

Lecture 7: Steady State Errors

Note Title

28-02-2010

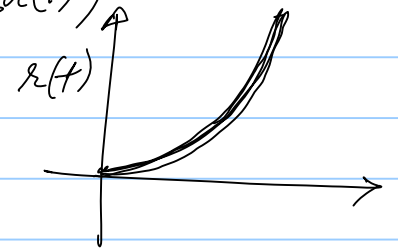
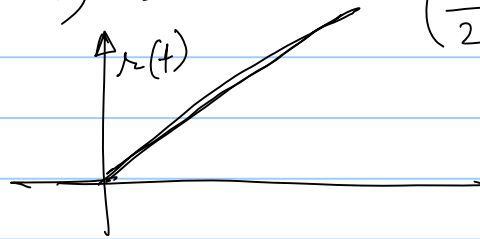
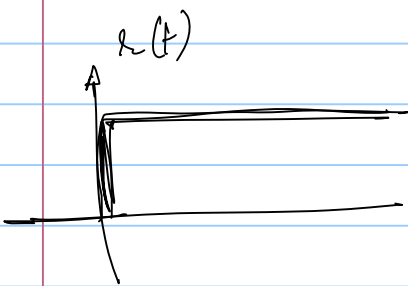
- Control Specs :
- 1) Transient Response ✓
 - 2) Stability ✓
 - 3) Steady State Errors ←

Def: Steady state error is the difference between input and output (for a particular test input) as $t \rightarrow \infty$

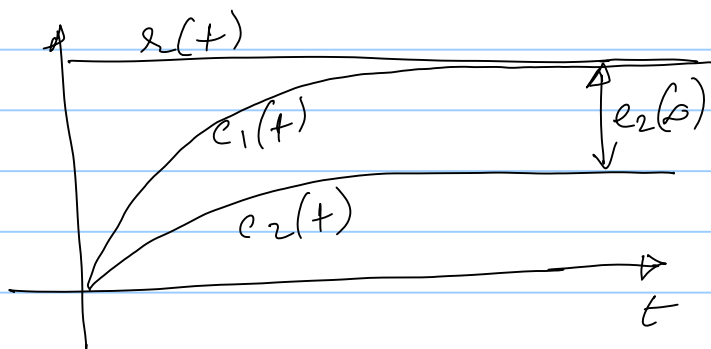
[NOTE: Stability is a system property (not defined in terms of any particular input)]

S.S.E. is defined for a particular I/P.

- Test inputs:
- 1) Step ($u(t)$) → ^{const.} position tracking
 - 2) Ramp ($t u(t)$) → ^{const.} velocity "
 - 3) Parabola ($\frac{t^2}{2} u(t)$) → ^{const.} acc. "

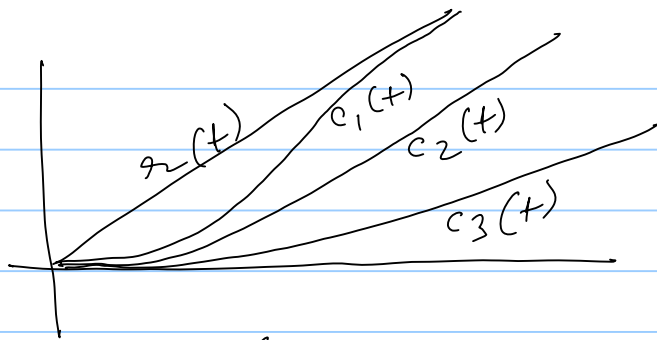


Assumption (Chap. wide): All systems are STABLE



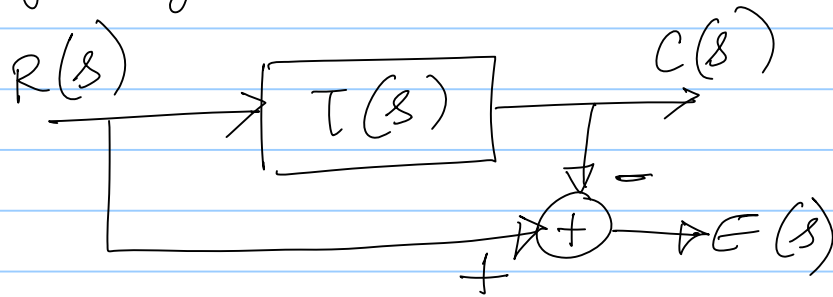
$$e_1(\infty) = r(\infty) - c_1(\infty) = 0$$
$$e_2(\infty) = r(\infty) - c_2(\infty)$$

S.S.E. for step input



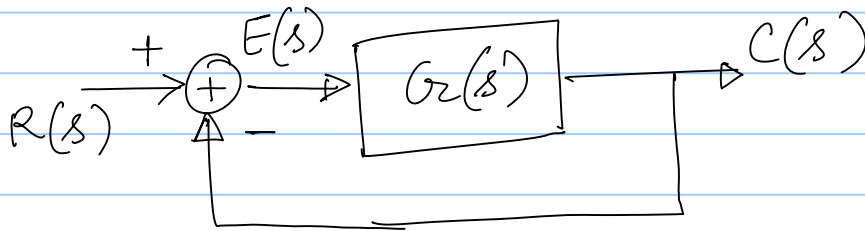
S.S.E for Ramp Input

S.S.E. for general T.F. : $T(s)$



$$\begin{aligned} \text{S.S.E} &= \lim_{t \rightarrow \infty} e(t) = \lim_{t \rightarrow \infty} [r_2(t) - c(t)] \\ &= \lim_{s \rightarrow 0} s [R(s) - C(s)] \\ &\quad (\text{by F.V. thm}) \end{aligned}$$

S.S.E. for Unity Feedback Config



For this config: $E(s) = R(s) - C(s)$
 $= \text{S.S.E. (by def)}^{\checkmark}$

If C.L. t.f. is $T(s)$ then $C(s) = T(s)R(s)$

Then $E(s) = R(s)[1 - T(s)]$

S.S.E. = $\lim_{t \rightarrow \infty} e(t) = \lim_{s \rightarrow 0} sE(s)$

or $\boxed{\text{S.S.E.} = \lim_{s \rightarrow 0} sR(s)[1 - T(s)]}$

$$\left. \begin{aligned} \text{Similarly, } E(s) &= R(s) - C(s) \\ \text{and } C(s) &= G(s)E(s) \end{aligned} \right\}$$

$$E(s) = \frac{R(s)}{1 + G(s)}$$

$$e(s) = \lim_{s \rightarrow 0} sE(s) = \lim_{s \rightarrow 0} \frac{sR(s)}{1 + G(s)} \quad (*)$$

Using (*) we can calculate $e(s)$ for any test signal for the unity feedback configuration.

Step Input: $R(s) = \frac{1}{s}$

$$e(s) = \lim_{s \rightarrow 0} \frac{s \cdot \frac{1}{s}}{1 + G(s)}$$

$$= \frac{1}{1 + \lim_{s \rightarrow 0} G(s)} = \frac{1}{1 + K_p}$$

$\underbrace{\lim_{s \rightarrow 0} G(s)}_{K_p}$

$K_p := \lim_{s \rightarrow 0} G(s) \equiv \text{Position Error Constant}$

* To make $e(s) = 0$, $K_p = \infty$ is required

i.e. $\lim_{s \rightarrow 0} G(s) = \infty$ is required.

$$\text{Let } G(s) = \frac{(s+z_1)(s+z_2) \dots}{s^n (s+p_1)(s+p_2) \dots}$$

$$\star \text{ For } \underline{n=0}, \lim_{s \rightarrow 0} G(s) = \frac{z_1 z_2 \dots}{p_1 p_2 \dots}$$

Hence, $e(\infty) \neq 0$

$$\star \text{ For } n \geq 1, \lim_{s \rightarrow 0} G(s) = \infty \Rightarrow e(\infty) = 0$$

FACT : The S.S.E. is zero for step input only when there are ≥ 1 integrators in the forward path (for unity feedback system)

Exercise: 1) Explain this intuitively.
2) What is the S.S.E for a pure gain in the forward path?

Ramp Input : $R(s) = \frac{1}{s^2}$

$$e(\infty) = \lim_{s \rightarrow 0} \frac{s \cdot \frac{1}{s^2}}{1 + G(s)} = \frac{1}{\lim_{s \rightarrow 0} s G(s)} = \frac{1}{K_v}$$

$K_v := \lim_{s \rightarrow 0} s G(s) =$: velocity error constant

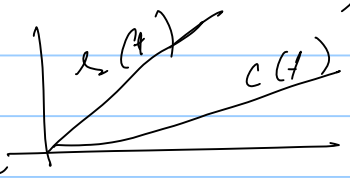
For $e(\infty) = 0$ we require $K_v = \lim_{s \rightarrow 0} s G(s) = \infty$

$$G(s) = \frac{(s+z_1)(s+z_2) \dots}{s^n (s+p_1)(s+p_2) \dots}$$

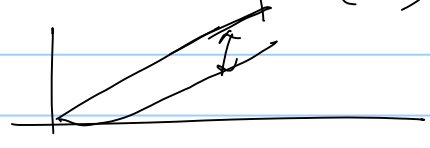
Strictly speaking this calculation is not valid. (F.V. thm is not applicable). However this is conventionally done since it gives correct answer.



* For $n=0$, $K_V = \lim_{s \rightarrow 0} s G(s) = 0 \Rightarrow e(\infty) = \infty$
(Diverging ramps)



* For $n=1$, $K_V = \lim_{s \rightarrow 0} s G(s) = \frac{z_1 z_2 \dots}{p_1 p_2 \dots}$
 $\Rightarrow 0 < |e(\infty)| < \infty$ (Finite error)



* For $n \geq 2$, $K_V = \lim_{s \rightarrow 0} s G(s) = \infty \Rightarrow e(\infty) = 0$

FACT: The S.S.E. for unit ramp is zero only when there are at least 2 integrators in the fwd. path.

Parabolic Input: $R(s) = \frac{1}{s^3}$

$$e(\infty) = \lim_{s \rightarrow 0} \frac{\frac{1}{s^3} \cdot s}{1 + G(s)} = \frac{1}{\lim_{s \rightarrow 0} s^2 G(s)} = \frac{1}{K_a}$$

$K_a := \lim_{s \rightarrow 0} s^2 G(s) =:$ Acceleration error constant

Clearly $n \geq 3 \Rightarrow e(\infty) = 0$

$n = 2 \Rightarrow 0 < |e(\infty)| < \infty$

$(n = 0, 1 \Rightarrow |e(\infty)| = \infty$

\hookrightarrow This calculation is also not strictly valid. (F.V. thm is not applicable)

System Type: Since S.S.E. for various test inputs depend on the no. of integrations in fwd. path systems are classified into "Types" accordingly.

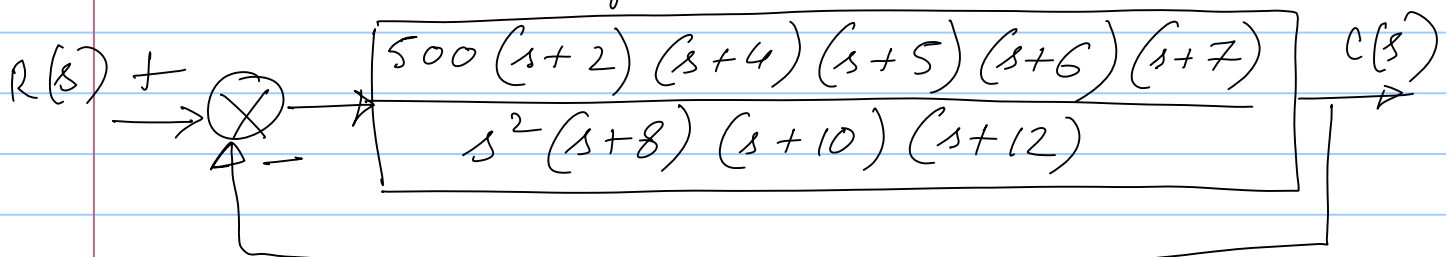
0 integrators $\Leftrightarrow (n=0) =: \text{Type '0'}$

1 integrators $\Leftrightarrow (n=1) =: \text{Type '1'}$

2 integrators $\Leftrightarrow (n=2) =: \text{Type '2'}$

Exercise: Read Table 7.2 [IMP]

Example: Find the static error constants and S.S.E. for step, ramp & parabolic I/P.



First verify stability: (Use MATLAB) \checkmark

$$K_p = \lim_{s \rightarrow 0} G(s) = \infty$$

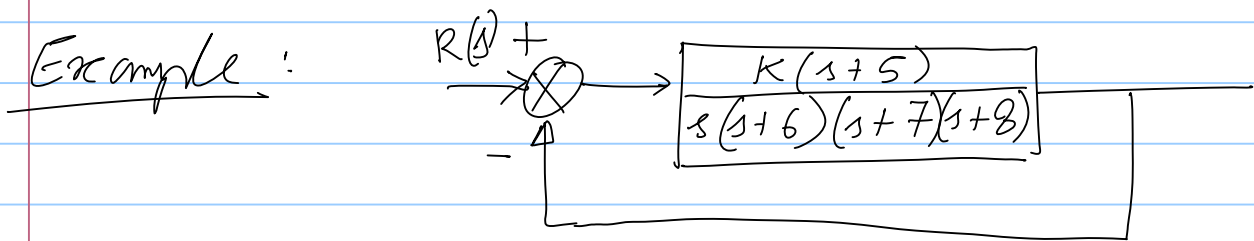
$$K_v = \lim_{s \rightarrow 0} sG(s) = \infty$$

$$K_a = \lim_{s \rightarrow 0} s^2 G(s) = \frac{500 \times 2 \times 4 \times 5 \times 6 \times 7}{8 \times 10 \times 12} = 875$$

$$\text{For } r(t) \equiv u(t), \quad e(\infty) = \frac{1}{1+K_p} = 0$$

$$r(t) = tu(t), \quad e(\infty) = \frac{1}{K_v} = 0$$

$$r(t) = \frac{1}{2} t^2 u(t), \quad e(\infty) = \frac{1}{K_a} = 1.14 \times 10^{-3}$$



Find K s.t. S.S.E. is 10%.

Type 1 system \rightarrow So S.S.E. spec must correspond to ramp input. (Ramp only yields finite error in Type 1)

$$e(\infty) = 0.1 = \frac{1}{\lim_{s \rightarrow 0} s G(s)} \quad \text{Type 1}$$

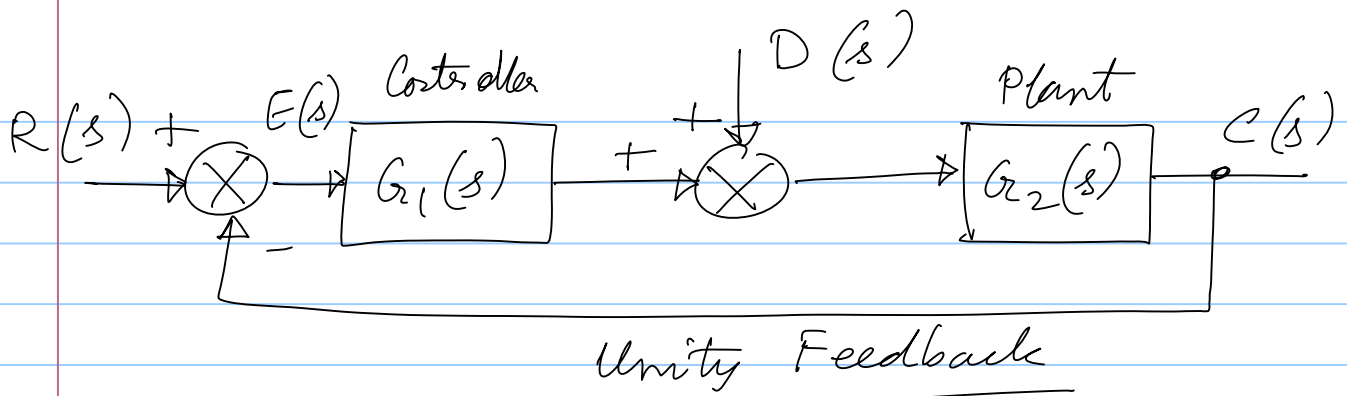
$$\text{i.e.} \quad \lim_{s \rightarrow 0} s G(s) = 10$$

$$\Rightarrow \frac{5K}{6 \times 7 \times 8} = 10 \Rightarrow K = 672$$

Exercise: 1) Is the system stable at this gain?
2) Can we meet transient response specs?

Steady State Error for Disturbances (Unity Feedback)

* Assumption: Disturbance is injected between controller & plant.



$$\begin{cases} C(s) = E(s) G_1(s) G_2(s) + D(s) G_2(s) \\ C(s) = R(s) - E(s) \end{cases}$$

Eliminating $C(s)$ yields:

$$E(s) = \frac{R(s)}{1 + G_1(s) G_2(s)} - \frac{G_2(s)}{1 + G_1(s) G_2(s)} D(s)$$

$$e(s) = \lim_{s \rightarrow 0} \frac{s R(s)}{1 + G_1(s) G_2(s)} - \lim_{s \rightarrow 0} \frac{s G_2(s) D(s)}{1 + G_1(s) G_2(s)}$$

$$= e_R(s) + e_D(s)$$

same as before

new term due to disturbance

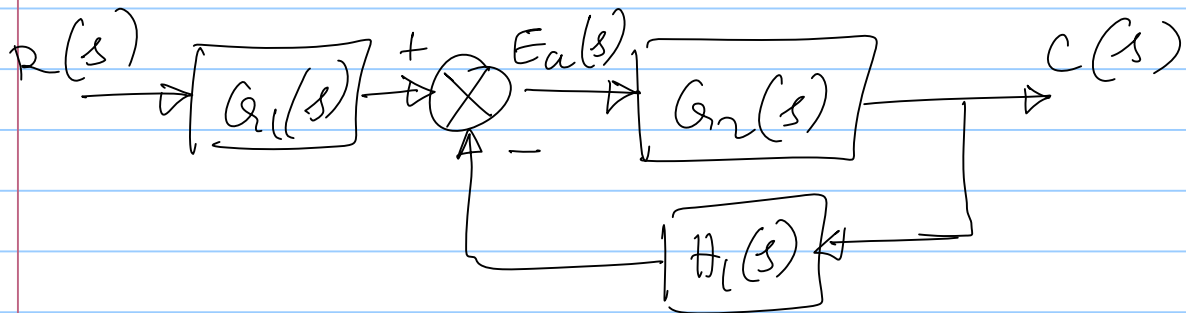
Step Disturbance : $D(s) = \frac{1}{s}$

$$e_D(s) = \lim_{s \rightarrow 0} \frac{-s G_2(s) \cdot \frac{1}{s}}{1 + G_1(s) G_2(s)}$$

$$= \frac{-1}{\left[\lim_{s \rightarrow 0} \frac{1}{G_2(s)} \right] + \left[\lim_{s \rightarrow 0} G_1(s) \right]}$$

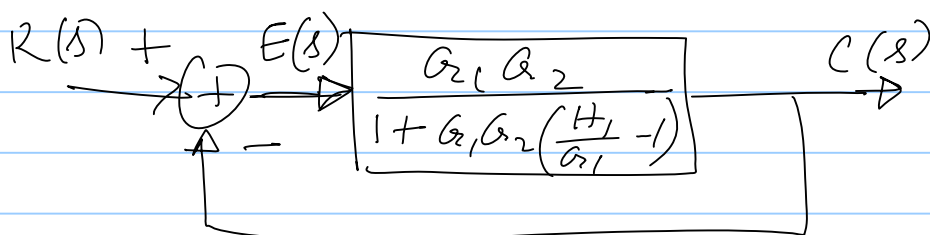
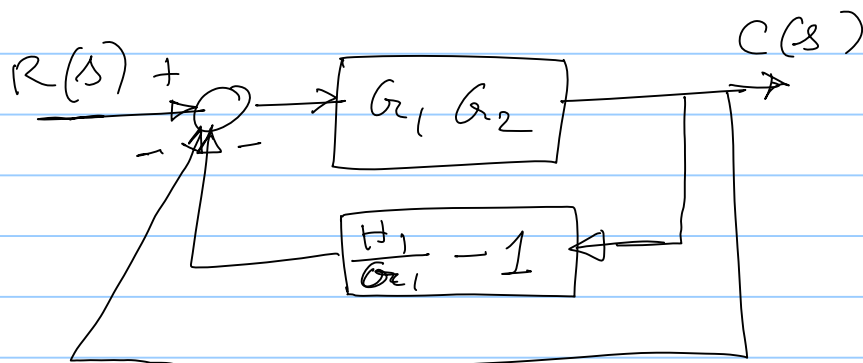
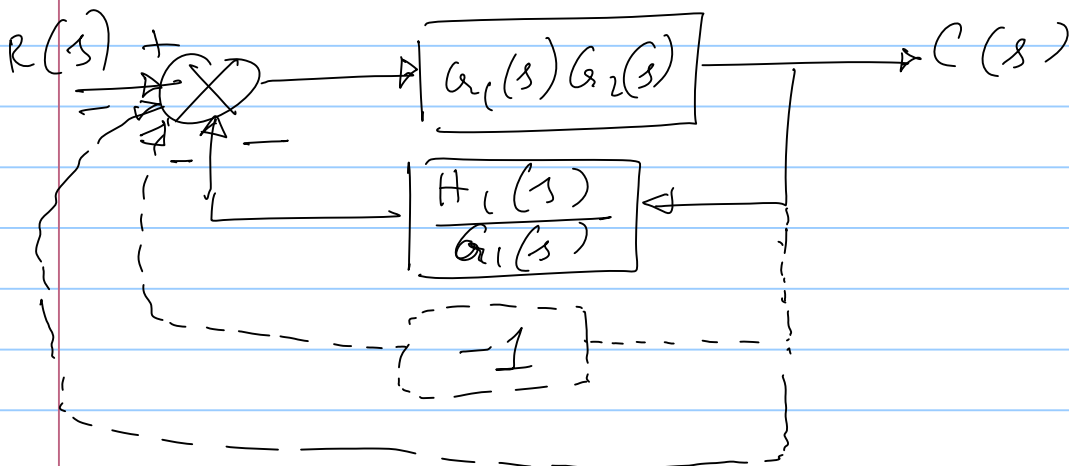
$$\Leftrightarrow e_D(s) \downarrow \text{ as } \lim_{s \rightarrow 0} G_2(s) \downarrow \quad \lim_{s \rightarrow 0} G_1(s) \uparrow$$

S.S.E. for Non-unity feedback systems

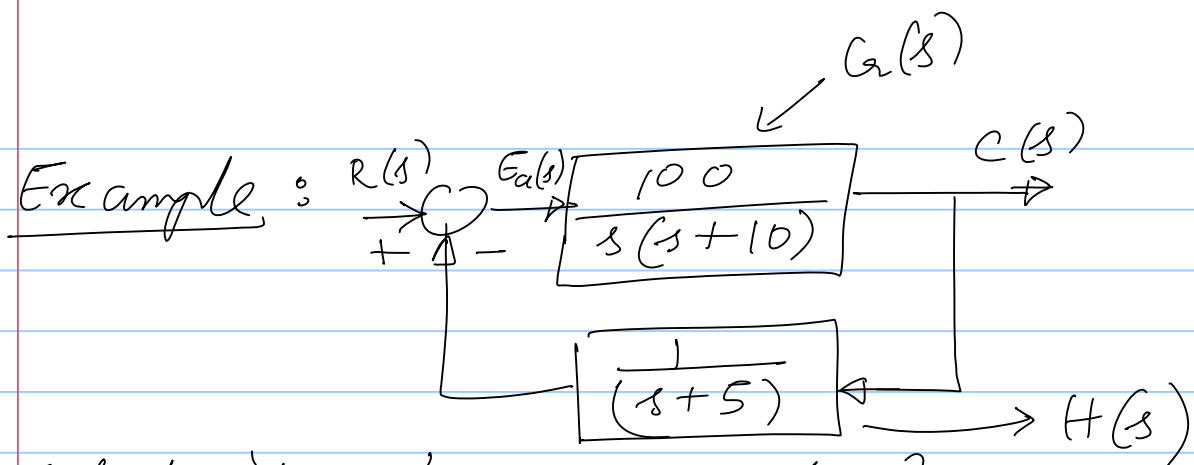


NOTE: $E_a(s)$ (= Actuating signal) is NOT the S.S.E.

We need to calculate, $E(s) = R(s) - C(s)$



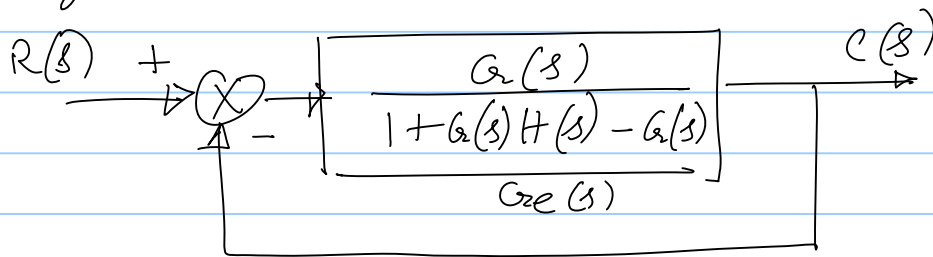
Then use the usual formulae.



- 1) What 'type' is the system?
- 2) Determine appropriate error constant
- 3) Determine S.S.E. for unit step.

First check stability ✓

Using the derivation done above,



$$G_{ee}(s) = \frac{G_c(s)}{1 + G_c(s)[H(s) - 1]} = \frac{100(s+5)}{s^3 + 15s^2 - 50s - 400}$$

System is Type '0'; $K_p = \lim_{s \rightarrow 0} G_{ee}(s)$
 $= -\frac{5}{4}$

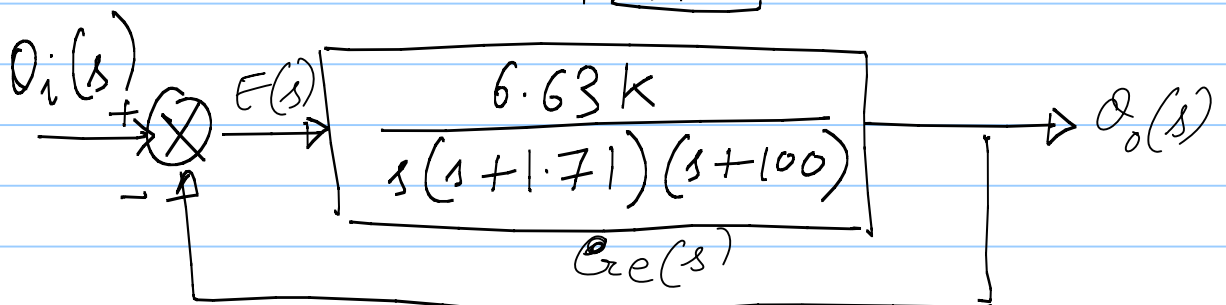
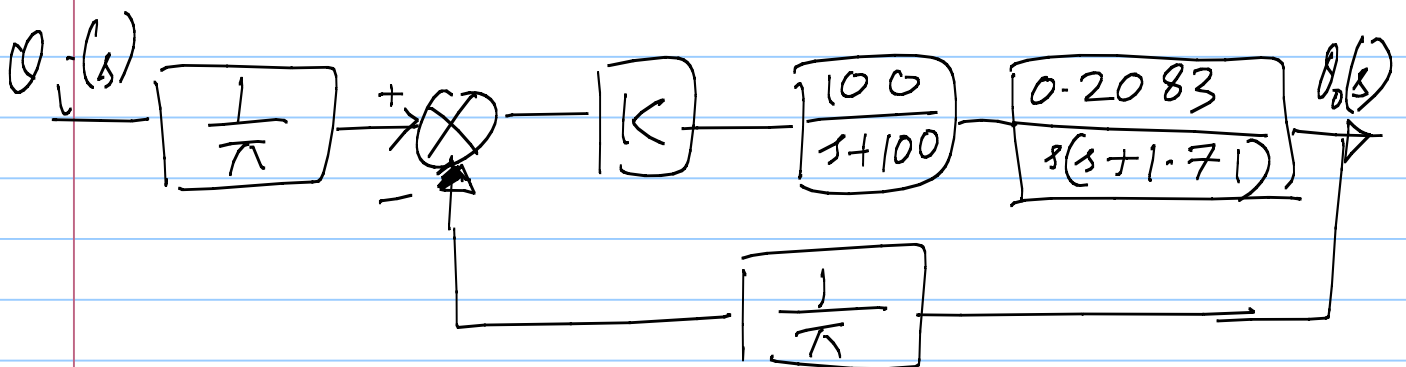
$$e(\infty) = \frac{1}{1 + K_p} = \frac{1}{1 - (5/4)} = -4 \quad (\text{O/P larger than I/P})$$

Steady - State Error for St. Sp. System

$$\begin{aligned} \dot{x} &= Ax + Br \\ y &= cx \end{aligned} \quad \left| \quad \begin{aligned} E(s) &= R(s) - Y(s) \\ &= R(s) - T(s)R(s) \\ &= R(s) [I - C(sI - A)^{-1}B] \end{aligned} \right.$$

$$\begin{aligned} e(s) &= \lim_{s \rightarrow 0} sE(s) \\ &= \lim_{s \rightarrow 0} sR(s) [I - C(sI - A)^{-1}B] \end{aligned}$$

Antenna Control: Steady-State Error Design



$$\text{S.S.E.} = \lim_{t \rightarrow \infty} [\theta_i(t) - \theta_o(t)] = e(\infty)$$

$$e(\infty) = \lim_{s \rightarrow 0} sE(s) = \lim_{s \rightarrow 0} \frac{s \theta_i(s)}{1 + G_e(s)}$$

Type 1: So $K_p = \lim_{s \rightarrow 0} G_e(s) = \infty$

$$\Rightarrow \text{Step Input} \rightarrow e(\infty) = 0$$

$$\text{Ramp Input} \rightarrow e(\infty) = \frac{1}{K_v} = \frac{25.79}{K}$$

Parabolic I/P $\rightarrow e(s) = \frac{1}{K_a} = \infty$

Suppose we want a 10% S.S. error for ramp I/P.

$$e(s) = 0.1 = \frac{1}{K_V} = \frac{25.79}{K} \Rightarrow K = 257.9$$

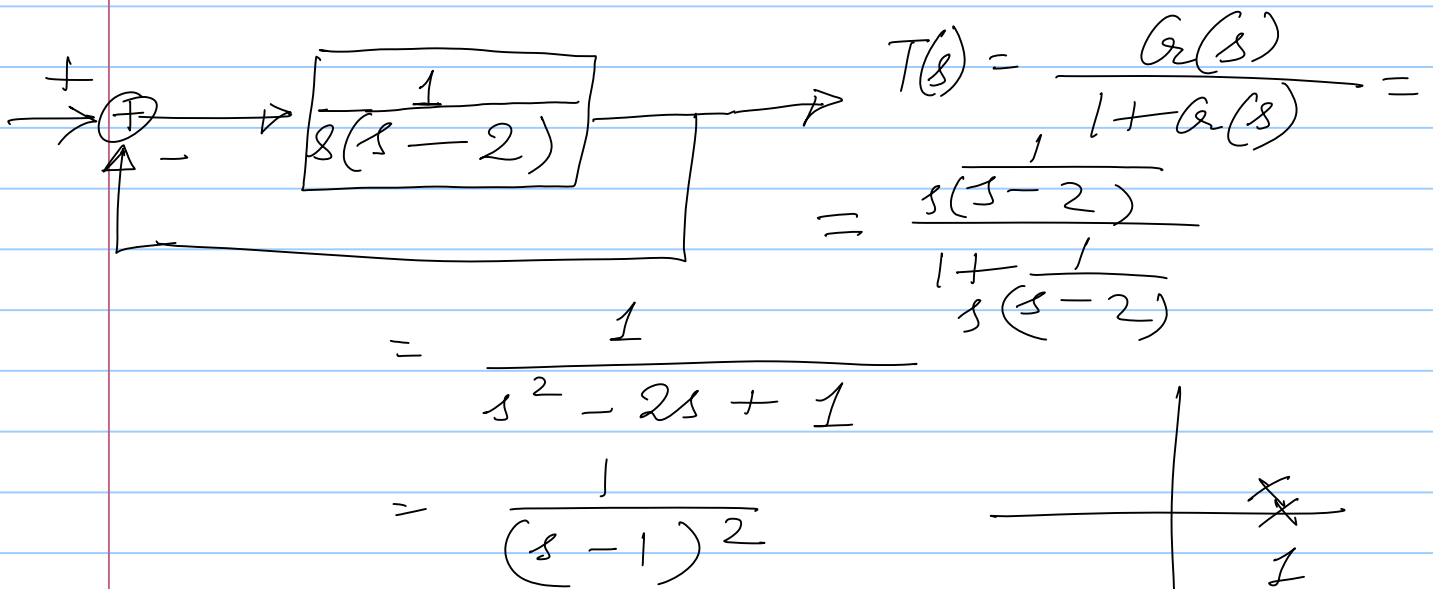
Using ROUTH-HURWITZ criterion, we found the range of stability for K : $0 < K < 2623$.

Hence $K = 257.9$ makes system stable.

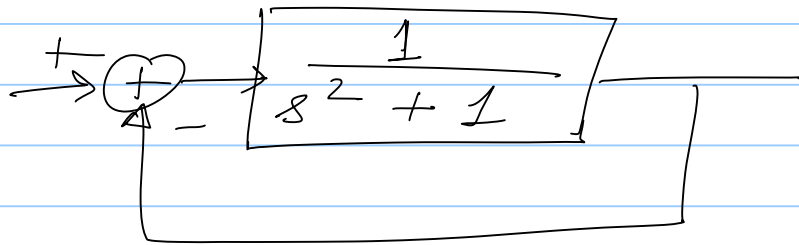
NOTE We need to check STABILITY explicitly before calculating SSE.

REASON : Our error calculations use F.V. value that which in turn is valid only if $sE(s)$ has poles on open LHP.

Requirement for stability



So for any input $R(s) = \frac{1}{s}, \frac{1}{s^2}, \frac{1}{s^3}$
 output diverges. No question of
 S.S.E.



$$T(s) = \frac{1}{s^2 + 2}$$

For unit step, $C(s) = \frac{1}{s^2 + 2} \cdot \frac{1}{s}$

$$= \frac{1}{2} \left[\frac{1}{s} - \frac{s}{s^2 + 2} \right]$$

$$= \left[\frac{1}{2} - \frac{1}{2} \cos \sqrt{2}t \right] u(t)$$

So $\lim_{t \rightarrow \infty} e(t)$ does not exist.

Exercise: Try to give an example
 where the system is
 unstable / marginally stable but
 still has finite s.s.e. for
 step / ramp / parabola.

Ans: