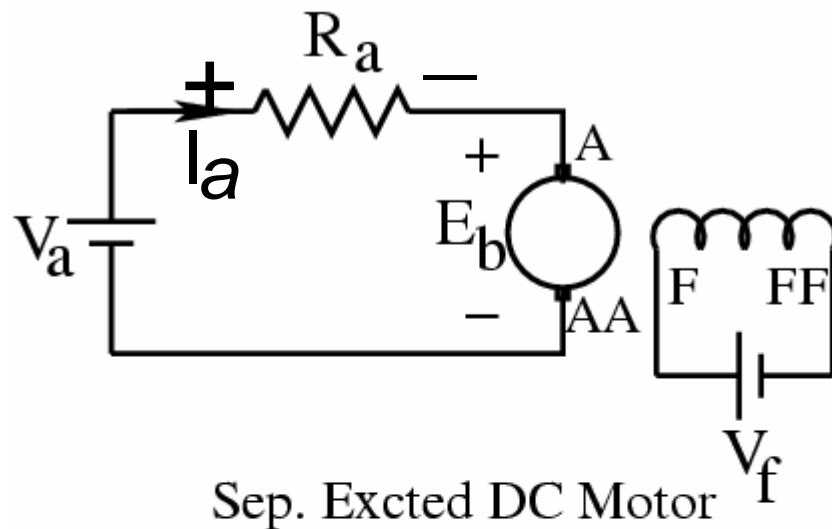
# Speed-Torque Characteristics

$$V_a = E_b + I_a R_a$$

$$E_b = K_e \Phi \omega$$

$$T = K_e \Phi I_a$$

$$\begin{aligned} \omega &= \frac{V}{K_e \phi} - \frac{R_a}{K_e \phi} I_a \\ &= \frac{V}{K_e \phi} - \frac{R_a}{(K_e \phi)^2} T \end{aligned}$$



# DC Machine: Torque vs. speed Characteristics

## For Sep. Excited Motor:

$$V_a = E_b + I_a R_a$$

$$E_b = K_e \Phi \omega$$

$$T = K_e \Phi I_a$$

$$\begin{aligned}\omega &= \frac{V}{K_e \Phi} - \frac{R_a}{K_e \Phi} I_a \\ &= \frac{V}{K_e \Phi} - \frac{R_a}{(K_e \Phi)^2} T\end{aligned}$$

$$K_e \Phi = K$$

$$\begin{aligned}\omega &= \frac{V_a}{K_e \Phi} - \\ &\quad \frac{R_a}{(K)^2} T\end{aligned}$$



## For Series Motor:

$$V_a = E_b + I_a R_a$$

$$E_b = K_e \Phi \omega$$

$$T = K_e \Phi I_a$$

$$\begin{aligned}\omega &= \frac{V}{K_e \Phi} - \frac{R_a}{K_e \Phi} I_a \\ &= \frac{V}{K_e \Phi} - \frac{R_a}{(K_e \Phi)^2} T\end{aligned}$$

$$\Phi = K_f I_a$$

$$\begin{aligned}\omega &= \frac{V_a}{\sqrt{K_e K_f} \sqrt{T}} \\ &\quad - \frac{R_a}{K_e K_f}\end{aligned}$$

# Speed – Torque Characteristic

