

OPTIMAL SINGULAR LQR PROBLEM: A PD FEEDBACK SOLUTION*

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Abstract. Unlike regular linear quadratic regulator (LQR) problems, singular LQR problems, in general, cannot be solved using a static state-feedback controller. This work is primarily focused on the design of feedback controllers which solve the singular LQR problem. We show that such problems can be solved using proportional-derivative (PD) state-feedback controllers. It is well known in the literature that the *maximal rank-minimizing* solution of the singular LQR linear matrix inequality (LMI) is pivotal in solving the singular LQR problem. In this paper, we first make use of this maximal rank-minimizing solution to compute the optimal trajectories. Then, we provide a PD feedback controller that restricts the trajectories of the closed-loop system to these optimal ones, and thus solves the singular LQR problem. While numerous solutions to this problem have been proposed over the course of the extensive research efforts in this field, a controller in the form of a PD state-feedback has been long sought after. Our approach is based on the notion of *weakly unobservable (slow)* and *strongly reachable (fast)* subspaces developed in [3]. But unlike [3], we employ these notions to the corresponding Hamiltonian system and not to the plant. This crucial extension of these well-known subspaces to the corresponding Hamiltonian system is key to the optimal PD feedback design that we propose in this paper. It is well-known that an optimal state feedback for the singular LQR problem does not exist; the limiting state feedback controller of the sub-optimal ones (high gain controllers) has unbounded coefficients as optimality is approached. We show in this paper that the limiting high gain controller is in fact a PD controller.

1. Introduction. In this paper, we provide a closed-loop solution for the singular case of the well-known infinite-horizon linear quadratic regulator (LQR) problem.

Problem 1.1. (Infinite-horizon LQR problem) Consider a stabilizable system with the state-space dynamics $\frac{d}{dt}x = Ax + Bu$, where $A \in \mathbb{R}^{n \times n}$, $B \in \mathbb{R}^{n \times m}$. Then, for every initial condition x_0 , find an input u that minimizes the functional

$$(1.1) \quad J(x_0, u) := \int_0^\infty \begin{bmatrix} x(t) \\ u(t) \end{bmatrix}^T \begin{bmatrix} Q & S \\ S^T & R \end{bmatrix} \begin{bmatrix} x(t) \\ u(t) \end{bmatrix} dt, \quad \text{with } \lim_{t \rightarrow \infty} x(t) = 0,$$

where $\begin{bmatrix} Q & S \\ S^T & R \end{bmatrix} \geq 0$, $Q \in \mathbb{R}^{n \times n}$, and $R \in \mathbb{R}^{m \times m}$.

For regular LQR problems, i.e., LQR problems with $R > 0$, the input u that minimizes $J(x_0, u)$ in equation (1.1) can be obtained using a static state-feedback constructed using the *maximal* solution of the algebraic Riccati equation (ARE):

$$(1.2) \quad A^T K + KA + Q - (KB + S)R^{-1}(B^T K + S^T) = 0.$$

Here, by a maximal solution K_{\max} , we mean that $K_{\max} - K \geq 0$ for any other arbitrary solution K of the ARE. If K_{\max} is the maximal solution of the ARE, then the LQR problem can be solved using the feedback law $u = Fx$, where $F := -R^{-1}(S^T + B^T K_{\max})$. Naturally, a singular LQR problem ($R \geq 0$ with $\det R = 0$) does not admit an ARE and cannot be solved using this feedback law due to singularity of R .

Singular LQR problem has been extensively studied over the past few decades (see, for example, the seminal paper [3]); but, a feedback solution that restricts the system to the optimal trajectories has remained largely elusive. Interestingly, [3] shows existence of a state-feedback controller for every regular relaxation of the problem, but, the limiting controller that is naively expected to work for the singular case fails to exist. Such controllers are known as high gain controllers, for their coefficients grow unbounded in the limit. A polynomial matrix based method for designing a

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47 PD feedback controller has been put forth in [4], but applicability of this result does
 48 not allow the initial condition to be free. It is also built on certain assumptions like
 49 controllability of (A, B) and observability of (Q, A) . In [5], the notion of deflating
 50 subspaces has been used to provide a linear implicit control law of the form $Px +$
 51 $Tu = 0$. But, most often this form does not lead to a feedback law, essentially due
 52 to non-invertibility of T (See [6] for the importance of feedback control). Another
 53 major drawback of this result is that it assumes the function space to be locally
 54 square-integrable. It is well known in the literature that the optimal trajectories
 55 for a singular LQR problem, in general, are impulsive in nature. Therefore, the
 56 local square-integrability of the signals is an extremely restrictive assumption, for the
 57 locally square-integrable functions cannot account for these impulses. Consideration
 58 of only square-integrable functions imposes a restriction on the initial condition of the
 59 system.

60 Yet another method of solving the singular LQR problem is via the solution of
 61 the constrained generalized continuous algebraic Riccati equations (CGCAREs) (see
 62 the recent papers [7], [8], [9]):

$$63 \quad (1.3) \quad A^T K + KA + Q - (KB + S)R^\dagger(B^T K + S^T) = 0 \text{ and } \ker(R) \subseteq \ker(S + KB),$$

64 where R^\dagger is the Moore-Penrose pseudo-inverse of R . However, it has been shown
 65 in [10] that solvability of CGCARE is equivalent to the corresponding Hamiltonian
 66 pencil satisfying a certain rank condition. Hence, CGCARE is generically unsolvable.
 67 Thus, in almost all cases of singular LQR problem, this method fails to provide a
 68 solution.

69 In this paper, we provide a method to design a proportional-derivative (PD) state-
 70 feedback controller that solves the singular LQR problem. While doing so, we do not
 71 put any restriction on the initial condition. Since the initial condition is arbitrary, the
 72 optimal trajectories, in general, are impulsive in nature. Hence, the function space
 73 assumed in this paper allows impulses.

74 The first step in computing the optimal solution is to compute the maximal rank-
 75 minimizing solution of the following LMI:

$$76 \quad (1.4) \quad \mathcal{L}(K) := \begin{bmatrix} A^T K + KA + Q & KB + S \\ B^T K + S^T & R \end{bmatrix} \geq 0.$$

78 We call inequality (1.4) the *LQR LMI*. Interestingly, for *every* LQR problem, the op-
 79 timal cost is given by $x_0^T K_{\max} x_0$, where K_{\max} is the maximal rank-minimizing solution
 80 of the LQR LMI (1.4), that is, $K_{\max} - K \geq 0$ and $\text{rank } \mathcal{L}(K_{\max}) \leq \text{rank } \mathcal{L}(K)$ for all
 81 K that satisfies $\mathcal{L}(K) \geq 0$ (see [11]). Hence, in order to compute the optimal cost of
 82 a general LQR problem, it is imperative that the maximal rank-minimizing solution
 83 of the LQR LMI (1.4) be computed. For regular LQR problems the maximal solution
 84 of the ARE given by equation (1.2) is, indeed, the maximal rank-minimizing solution
 85 (K_{\max}) of the LMI (1.4). For singular LQR problems, if the CGCARE is solvable then
 86 K_{\max} can be found by obtaining the maximal solution of the CGCARE (1.3); but, as
 87 has been mentioned before, CGCARE is generically unsolvable. There are numerous
 88 methods to compute the maximal solution of an ARE: see [12] for different methods.
 89 However, these methods cannot be used in the singular case due to nonexistence of
 90 an ARE. In [2] we showed that one of the methods to compute K_{\max} for an LQR
 91 LMI of the regular case can be extended to the singular case (see [13, Chapter 5] for
 92 the regular case). This method, for the regular case, is based on computing a suit-
 93 able eigenspace of the corresponding *Hamiltonian system*. A direct extension of this
 94 method to the singular case fails, since the dimension of the suitable eigenspace of
 95 the Hamiltonian system in such a case is less than what is required to compute K_{\max} .
 96 It has been shown [2] that the Hamiltonian system based method for the regular case
 97 can indeed be extended to the singular case by substituting the role of the eigenspace
 98 of the Hamiltonian system in the regular case by the subspaces namely the *weakly*

99 *unobservable subspace (slow space)* and the *strongly reachable subspace (fast space)* of
100 the Hamiltonian system. This observation is crucially used for the development of
101 our results. It is worthwhile to mention here that the idea of employing the notion of
102 slow space of the Hamiltonian in the context of the singular LQR problem has also
103 been used in [14], where the authors consider a special case of the problem, namely
104 the *cheap* LQR problem (where $R = 0$).

105 The paper is structured as follows: Section 2 consists of the notation and a
106 few preliminary results. The idea of weakly unobservable and strongly reachable
107 subspaces have been known to be crucial in singular LQR problems (see [3], [15], [16],
108 [17]). Matrix theoretic characterizations of the weakly unobservable and the strongly
109 reachable subspaces have been provided in [1] and [18], respectively. These works also
110 provide a method to compute the dimensions of these subspaces from the transfer
111 function matrix of the primal. For the sake of completeness we present the results
112 of [2], [1], and [18] in Section 3. In Section 4 we compute the optimal trajectories,
113 while Section 5 provides a PD state-feedback controller that restricts the system to
114 exhibit the optimal trajectories only. We provide an illustrative example in Section
115 7 to demonstrate the theory presented in this paper. A comparative analysis of this
116 result with the existing results in the literature has been carried out in Section 8.
117 Finally, Section 9 provides a few concluding remarks.

118 2. Notation and Preliminaries.

119 **2.1. Notation.** The symbols \mathbb{R} , \mathbb{C} , and \mathbb{N} are used for the sets of real numbers,
120 complex numbers, and natural numbers, respectively. We use the symbols \mathbb{R}_+ and
121 \mathbb{C}_- for the sets of non-negative real numbers and complex numbers with negative real
122 parts, respectively. The symbol $\mathbb{R}^{n \times p}$ denotes the set of $n \times p$ matrices with elements
123 from \mathbb{R} . We use the symbol I_n for an $n \times n$ identity matrix and the symbol $0_{n,m}$ for an
124 $n \times m$ matrix with all entries zero. Symbol $\text{col}(B_1, B_2, \dots, B_n)$ represents a matrix of
125 the form $[B_1^T \ B_2^T \ \dots \ B_n^T]^T$. By $\text{im } A$ and $\text{ker } A$ we denote the image and nullspace
126 of a matrix A , respectively. The symbols $\text{rank } A$ and $\text{nullity } A$ denote the rank and
127 the dimension of the nullspace of a matrix A , respectively. $\det(A)$ represents the
128 determinant of a square matrix A . We use the symbols $\text{deg}(p(s))$ and $\text{roots}(p(s))$ to
129 denote the degree and the set of roots (over complex numbers) of a polynomial $p(s)$
130 with real or complex coefficients (with a root λ included in the set as many times as
131 its multiplicity), respectively. The symbol $\text{num}(p(s))$ is used to denote the numerator
132 of a rational function $p(s)$. By $\text{degdet}(A(s))$ we denote the degree of the determinant
133 of a polynomial matrix $A(s)$ and by $\text{numdet}(A(s))$ we denote the numerator of the
134 determinant of a rational function matrix $A(s)$. The symbol $\sigma(A)$ denotes the set of
135 eigenvalues of a square matrix A (with an eigenvalue λ included in the set as many
136 times as its algebraic multiplicity). We use the symbol $\sigma(E, H)$ to denote the set
137 of eigenvalues of the matrix pencil (E, H) (with $\lambda \in \sigma(E, H)$ included in the set as
138 many times as its algebraic multiplicity). The symbol $|\Gamma|$ denotes the cardinality of a
139 set Γ (counted with multiplicity). We use the symbol $\sigma(A|_{\mathcal{S}})$ to represent the set of
140 eigenvalues of A restricted to an A -invariant subspace \mathcal{S} . We use the symbol $\dim(\mathcal{S})$
141 to denote the dimension of a space \mathcal{S} . The space of all infinitely often differentiable
142 functions and locally square-integrable functions from \mathbb{R} to \mathbb{R}^n are represented by the
143 symbol $\mathcal{C}^\infty(\mathbb{R}, \mathbb{R}^n)$ and $\mathcal{L}_{\text{loc}}^2(\mathbb{R}, \mathbb{R}^n)$, respectively. We use the symbol $\mathcal{C}^\infty(\mathbb{R}, \mathbb{R}^n)|_{\mathbb{R}_+}$
144 to represent the set of all functions from \mathbb{R}_+ to \mathbb{R}^n that are restrictions of $\mathcal{C}^\infty(\mathbb{R}, \mathbb{R}^n)$
145 functions to \mathbb{R}_+ . The symbol δ represents the Dirac delta impulse distribution and
146 $\delta^{(i)}$ represents the i -th distributional derivative of δ with respect to t .

147 **2.2. Weakly unobservable and strongly reachable subspaces.** Consider a
148 system described by $\frac{d}{dt}x = Ax + Bu$ and $y = Cx + Du$, where $A \in \mathbb{R}^{n \times n}$, $B \in \mathbb{R}^{n \times m}$,
149 $C \in \mathbb{R}^{p \times n}$ and $D \in \mathbb{R}^{p \times m}$. Associated with such a system are two important subspaces
150 called the weakly unobservable subspace and the strongly reachable subspace (see [3])

151 for more on these spaces). Before we delve into the definitions of these subspaces, we
 152 need to define the space of impulsive-smooth distributions (see [3], [17]).

153 DEFINITION 2.1. *The set of impulsive-smooth distributions $\mathfrak{C}_{\text{imp}}^w$ is defined as:*

$$154 \mathfrak{C}_{\text{imp}}^w := \left\{ f = f_{\text{reg}} + f_{\text{imp}} \mid f_{\text{reg}} \in \mathfrak{C}^\infty(\mathbb{R}, \mathbb{R}^w)|_{\mathbb{R}_+} \text{ and } f_{\text{imp}} = \sum_{i=0}^k a_i \delta^{(i)}, \text{ with } a_i \in \mathbb{R}^w, k \in \mathbb{N} \right\}.$$

155

156 In what follows, we denote the state-trajectory x and output-trajectory y of the
 157 system, that result from initial condition x_0 and input u , using the symbols $x(t; x_0, u)$
 158 and $y(t; x_0, u)$, respectively. $x(0^+; x_0, u)$ denotes the value of the state-trajectory that
 159 can be reached from x_0 instantaneously on application of the input u at $t = 0$.

160 DEFINITION 2.2. *A state $x_0 \in \mathbb{R}^n$ is called weakly unobservable if there exists*
 161 *an input $u \in \mathfrak{C}^\infty(\mathbb{R}, \mathbb{R}^m)|_{\mathbb{R}_+}$ such that $y(t; x_0, u) \equiv 0$ for all $t \geq 0$. The collection of*
 162 *all such weakly unobservable states is called the weakly unobservable subspace of the*
 163 *system and is denoted by \mathcal{O}_w .*

164 The other space of interest is the space of strongly reachable states (see [3]).

165 DEFINITION 2.3. *A state $x_1 \in \mathbb{R}^n$ is called strongly reachable (from the origin) if*
 166 *there exists an input $u \in \mathfrak{C}_{\text{imp}}^m$ such that $x(0^+; 0, u) = x_1$ and $y(t; 0, u) \in \mathfrak{C}^\infty(\mathbb{R}, \mathbb{R}^p)|_{\mathbb{R}_+}$*
 167 *(that is, the output is regular). The collection of all such strongly reachable states is*
 168 *called the strongly reachable subspace of the state-space and is denoted by \mathcal{R}_s .*

169 Since \mathcal{O}_w deals with inputs from the space of infinitely differentiable functions, we
 170 call \mathcal{O}_w the *slow space* of the system. On the other hand, since the space \mathcal{R}_s admits
 171 impulsive inputs, we call \mathcal{R}_s the *fast space* of the system. Further, by [3, Theorem
 172 3.10] we know that \mathcal{O}_w is the largest among the subspaces \mathcal{V} for which there exists
 173 an $F_{\mathcal{V}} \in \mathbb{R}^{m \times n}$ such that

$$174 (2.1) \quad (A + BF_{\mathcal{V}})\mathcal{V} \subseteq \mathcal{V} \text{ and } (C + DF_{\mathcal{V}})\mathcal{V} = \{0\}.$$

176 In other words, there exists $F_{\mathcal{O}_w} \in \mathbb{R}^{m \times n}$ such that \mathcal{O}_w satisfies the above equation;
 177 and for any arbitrary subspace \mathcal{V} that satisfies the above equation, we must have
 178 that $\mathcal{V} \subseteq \mathcal{O}_w$. Note that, the class of subspaces that satisfy equation (2.1) also
 179 admits a subspace \mathcal{O}_{wg} such that $\sigma((A + BF_{\mathcal{O}_{wg}})|_{\mathcal{O}_{wg}}) \subseteq \mathbb{C}_-$; and $\mathcal{V} \subseteq \mathcal{O}_{wg}$ whenever
 180 $\sigma((A + BF_{\mathcal{V}})|_{\mathcal{V}}) \subseteq \mathbb{C}_-$. (see [19, Chapter 4, Chapter 5] for more on this). We call
 181 such a space the *good slow space* of the system as defined below (see [20, Chapter 3]).

182 DEFINITION 2.4. *The good slow space \mathcal{O}_{wg} is the largest subspace \mathcal{V} of the state-*
 183 *space for which there exists a feedback $F_{\mathcal{V}} \in \mathbb{R}^{m \times n}$ such that*

$$184 (A + BF_{\mathcal{V}})\mathcal{V} \subseteq \mathcal{V}, (C + DF_{\mathcal{V}})\mathcal{V} = \{0\}, \text{ and } \sigma((A + BF_{\mathcal{V}})|_{\mathcal{V}}) \subseteq \mathbb{C}_-.$$

185 **2.3. Alternative formulation of the singular LQR problem.** Recall from
 186 Problem 1.1 that $R \geq 0$. Therefore, there exists an orthogonal matrix $U \in \mathbb{R}^{m \times m}$ such
 187 that $U^T R U = \text{diag}(0, \hat{R})$, where $\hat{R} \in \mathbb{R}^{r \times r}$ and $r := \text{rank } R$. Notice that $\hat{R} > 0$. This
 188 transformation enables us to provide an alternative formulation of the singular LQR
 189 Problem 1.1, which separates the regular part from the singular part of the problem.
 190 The following lemma is crucial for this purpose.

191 LEMMA 2.5. *Consider the singular LQR Problem 1.1, where $\text{rank } R = r$. Let*
 192 *$U \in \mathbb{R}^{m \times m}$ be an orthogonal matrix such that $U^T R U = \text{diag}(0, \hat{R})$, where $\hat{R} \in \mathbb{R}^{r \times r}$*
 193 *and $\hat{R} > 0$. Define $B U =: [B_1 \ B_2]$ and $S U =: [S_1 \ S_2]$, where $B_2, S_2 \in \mathbb{R}^{n \times r}$.*
 194 *Then, the following statements hold:*

$$195 \quad 1. \quad \begin{bmatrix} Q & S \\ S^T & R \end{bmatrix} \geq 0 \text{ if and only if } S_1 = 0, Q - S_2 \hat{R}^{-1} S_2^T \geq 0.$$

196 2. u^* is a solution to the singular LQR Problem 1.1 if and only if $U^T u^* :=$
 197 $\text{col}(u_1^*, u_2^*)$ minimizes

$$198 \quad (2.2) \quad J(x_0, u) := \int_0^\infty \begin{bmatrix} x \\ u_1 \\ u_2 \end{bmatrix}^T \begin{bmatrix} Q & 0 & S_2 \\ 0 & 0 & 0 \\ S_2^T & 0 & \hat{R} \end{bmatrix} \begin{bmatrix} x \\ u_1 \\ u_2 \end{bmatrix} dt.$$

200 3. $K = K^T$ satisfies $\mathcal{L}(K) \geq 0$ (equation 1.4) if and only if K satisfies the LMI:

$$201 \quad (2.3) \quad \mathcal{L}_t(K) := \begin{bmatrix} A^T K + K A + Q & K B_1 & K B_2 + S_2 \\ B_1^T K & 0 & 0 \\ B_2^T K + S_2^T & 0 & \hat{R} \end{bmatrix} \geq 0.$$

203 4. K_{\max} is the maximal rank-minimizing solution of the LQR LMI (1.4) if and
 204 only if K_{\max} is the maximal rank-minimizing solution of the LMI (2.3).

205 *Proof* Statement 1 and Statement 2 follow directly from [10, Lemma 2.1].

206 3. Define the orthogonal matrix $\hat{U} := \text{diag}(I_n, U)$. From the assumptions and State-
 207 ment 1 of this lemma, it can be verified that $\hat{U}^T \mathcal{L}(K) \hat{U} = \mathcal{L}_t(K)$. Thus $\mathcal{L}(K) \geq 0$ if
 208 and only if $\mathcal{L}_t(K) \geq 0$. This proves Statement 3.

209 4. $\hat{U}^T \mathcal{L}(K) \hat{U} = \mathcal{L}_t(K) \Rightarrow \text{rank } \mathcal{L}(K) = \text{rank } \mathcal{L}_t(K)$. Also, from Statement 3 of this
 210 lemma we know that the solution sets of the LMIs $\mathcal{L}(K) \geq 0$ and $\mathcal{L}_t(K) \geq 0$ are
 211 equal. Thus, K_{\max} is the maximal rank-minimizing solution of the LQR LMI (1.4) if
 212 and only if K_{\max} is the maximal rank-minimizing solution of the LMI (2.3). \square

213 Notice that the LMI (2.3) is the LQR LMI corresponding to the singular LQR prob-
 214 lem that minimizes the objective function given by equation (2.2). Therefore, Lemma
 215 2.5 allows us to write any singular LQR problem as follows:

216 **Problem 2.6.** Let $Q \in \mathbb{R}^{n \times n}$, $S_2 \in \mathbb{R}^{n \times r}$, and $\hat{R} \in \mathbb{R}^{r \times r}$ be such that $\hat{R} > 0$
 217 and $\begin{bmatrix} Q & 0 & S_2 \\ 0 & 0_{d,d} & 0 \\ S_2^T & 0 & \hat{R} \end{bmatrix} \geq 0$, where $d := m - r$. Consider a stabilizable system with state-
 218 space dynamics $\frac{d}{dt}x = Ax + B_1 u_1 + B_2 u_2$, where $A \in \mathbb{R}^{n \times n}$, $B_1 \in \mathbb{R}^{n \times d}$, and $B_2 \in$
 219 $\mathbb{R}^{n \times r}$. Then, for every initial condition x_0 , find an input $u := \text{col}(u_1, u_2)$ such that
 220 $\lim_{t \rightarrow \infty} x(t) = 0$ and u minimizes the functional (2.2).

221 This reduction of the original singular LQR problem (Problem 1.1) to its equivalent
 222 Problem 2.6 plays a crucial role in the sequel, where we exploit the special structure
 223 of the matrices involved in Problem 2.6 to obtain the main results.

224 **2.4. The primal and the Hamiltonian.** Suppose $p := \text{rank} \begin{bmatrix} Q & 0 & S_2 \\ 0 & 0 & 0 \\ S_2^T & 0 & \hat{R} \end{bmatrix}$. This
 225 matrix being positive semi-definite, admits a factorization given by $\begin{bmatrix} Q & 0 & S_2 \\ 0 & 0 & 0 \\ S_2^T & 0 & \hat{R} \end{bmatrix} =$
 226 $[C \ 0 \ D_2]^T [C \ 0 \ D_2]$, where $C \in \mathbb{R}^{p \times n}$, and $D_2 \in \mathbb{R}^{p \times r}$. Using this factorization in
 227 equation (2.2), it can be easily seen that the singular LQR Problem 2.6 can be viewed as
 228 an output energy minimization problem of the system Σ defined as follows:

$$229 \quad (2.4) \quad \Sigma : \quad \frac{d}{dt}x = Ax + B_1 u_1 + B_2 u_2 \text{ and } y = Cx + D_2 u_2.$$

230 We call the system Σ the *primal* for the given singular LQR Problem 2.6.

231 **REMARK 2.7.** The optimal trajectories for the singular LQR problem are impul-
 232 sive. Therefore, in this paper we consider the trajectory space $\mathfrak{C}_{\text{imp}}^m$ (see Definition
 233 2.1) which allows impulses in trajectories. By equation (2.2) it can be inferred that
 234 in order for the objective function to be well-defined, the output $y(t)$ of the primal
 235 must be regular. Hence, while searching for an optimal input from the space $\mathfrak{C}_{\text{imp}}^m$, it
 236 suffices to restrict our search to the inputs which cause the output $y(t)$ to be regular.
 237 We call such inputs the *admissible inputs*. \square

238 By Pontryagin's maximum principle, all the smooth optimal trajectories of Prob-
 239 lem 2.6 must necessarily be a trajectory of the following singular descriptor system:
 240

$$241 \quad (2.5) \quad \underbrace{\begin{bmatrix} I_n & 0 & 0 & 0 \\ 0 & I_n & 0 & 0 \\ 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 \end{bmatrix}}_E \frac{d}{dt} \begin{bmatrix} x \\ z \\ u_1 \\ u_2 \end{bmatrix} = \underbrace{\begin{bmatrix} A & 0 & B_1 & B_2 \\ -Q & -A^T & 0 & -S_2 \\ 0 & B_1^T & 0 & 0 \\ S_2^T & B_2^T & 0 & \hat{R} \end{bmatrix}}_H \begin{bmatrix} x \\ z \\ u_1 \\ u_2 \end{bmatrix},$$

242

243 where $\text{col}(x, z)$ is the state-costate pair. The system described by equation (2.5) is
 244 known in the literature as the *Hamiltonian* system corresponding to the LQR Prob-
 245 lem 2.6 and the matrix pair (E, H) is known as the Hamiltonian matrix pair. The
 246 Hamiltonian system admits an output-nulling representation given by

$$247 \quad (2.6) \quad \frac{d}{dt} \begin{bmatrix} x \\ z \end{bmatrix} = \hat{A} \begin{bmatrix} x \\ z \end{bmatrix} + \hat{B} \begin{bmatrix} u_1 \\ u_2 \end{bmatrix} \quad \text{and} \quad 0 = \hat{C} \begin{bmatrix} x \\ z \end{bmatrix} + \hat{D} \begin{bmatrix} u_1 \\ u_2 \end{bmatrix},$$

248 where $\hat{A} := \begin{bmatrix} A & 0 \\ -Q & -A^T \end{bmatrix}$, $\hat{B} := \begin{bmatrix} B_1 & B_2 \\ 0 & -S_2 \end{bmatrix}$, $\hat{C} := \begin{bmatrix} 0 & B_1^T \\ S_2^T & B_2^T \end{bmatrix}$, and $\hat{D} := \begin{bmatrix} 0 & 0 \\ 0 & \hat{R} \end{bmatrix}$.

249 In this paper we show that not only the smooth optimal trajectories, but also the
 250 distributional ones must necessarily satisfy the Hamiltonian system's equation.

251 Due to non-singularity of \hat{R} , we can further reduce the Hamiltonian system to
 252 obtain an equivalent system described by the following differential algebraic equations:

$$253 \quad (2.7) \quad \underbrace{\begin{bmatrix} I_n & 0 & 0 \\ 0 & I_n & 0 \\ 0 & 0 & 0 \end{bmatrix}}_{E_r} \frac{d}{dt} \begin{bmatrix} x \\ z \\ u_1 \end{bmatrix} = \underbrace{\begin{bmatrix} A - B_2 \hat{R}^{-1} S_2^T & -B_2 \hat{R}^{-1} B_2^T & B_1 \\ -Q + S_2 \hat{R}^{-1} S_2^T & -(A - B_2 \hat{R}^{-1} S_2^T)^T & 0 \\ 0 & B_1^T & 0 \end{bmatrix}}_{H_r} \begin{bmatrix} x \\ z \\ u_1 \end{bmatrix}.$$

254

255 We call the system described by equation (2.7), the *reduced Hamiltonian system*, and
 256 the pair (E_r, H_r) the *reduced Hamiltonian matrix pair*. The reduced Hamiltonian
 257 system admits an output-nulling representation Σ_{Ham} as follows:

$$258 \quad (2.8) \quad \frac{d}{dt} \begin{bmatrix} x \\ z \end{bmatrix} = \begin{bmatrix} A_r & -L \\ -Q_r & -A_r^T \end{bmatrix} \begin{bmatrix} x \\ z \end{bmatrix} + \begin{bmatrix} B_r \\ 0 \end{bmatrix} u_1 \quad \text{and} \quad 0 = \begin{bmatrix} 0 & B_r^T \end{bmatrix} \begin{bmatrix} x \\ z \end{bmatrix},$$

259

260 where $A_r := A - B_2 \hat{R}^{-1} S_2^T$, $Q_r := Q - S_2 \hat{R}^{-1} S_2^T$, $L := B_2 \hat{R}^{-1} B_2^T$, and $B_r := B_1$.
 261 The reduced Hamiltonian system and the Hamiltonian system are equivalent in the
 262 sense that $\text{col}(x, z, u_1)$ is a trajectory of the reduced Hamiltonian system if and only
 263 if $\text{col}(x, z, u_1, -\hat{R}^{-1}(S_2^T x + B_2^T z))$ is a trajectory of the Hamiltonian system. But,
 264 it is easier to carry out the analysis using the reduced Hamiltonian system. We
 265 characterize the slow space and the fast space in terms of the reduced Hamiltonian
 266 system, which finally leads to the maximal rank-minimizing solution of the LQR LMI.

267 The following lemma establishes a few important relations between the primal
 268 and the Hamiltonian (see [21, Lemma 4.4]).

269 LEMMA 2.8. Consider the primal Σ , the Hamiltonian matrix pair (E, H) , the
 270 reduced Hamiltonian matrix pair (E_r, H_r) , and the matrices $\hat{A}, \hat{B}, \hat{C}, \hat{D}$ defined in
 271 equation (2.4), equation (2.5), equation (2.7), and equation (2.6), respectively. Define
 272 $G(s) := C(sI_n - A)^{-1} \begin{bmatrix} B_1 & B_2 \end{bmatrix} + \begin{bmatrix} 0 & D_2 \end{bmatrix}$. Then the following statements hold:

- 273 1. $G(-s)^T G(s) = \hat{C}(sI_{2n} - \hat{A})^{-1} \hat{B} + \hat{D}$.
- 274 2. $\text{numdet}(G(-s)^T G(s))^1 = \det(sE - H) = (-1)^r \det \hat{R} \times \det(sE_r - H_r)$.

¹Here by $\text{numdet}(G(-s)^T G(s))$, we mean the numerator of $\det(G(-s)^T G(s))$ before any possible pole-zero cancellations.

275 REMARK 2.9. Throughout this paper, we assume that (i) $(sE_r - H_r)$ is a regular
276 matrix pencil, that is, $\det(sE_r - H_r) \neq 0$; and (ii) $\sigma(E_r, H_r) \cap j\mathbb{R} = \emptyset$. The assumption
277 that $\det(sE_r - H_r) \neq 0$ is a standard assumption in the literature. It means that
278 the Hamiltonian system is autonomous and ensures that, for a given initial condition,
279 the optimal trajectory is unique. It has been shown in [10] that for singular LQR
280 problems, the condition $\det(sE_r - H_r) \neq 0$ is generically satisfied. Therefore, this
281 assumption is not restrictive. From Statement 2 of Lemma 2.8, it follows that the
282 condition $\det(sE_r - H_r) \neq 0$ is equivalent to the transfer function matrix $G(s)$ of the
283 primal Σ being left-invertible. So, in terms of the primal Σ , this assumption translates
284 to the primal Σ being a left-invertible system (see [3, Theorem 3.26]). See [22] for the
285 case when the primal is not a left-invertible system.

286 Since the primal Σ is assumed to be stabilizable, from Statement 2 of Lemma
287 2.8, it follows that the assumption $\sigma(E_r, H_r) \cap j\mathbb{R} = \emptyset$ is equivalent to saying that:
288 (a) the primal Σ does not have any unobservable eigenvalue on the imaginary axis,
289 and (b) the primal has no transmission zeros on the imaginary axis. Note that, this
290 assumption, too, is not restrictive, because the property that a polynomial has no
291 root on the imaginary axis is generically satisfied. This assumption also is a standard
292 assumption in the literature (see [14], [17]).

293 Due to Statement 2 of Lemma 2.8 we further infer that if λ is a root of $\det(sE_r -$
294 $H_r)$ (that is, $\lambda \in \sigma(E_r, H_r)$), then $-\lambda$, too, is a root of the same. Of course, the
295 roots also appear in complex conjugate pairs. Therefore, the roots are symmetric
296 about the origin. Consequently, $\det(sE_r - H_r)$ is an even-degree polynomial. Hence,
297 for a singular LQR problem $\text{degdet}(sE_r - H_r) =: 2\mathbf{n}_s$, where $\mathbf{n}_s < \mathbf{n}$ (because \widehat{D}
298 is singular). Hence, the assumption that $\sigma(E_r, H_r) \cap j\mathbb{R} = \emptyset$ further implies that
299 $|\sigma(E_r, H_r) \cap \mathbb{C}_-| = \mathbf{n}_s$. \square

300 For a quick reference, in Table 1 we have listed some matrices and numbers that have
been frequently used throughout this paper.

Matrix/Number	Definition	Remark
A_r	$A_r := A - B_2 \widehat{R}^{-1} S_2^T$	Defined in equation (2.8).
B_r	$B_r := B_1$	
L	$L := B_2 \widehat{R}^{-1} B_2^T$	
Q_r	$Q_r := Q - S_2 \widehat{R}^{-1} S_2^T$	Defined in Lemma 3.2. Notice that $C_r^T C_r = Q_r$.
C_r	$C_r := C - D_2 \widehat{R}^{-1} S_2^T$	
\mathbf{r} and \mathbf{d}	$\mathbf{r} := \text{rank } R$ and $\mathbf{d} := \text{nullity } R$	Notice that $\mathbf{d} = \mathbf{m} - \mathbf{r}$.
E_r	$E_r := \begin{bmatrix} I_{\mathbf{n}} & 0 & 0 \\ 0 & I_{\mathbf{n}} & 0 \\ 0 & 0 & 0_{\mathbf{d}, \mathbf{d}} \end{bmatrix}$	(E_r, H_r) is the reduced Hamiltonian matrix pair defined in equation (2.7).
H_r	$H_r := \begin{bmatrix} A_r & -L & B_r \\ -Q_r & -A_r^T & 0 \\ 0 & B_r^T & 0 \end{bmatrix}$	
\mathbf{n}_s and \mathbf{n}_f	$2\mathbf{n}_s := \text{degdet}(sE_r - H_r)$ and $\mathbf{n}_f := \mathbf{n} - \mathbf{n}_s$	See Remark 2.9 and Lemma 3.2.

TABLE 1
Definitions of some matrices and numbers for a quick reference

302 **3. Constructive solution of the singular LQR LMI.** In this section we first
303 provide a characterization of the good slow space of the Hamiltonian system. Then,
304 we present a characterization of the fast space of the primal. We also depict how to
305 get the dimensions of these spaces from the transfer function matrix of the primal.

306 Finally, we construct the maximal rank-minimizing solution of the LQR LMI 2.3 using
 307 these subspaces. These results have already appeared in [2], [1], and [18]. They are
 308 being presented here for completeness and ease of referencing in the main results.

309 **3.1. Characterization of the good slow space of the Hamiltonian system.**
 310 The good slow space (\mathcal{O}_{wg}) of the Hamiltonian system provides us with the
 311 subspace of the state-space, which contains all the initial conditions that result in
 312 smooth optimal trajectories for the given singular LQR problem (see Lemma 4.1). In
 313 the following lemma we present a characterization of \mathcal{O}_{wg} (see [1, Section 3]).

314 **LEMMA 3.1.** *Consider the reduced Hamiltonian matrix pair (E_r, H_r) correspond-*
 315 *ing to the singular LQR Problem 2.6 as defined in equation (2.7). Assume that*
 316 *$\sigma(E_r, H_r) \cap j\mathbb{R} = \emptyset$. Define $\text{degdet}(sE_r - H_r) =: 2\mathbf{n}_s$ and $\Lambda := \sigma(E_r, H_r) \cap \mathbb{C}_-$*
 317 *(recall from Remark 2.9 that $|\Lambda| = \mathbf{n}_s$). Let $V_{1\Lambda}, V_{2\Lambda} \in \mathbb{R}^{\mathbf{n} \times \mathbf{n}_s}$ and $V_{3\Lambda} \in \mathbb{R}^{\mathbf{d} \times \mathbf{n}_s}$ be*
 318 *such that the matrix $\text{col}(V_{1\Lambda}, V_{2\Lambda}, V_{3\Lambda})$ is full column-rank and the following holds²:*

$$319 \quad (3.1) \quad \begin{bmatrix} A_r & -L & B_r \\ -Q_r & -A_r^T & 0 \\ 0 & B_r^T & 0 \end{bmatrix} \begin{bmatrix} V_{1\Lambda} \\ V_{2\Lambda} \\ V_{3\Lambda} \end{bmatrix} = \begin{bmatrix} I_n & 0 & 0 \\ 0 & I_n & 0 \\ 0 & 0 & 0 \end{bmatrix} \begin{bmatrix} V_{1\Lambda} \\ V_{2\Lambda} \\ V_{3\Lambda} \end{bmatrix} \Gamma,$$

321 where $\sigma(\Gamma) = \Lambda$. Then, the following are true:

- 322 1. The good slow space of $\Sigma_{\text{Ham}} =: \mathcal{O}_{wg} = \text{im} \begin{bmatrix} V_{1\Lambda} \\ V_{2\Lambda} \end{bmatrix}$.
- 323 2. $\begin{bmatrix} V_{1\Lambda} \\ V_{2\Lambda} \end{bmatrix}$ is full column-rank; that is, $\dim(\mathcal{O}_{wg}) = \mathbf{n}_s$.
- 324 3. $V_{1\Lambda}$ is full column-rank.

325 Statement 3 of Lemma 3.1 gives us an important structural property of the good
 326 slow space of the Hamiltonian system. This property is known as *disconjugacy* of the
 327 eigenspace of the matrix pair (E_r, H_r) (see [13, Definition 6.1.5]). Columns of the
 328 matrix $V_{1\Lambda}$ constitute a basis of a special subspace of the state space. Any initial
 329 condition from this subspace results in a smooth optimal trajectory. Moreover, left-
 330 invertibility of $V_{1\Lambda}$ plays a crucial role in providing a closed-form expression of the
 331 maximal rank-minimizing solution of the singular LQR LMI; it is also pivotal to the
 332 design of a PD state-feedback controller.

333 **3.2. Characterization of the fast space of the primal.** The following lemma
 334 presents a closed-form expression for the fast space of the primal ([2, Proposition 3.2],
 335 also see [18] for more details). It also enables us to read off the dimension of the fast
 336 space from the transfer function matrix of the system.

337 **LEMMA 3.2.** *Consider the primal Σ and the matrices A_r, B_r as defined in equation*
 338 *(2.4) and equation (2.8), respectively. Define $C_r := C - D_2 \widehat{R}^{-1} S_2^T$. Recall that*
 339 *$2\mathbf{n}_s = \text{deg}\{\text{numdet } G(-s)^T G(s)\}$, where $G(s)$ is the transfer function matrix of Σ and*
 340 *$\mathbf{d} = \text{nullity } R$. Let \mathcal{R}_s denote the fast space of Σ . Define*

$$341 \quad \mathcal{M} := \begin{cases} \begin{bmatrix} 0_{\mathbf{p}, \mathbf{d}} & & & & \\ 0_{\mathbf{p}, \mathbf{d}} & 0 & \dots & 0 & 0 \\ 0 & 0 & \dots & 0 & C_r B_r \\ 0 & 0 & \dots & C_r B_r & C_r A_r B_r \\ \vdots & \vdots & \ddots & \vdots & \vdots \\ 0 & C_r B_r & \dots & C_r A_r^{\mathbf{n}_f - \mathbf{d} - 2} B_r & C_r A_r^{\mathbf{n}_f - \mathbf{d} - 1} B_r \end{bmatrix} & \text{if } \mathbf{n}_f = \mathbf{d} \\ & \text{if } \mathbf{n}_f \geq \mathbf{d} + 1. \end{cases}$$

342 Then, the following are true:

- 343 1. $\dim(\ker \mathcal{M}) = \mathbf{n}_f$, where $\mathbf{n}_f := \mathbf{n} - \mathbf{n}_s$.
- 344 2. $\dim \mathcal{R}_s = \mathbf{n}_f$.

²Such matrices $V_{1\Lambda}, V_{2\Lambda}$, and $V_{3\Lambda}$ always exist. See [1, Section 3.2] for more on this.

345 3. Let $N \in \mathbb{R}^{d(n_f-d+1) \times n_f}$ be a matrix such that its columns form a basis for
 346 $\ker \mathcal{M}$. Define

$$347 \quad (3.2) \quad W := [B_r \quad A_r B_r \quad \dots \quad A_r^{n_f-d} B_r] N.$$

348 Then, $\mathcal{R}_s = \text{im } W$.

349 4. W is full column-rank, that is, the columns of W form a basis for \mathcal{R}_s .

350 We call \mathcal{M} the *Markov parameter matrix*. It is evident from Lemma 3.2 that \mathcal{M} plays
 351 a vital role in providing a closed-form expression of the fast space of the primal. It
 352 also plays a crucial role in computation of the optimal trajectories and also in the
 353 design of the PD feedback controller.

354 3.3. The maximal rank-minimizing solution of the singular LQR LMI.

355 The slow space of the Hamiltonian system and the fast space of the primal are inti-
 356 mately related to the maximal rank-minimizing solution K_{\max} of the LQR LMI. The
 357 following theorem provides a closed-form expression for K_{\max} by making use of these
 358 spaces. See [2, Section IV] for more details.

359 THEOREM 3.3. Consider the LQR Problem 2.6 with the corresponding LMI given
 360 by equation (2.3). Recall from Lemma 3.1 that the good slow space of the Hamiltonian
 361 system Σ_{Ham} is given by $\mathcal{O}_{wg} = \text{im} \begin{bmatrix} V_{1\Lambda} \\ V_{2\Lambda} \end{bmatrix}$. Further recall from Lemma 3.2 that the
 362 fast space of the primal Σ is given by $\mathcal{R}_s = \text{im } W$. Define $\begin{bmatrix} V_{1\Lambda} & W \\ V_{2\Lambda} & 0 \end{bmatrix} =: \begin{bmatrix} X \\ Y \end{bmatrix}$, where
 363 $X, Y \in \mathbb{R}^{n \times n}$. Then, the following statements hold:

- 364 1. X is invertible.
- 365 2. $K_{\max} := YX^{-1}$ is symmetric.
- 366 3. K_{\max} is a rank-minimizing solution of LMI (2.3).
- 367 4. For any other solution K of LMI (2.3), $K \leq K_{\max}$.
- 368 5. $K_{\max} \geq 0$.

369 REMARK 3.4. For the regular LQR problem, the relation between a rank min-
 370 imizing solution of the LQR LMI and its corresponding ARE is a well-known fact
 371 [23, Theorem 4.3.1]. For a regular problem, the maximal rank-minimizing solution
 372 of the corresponding LMI can be found using the algorithm provided in the seminal
 373 paper [24]. Note that, for a regular LQR problem, $n_s = n$; and hence by Lemma 3.1,
 374 it follows that $V_{1\Lambda} \in \mathbb{R}^{n \times n}$ is invertible. Further, for such a problem the fast space
 375 of the primal, $\mathcal{R}_s = \{0\}$. Thus, by Theorem 3.3, it follows that $K_{\max} = V_{2\Lambda} V_{1\Lambda}^{-1}$;
 376 which is in agreement with [24]. So, the algorithm for computation of the maximal
 377 rank-minimizing solution of the regular LQR LMI as given in [24] is a special case
 378 of Theorem 3.3. However, in this paper Theorem 3.3 provides a recipe to compute
 379 the maximal rank minimizing solution of the LQR LMI, both for the regular and
 380 the singular case. This eventually leads to a solution of the singular LQR problem.
 381 Interestingly, [23] uses special co-ordinate basis (SCB) to show that for the singular
 382 LQR case, the rank minimizing solution of the LQR LMI admits a special structure
 383 [23, Equation 4.3.20]. Hence, a natural question would be to investigate if the bases
 384 of the fast and the slow spaces admit some structure when the primal system is in
 385 SCB to start with. Thus, a study on the relation between fast/slow spaces and the
 386 SCB might provide valuable insights into the singular LQR problem and its solutions.
 387 We do not delve into such a study in this paper, as our primary focus in this paper
 388 is the design of a PD state-feedback controller, using the maximal rank minimizing
 389 solution of the singular LQR LMI, that solves the singular LQR problem. \square

390 In the following remark we discuss about a certain observation regarding the kernel
 391 of K_{\max} and its implication.

392 REMARK 3.5. In [23, Lemma 4.3.4] it has been shown that an arbitrary solution
 393 K of the LQR LMI contains a certain subspace of the state space of the primal inside

394 its kernel (which the authors in [23] call the *detectable strongly controllable subspace*).
395 From Theorem 3.3, we know that $K_{\max} = [V_{2\lambda} \ 0] [V_{1\lambda} \ W]^{-1}$. From [2, Remark 2.11
396 and Lemma 2.12], it follows that, without loss of generality, $[V_{2\lambda}^{\top}]$ can be written as
397 $[V_{2\lambda}^{\top}] = \begin{bmatrix} V_g & V_{1e} \\ 0 & V_{2e} \end{bmatrix}$, where the columns of the matrix V_g form a basis for the good slow
398 space of the primal and V_{2e} is full column-rank. Hence, $K_{\max} = [0 \ V_{2e} \ 0] [V_g \ V_{1e} \ W]^{-1}$.
399 So, $K_{\max} V_g = 0$ and $K_{\max} W = 0$. Also, since V_{2e} is full column-rank, the kernel of
400 K_{\max} is exactly equal to the direct-sum of the good slow space and the fast space of
401 the primal. This observation gives rise to an interesting conclusion: since, for a given
402 initial condition, the optimal cost of the singular LQR problem is given by $x_0^T K_{\max} x_0$
403 (see [11, Theorem 2]), any initial condition belonging to the direct-sum of the good
404 slow space and the fast space of the primal incurs zero optimal cost. \square

405 An auxiliary result pertaining to any arbitrary solution K of the LQR LMI (2.3) is
406 required in the sequel. We present this result as a lemma next (see [2, Lemma 4.1]).

407 **LEMMA 3.6.** *Let $K \in \mathbb{R}^{n \times n}$ be an arbitrary solution of the LQR LMI (2.3). Then,*
408 *$KW = 0$, where W is as defined in equation (3.2).*

409 **REMARK 3.7.** Lemma 3.6 shows that the fast space (\mathcal{R}_s) of the primal is a sub-
410 space of the kernel of any solution K of the LQR LMI (2.3). So, in particular, \mathcal{R}_s
411 is a subspace of $\ker K_{\max}$. Hence, for an initial condition from $\text{im } W$, the optimal cost
412 must be zero. This conclusion has also been drawn in Remark 3.5. \square

413 **3.4. A few auxiliary results.** The structure of the matrix \mathcal{M} leads to sub-
414 spaces that follow a chain of inclusions elaborated in the following lemma.

LEMMA 3.8. *Consider the matrix \mathcal{M} as defined in Lemma 3.2 and let $N \in \mathbb{R}^{d(n_f-d+1) \times n_f}$
be a matrix such that its columns form a basis for $\ker \mathcal{M}$. Partition N as $N = \text{col}(N_0, N_1, \dots, N_{n_f-d})$ with $N_0, N_1, \dots, N_{n_f-d} \in \mathbb{R}^{d \times n_f}$. For all
 *$i \in \{1, 2, \dots, (n_f - d)\}$ define $\bar{N}_i := \text{col}(N_i, N_{i+1}, \dots, N_{n_f-d})$. Then,**

$$\text{im} \begin{bmatrix} \bar{N}_{n_f-d} \\ 0 \end{bmatrix} \subseteq \text{im} \begin{bmatrix} \bar{N}_{n_f-d-1} \\ 0 \end{bmatrix} \subseteq \dots \subseteq \text{im} \begin{bmatrix} \bar{N}_2 \\ 0 \end{bmatrix} \subseteq \text{im} \begin{bmatrix} \bar{N}_1 \\ 0 \end{bmatrix} \subseteq \text{im } N.$$

415 Here the sizes of the zero matrices are such that $\begin{bmatrix} \bar{N}_i \\ 0 \end{bmatrix} \in \mathbb{R}^{d(n_f-d+1) \times n_f}$ for all $i \in$
416 $\{1, 2, \dots, (n_f - d)\}$.

417 *Proof* Let $\bar{\mathcal{M}}$ be the matrix obtained by removing the first d columns and the
418 last p rows of \mathcal{M} , that is, $\mathcal{M} = \begin{bmatrix} 0 & \bar{\mathcal{M}} \\ 0_{p,d} & \bar{m} \end{bmatrix}$ with $\bar{m} := [C_r B_r \ C_r A_r B_r \ \dots \ C_r A_r^{n_f-d-1} B_r]$.

419 Then, due to the structure of \mathcal{M} it also follows that $\mathcal{M} = \begin{bmatrix} 0 & 0_{p,d} \\ \bar{\mathcal{M}} & \bar{n} \end{bmatrix}$, where $\bar{n} :=$
420 $\text{col}(C_r B_r, C_r A_r B_r, \dots, C_r A_r^{n_f-d-1} B_r)$. We use this observation to first show that

421 $\text{im} \begin{bmatrix} \bar{N}_1 \\ 0 \end{bmatrix} \subseteq \text{im } N$. Since $\text{im } N = \ker \mathcal{M}$, it follows that

$$422 \quad \mathcal{M}N = 0 \Leftrightarrow \begin{bmatrix} 0 & \bar{\mathcal{M}} \\ 0_{p,d} & \bar{m} \end{bmatrix} \begin{bmatrix} N_0 \\ \bar{N}_1 \end{bmatrix} = 0 \Rightarrow \bar{\mathcal{M}} \bar{N}_1 = 0 \Rightarrow \begin{bmatrix} 0 & 0_{p,d} \\ \bar{\mathcal{M}} & \bar{n} \end{bmatrix} \begin{bmatrix} \bar{N}_1 \\ 0 \end{bmatrix} = 0 \Rightarrow \mathcal{M} \begin{bmatrix} \bar{N}_1 \\ 0 \end{bmatrix} = 0$$

$$423 \quad (3.3) \quad \Rightarrow \text{im} \begin{bmatrix} \bar{N}_1 \\ 0 \end{bmatrix} \subseteq \text{im } N \Leftrightarrow \text{im} \begin{bmatrix} N_1 \\ N_2 \\ \vdots \\ N_{n_f-d} \\ 0_{d,n_f} \end{bmatrix} \subseteq \text{im} \begin{bmatrix} N_0 \\ N_1 \\ \vdots \\ N_{n_f-d-1} \\ N_{n_f-d} \end{bmatrix}.$$

424 Let $i \in \{2, 3, \dots, (n_f - d)\}$ be arbitrary. Then, we have to show that $\text{im} \begin{bmatrix} \bar{N}_i \\ 0 \end{bmatrix} \subseteq$

425 $\text{im} \begin{bmatrix} \bar{N}_{i-1} \\ 0 \end{bmatrix}$, which is equivalent to showing that $\text{im} \begin{bmatrix} \bar{N}_i \\ 0_{d,n_f} \end{bmatrix} \subseteq \text{im } \bar{N}_{i-1}$. This directly

426 follows from equation (3.3), because $\text{im } \text{col}(N_i, N_{i+1}, \dots, N_{n_f-d}, 0_{d,n_f}) \subseteq$

427 $\text{im col}(N_{i-1}, N_i, \dots, N_{n_f-d})$. This completes the proof. \square

428
 429 REMARK 3.9. Define the system given by $\frac{d}{dt}x(t) = A_r x(t) + B_r u_1(t)$, $y(t) =$
 430 $C_r x(t)$. Let the initial condition of the system be $x_0 = 0$. Then, it turns out that,
 431 the input $u_1(t) := \sum_{i=0}^{n_f-d} a_i \delta^{(i)}$ with $a_i \in \mathbb{R}^d$ results in a regular output, that is,
 432 $y(t; 0, u_1) \in \mathcal{C}^\infty(\mathbb{R}, \mathbb{R}^p)$ if and only if $\text{col}(a_0, a_1, \dots, a_{n_f-d}) = \text{col}(N_0, N_1, \dots, N_{n_f-d})\beta$
 433 for some $\beta \in \mathbb{R}^{n_f}$ (see [18, Lemma 4.1]). In [18], such an input has been termed as an
 434 *admissible impulsive input*. From Lemma 3.8, it can be concluded that if $\sum_{i=0}^{n_f-d} a_i \delta^{(i)}$
 435 is an admissible impulsive input, then $\sum_{i=k}^{n_f-d} a_i \delta^{(i-k)}$, too, is an admissible impulsive
 436 input for all $k \in \{1, 2, \dots, n_f - d\}$. \square

437 Using the subspaces in Lemma 3.8, we can form another class of subspaces that follow
 438 an inclusion chain as in Lemma 3.8. We present this next.

LEMMA 3.10. For all $i \in \{1, 2, \dots, (n_f - d)\}$ define $W_i := [B_r \ A_r B_r \ \dots \ A_r^{n_f-d} B_r] \begin{bmatrix} \bar{N}_i \\ 0_{i, n_f} \end{bmatrix}$,
 where \bar{N}_i is as defined in Lemma 3.8. Then, the following filtration follows:

$$\text{im } W_{n_f-d} \subseteq \text{im } W_{n_f-d-1} \subseteq \dots \subseteq \text{im } W_2 \subseteq \text{im } W_1 \subseteq \text{im } W.$$

439 The next lemma shows that the subspaces $\text{im } W_1, \text{im } W_2, \dots, \text{im } W_{n_f-d}$ are contained
 440 in the kernel of C_r .

441 LEMMA 3.11. Recall the matrices C_r and $W_1, W_2, \dots, W_{n_f-d}$ as defined in Lemma
 442 3.2 and Lemma 3.10, respectively. Then, $C_r W_i = 0$ for all $i \in \{1, 2, \dots, n_f - d\}$.

443 *Proof* By definition, $MN = 0$. Notice from the definitions of $W_1, W_2, \dots, W_{n_f-d}$ that
 444 $MN = \text{col}(0, C_r W_{n_f-d}, \dots, C_r W_2, C_r W_1)$. Hence the result follows. \square

445
 446 REMARK 3.12. Lemma 3.10 implies that if $\delta^{(i)}$ does not appear in the optimal
 447 state trajectory, then $\delta^{(i+1)}$ cannot appear in the optimal state trajectory. Lemma
 448 3.11 implies that the optimal output trajectory of the primal due to an initial condition
 449 from $\text{im } W$ is identically zero. This, further implies that the optimal cost due to an
 450 initial condition from the fast space of the primal is zero. Justification of these
 451 statements needs a few result, which we present in the sequel. Hence, we justify these
 452 statements in Section 5. \square

453 **4. Optimal trajectories.** In this section we evaluate the trajectories of the
 454 primal Σ (see equation (2.4)) for an arbitrary initial condition, which minimize the cost
 455 function given by equation (2.2). Due to Statement 1 of Theorem 3.3, it is evident that
 456 the state space \mathbb{R}^n admits a direct-sum decomposition given by $\mathbb{R}^n = \text{im } V_{1\Lambda} \oplus \text{im } W$.
 457 This enables us to compute the optimal trajectories in two steps. First, we compute
 458 the optimal trajectories when the initial condition is restricted to the *slow* part, i.e.,
 459 $\text{im } V_{1\Lambda}$. Then, we compute the optimal trajectories for an initial condition in the *fast*
 460 part, i.e., $\text{im } W$. We achieve these tasks in the following two lemmas.

461 LEMMA 4.1. Consider the LQR Problem 2.6 and the matrices $V_{1\Lambda}, V_{2\Lambda}, V_{3\Lambda}$, and
 462 Γ as defined in equation (3.1). Define $x_{0s} := V_{1\Lambda}\alpha$, $z_{0s} := V_{2\Lambda}\alpha$, $x_s := V_{1\Lambda}e^{\Gamma t}\alpha$, $z_s :=$
 463 $V_{2\Lambda}e^{\Gamma t}\alpha$, $u_{s_1} := V_{3\Lambda}e^{\Gamma t}\alpha$, and $u_{s_2} := -\hat{R}^{-1}(S_2^T + B_2^T K_{\max})x_s$, where $\alpha \in \mathbb{R}^{n_s}$ is
 464 arbitrary. Then,

- 465 1. $\text{col}(x_s, z_s, u_{s_1}, u_{s_2})$ is a trajectory of the Hamiltonian system defined in equa-
 466 tion (2.5) corresponding to the initial condition $\text{col}(x_{0s}, z_{0s})$.
- 467 2. $\text{col}(x_s, u_{s_1}, u_{s_2})$ is a trajectory of the primal Σ defined in equation (2.4) cor-
 468 responding to the initial condition x_{0s} .
- 469 3. $\int_0^\infty \begin{bmatrix} x_s \\ u_{s_1} \\ u_{s_2} \end{bmatrix}^T \begin{bmatrix} Q & 0 & S_2 \\ 0 & 0 & 0 \\ S_2^T & 0 & \hat{R} \end{bmatrix} \begin{bmatrix} x_s \\ u_{s_1} \\ u_{s_2} \end{bmatrix} dt = x_{0s}^T K_{\max} x_{0s}$.

470 *Proof* 1. Notice from the definition of K_{\max} that $K_{\max} V_{1\Lambda} = V_{2\Lambda}$. Using this identity
 471 along with equation (3.1), it can be easily seen that the trajectory $\text{col}(x_s, z_s, u_{s_1}, u_{s_2})$

472 satisfies the Hamiltonian system's equation (2.5). Hence, $\text{col}(x_s, z_s, u_{s_1}, u_{s_2})$ is a tra-
 473 jectory of the Hamiltonian system corresponding to the initial condition $\text{col}(x_{0s}, z_{0s})$.

474 2. It is a matter of simple verification that if $\text{col}(x_s, z_s, u_{s_1}, u_{s_2})$ is a trajectory of the
 475 Hamiltonian, then the projection $\text{col}(x_s, u_{s_1}, u_{s_2})$ is a trajectory of the primal.

3. Using the definitions of x_s, u_{s_1}, u_{s_2} , and K_{\max} and doing some simple algebraic
 manipulations with the help of equation (3.1) (see [2, proof of Theorem 4.5]) we
 get that $\frac{d}{dt}(x_s^T K_{\max} x_s) = - \begin{bmatrix} x_s \\ u_{s_1} \\ u_{s_2} \end{bmatrix}^T \begin{bmatrix} Q & 0 & S_2 \\ 0 & 0 & 0 \\ S_2^T & 0 & \hat{R} \end{bmatrix} \begin{bmatrix} x_s \\ u_{s_1} \\ u_{s_2} \end{bmatrix}$. Integrating both sides of this
 equation, we further get

$$\int_0^\infty \begin{bmatrix} x_s \\ u_{s_1} \\ u_{s_2} \end{bmatrix}^T \begin{bmatrix} Q & 0 & S_2 \\ 0 & 0 & 0 \\ S_2^T & 0 & \hat{R} \end{bmatrix} \begin{bmatrix} x_s \\ u_{s_1} \\ u_{s_2} \end{bmatrix} dt = x_s(0)^T K_{\max} x_s(0) - x_s(\infty)^T K_{\max} x_s(\infty).$$

Now, since Γ is Hurwitz, from the definition of x_s it is clear that $x_s(\infty) = 0$ and
 $x_s(0) = x_{0s}$. Therefore, we conclude that

$$\int_0^\infty \begin{bmatrix} x_s \\ u_{s_1} \\ u_{s_2} \end{bmatrix}^T \begin{bmatrix} Q & 0 & S_2 \\ 0 & 0 & 0 \\ S_2^T & 0 & \hat{R} \end{bmatrix} \begin{bmatrix} x_s \\ u_{s_1} \\ u_{s_2} \end{bmatrix} dt = x_{0s}^T K_{\max} x_{0s}.$$

476

□

477 The following lemma deals with the case when the initial condition is in the fast space.

478 LEMMA 4.2. Consider the LQR Problem 2.6 and the matrices N and W as defined
 479 in equation (3.2). Also recall the matrices $W_1, W_2, \dots, W_{n_f-d}$ as defined in Lemma
 480 3.10. Define $x_{0f} := W\beta, z_{0f} := 0 \in \mathbb{R}^n, x_f := -[W_1\delta + W_2\delta^{(1)} + \dots + W_{n_f-d}\delta^{(n_f-d-1)}]\beta,$
 481 $z_f := 0 \in \mathbb{R}^n, u_{f_1} := -[\delta I_d \delta^{(1)} I_d \dots \delta^{(n_f-d)} I_d] N\beta,$ and $u_{f_2} := -\hat{R}^{-1}(S_2^T + B_2^T K_{\max})x_f,$
 482 where $\beta \in \mathbb{R}^{n_f}$ is arbitrary. Then,

- 483 1. $\text{col}(x_f, z_f, u_{f_1}, u_{f_2})$ is a distributional trajectory of the Hamiltonian system
 484 defined in equation (2.5) corresponding to the initial condition $\text{col}(x_{0f}, z_{0f})$.
- 485 2. $\text{col}(x_f, u_{f_1}, u_{f_2})$ is a distributional trajectory of the primal Σ defined in equa-
 486 tion (2.4) corresponding to the initial condition x_{0f} .
- 487 3. $\int_0^\infty \begin{bmatrix} x_f \\ u_{f_1} \\ u_{f_2} \end{bmatrix}^T \begin{bmatrix} Q & 0 & S_2 \\ 0 & 0 & 0 \\ S_2^T & 0 & \hat{R} \end{bmatrix} \begin{bmatrix} x_f \\ u_{f_1} \\ u_{f_2} \end{bmatrix} dt = 0.$

488 *Proof* 1. Partition N as $N = \text{col}(N_0, N_1, \dots, N_{n_f-d})$ with $N_0, N_1, \dots, N_{n_f-d} \in \mathbb{R}^{d \times n_f}$.
 489 Recall from Lemma 3.10 that for all $i \in \{1, 2, \dots, (n_f - d)\}$, W_i has been defined as
 490 $W_i = [B_r \ A_r B_r \ \dots \ A_r^{n_f-d} B_r] \begin{bmatrix} \bar{N}_i \\ 0_{i, n_f} \end{bmatrix}$, where $\bar{N}_i = \text{col}(N_i, N_{i+1}, \dots, N_{n_f-d})$. Also recall
 491 that $W = [B_r \ A_r B_r \ \dots \ A_r^{n_f-d} B_r] N$. Clearly,

$$492 \quad (4.1) \quad W_i = B_r N_i + A_r W_{i+1} \text{ for all } i \in \{1, 2, \dots, (n_f - d - 1)\},$$

$$493 \quad W_{n_f-d} = B_r N_{n_f-d}, \text{ and } W = B_r N_0 + A_r W_1.$$

494 We need to show that the trajectory $\text{col}(x_f, z_f, u_{f_1}, u_{f_2})$ satisfies equation (2.5) in
 495 distributional sense. Using equation (4.1) we get that

$$496 \quad \frac{d}{dt}(x_f) = -x_{0f}\delta - [W_1\delta^{(1)} + W_2\delta^{(2)} + \dots + W_{n_f-d}\delta^{(n_f-d)}]\beta$$

$$497 \quad = -W\beta\delta - [W_1\delta^{(1)} + W_2\delta^{(2)} + \dots + W_{n_f-d}\delta^{(n_f-d)}]\beta$$

$$498 \quad = - \left[(B_r N_0 + A_r W_1)\delta + \sum_{i=1}^{n_f-d-1} (B_r N_i + A_r W_{i+1})\delta^{(i)} + B_r N_{n_f-d}\delta^{(n_f-d)} \right] \beta$$

$$499 \quad = -A_r [W_1\delta + W_2\delta^{(1)} + \dots + W_{n_f-d}\delta^{(n_f-d-1)}]\beta - B_r [N_0\delta + N_1\delta^{(1)} + \dots + N_{n_f-d}\delta^{(n_f-d)}]\beta$$

$$500 \quad (4.2) \quad \Leftrightarrow \frac{d}{dt}(x_f) = A_r x_f + B_r u_{f_1}.$$

501 Now, by Lemma 3.10 we know that $\text{im } W_{n_f-d} \subseteq \text{im } W_{n_f-d-1} \subseteq \dots \subseteq \text{im } W_1 \subseteq \text{im } W$.
 502 Again, by Lemma 3.6, it follows that $K_{\max} W = 0$. Consequently,

$$503 \quad (4.3) \quad K_{\max} x_f = 0.$$

504 Using equation (4.2) and equation (4.3), we deduce that

$$505 \quad (4.4) \quad Ax_f + B_1u_{f_1} + B_2u_{f_2} = A_rx_f - LK_{\max}x_f + B_ru_{f_1} = A_rx_f + B_ru_{f_1} = \frac{d}{dt}(x_f).$$

506 From Lemma 3.11 it directly follows that

$$507 \quad (4.5) \quad C_rx_f = 0.$$

508 Next, using the fact that $z_f = 0$ (by definition) along with equation (4.3) and equation
509 (4.5) we get the following equations

$$510 \quad (4.6) \quad -Qx_f + A^Tz_f - S_2u_{f_2} = -Q_rx_f - S_2\widehat{R}^{-1}B_2^TK_{\max}x_f = -C_r^TC_rx_f = 0 = \frac{d}{dt}(z_f),$$

$$511 \quad (4.7) \quad B_1^Tz_f = 0, \text{ and}$$

$$512 \quad (4.8) \quad S_2^Tx_f + B_2^Tz_f + \widehat{R}u_{f_2} = S_2^Tx_f - \widehat{R}\widehat{R}^{-1}(S_2^T + B_2^TK_{\max})x_f = 0.$$

513 Combining equation (4.4), equation (4.6), equation (4.7), and equation (4.8) together
514 yields equation (2.5). Hence, $\text{col}(x_f, z_f, u_{f_1}, u_{f_2})$ is a trajectory of the Hamiltonian
515 system corresponding to the initial condition $\text{col}(x_{0f}, z_{0f})$.

516 2. This statement directly follows from equation (4.4).

517 3. Recall from Section 2.4 that

$$518 \quad (4.9) \quad \begin{bmatrix} Q & 0 & S_2 \\ 0 & 0 & 0 \\ S_2^T & 0 & \widehat{R} \end{bmatrix} = \begin{bmatrix} C^T \\ 0 \\ D_2^T \end{bmatrix} [C \ 0 \ D_2].$$

519 Now, $[C \ 0 \ D_2] \begin{bmatrix} x_f \\ u_{f_1} \\ u_{f_2} \end{bmatrix} = Cx_f + D_2u_{f_2} = C_rx_f - D_2\widehat{R}^{-1}B_2^TK_{\max}x_f$. Therefore, from
520 equation (4.3) and equation (4.5), it is evident that

$$521 \quad (4.10) \quad [C \ 0 \ D_2] \begin{bmatrix} x_f \\ u_{f_1} \\ u_{f_2} \end{bmatrix} = 0.$$

522 Combining equation (4.9) and equation (4.10), we have $\begin{bmatrix} x_f \\ u_{f_1} \\ u_{f_2} \end{bmatrix}^T \begin{bmatrix} Q & 0 & S_2 \\ 0 & 0 & 0 \\ S_2^T & 0 & \widehat{R} \end{bmatrix} \begin{bmatrix} x_f \\ u_{f_1} \\ u_{f_2} \end{bmatrix} = 0$.

523 This further implies that $\int_0^\infty \begin{bmatrix} x_f \\ u_{f_1} \\ u_{f_2} \end{bmatrix}^T \begin{bmatrix} Q & 0 & S_2 \\ 0 & 0 & 0 \\ S_2^T & 0 & \widehat{R} \end{bmatrix} \begin{bmatrix} x_f \\ u_{f_1} \\ u_{f_2} \end{bmatrix} dt = 0$. \square

524 Recall from Statement 1 of Theorem 3.3 that $X = [V_{1\Lambda} \ W]$ is invertible. So, for an
525 arbitrary initial condition x_0 there exist $\alpha \in \mathbb{R}^{n_s}$ and $\beta \in \mathbb{R}^{n_f}$ such that $x_0 = V_{1\Lambda}\alpha +$
526 $W\beta$. Therefore, Lemma 4.1 and Lemma 4.2 can be combined to obtain an allowable
527 trajectory of the given system for an arbitrary initial condition. Here, a trajectory
528 being allowable means that the trajectory satisfies the system's equations. In the
529 following theorem, we show that this trajectory, indeed, is the optimal trajectory.

530 **THEOREM 4.3.** *Consider the LQR Problem 2.6. Recall the definitions of $x_{0s}, x_{0f},$
531 $x_s, x_f, u_{s_1}, u_{s_2}, u_{f_1}$, and u_{f_2} from Lemma 4.1 and Lemma 4.2. Define $x_0 := x_{0s} +$
532 $x_{0f}, x^* := x_s + x_f, u_1^* := u_{s_1} + u_{f_1}$, and $u_2^* := u_{s_2} + u_{f_2}$. Then, the following are true:*

533 1. $\text{col}(x^*, u_1^*, u_2^*)$ is an allowable trajectory of the primal Σ defined in equation
534 (2.4) corresponding to an arbitrary initial condition x_0 .

535 2. $\int_0^\infty \begin{bmatrix} x^* \\ u_1^* \\ u_2^* \end{bmatrix}^T \begin{bmatrix} Q & 0 & S_2 \\ 0 & 0 & 0 \\ S_2^T & 0 & \widehat{R} \end{bmatrix} \begin{bmatrix} x^* \\ u_1^* \\ u_2^* \end{bmatrix} dt = x_0^TK_{\max}x_0$.

536 3. $\text{col}(x^*, u_1^*, u_2^*)$ is the optimal trajectory for the initial condition x_0 .

537 *Proof* 1. This statement follows from application of Lemma 4.1 and Lemma 4.2
538 together with linearity of the system Σ .

539 2. Using equation 4.10, it is clear that

$$540 \quad (4.11) \quad [C \ 0 \ D_2] \begin{bmatrix} x^* \\ u_1^* \\ u_2^* \end{bmatrix} = [C \ 0 \ D_2] \begin{bmatrix} x_s + x_f \\ u_{s_1} + u_{f_1} \\ u_{s_2} + u_{f_2} \end{bmatrix} = [C \ 0 \ D_2] \begin{bmatrix} x_s \\ u_{s_1} \\ u_{s_2} \end{bmatrix}.$$

541 Combining equation (4.9) and equation (4.11) together, we have

$$542 \quad (4.12) \quad \begin{bmatrix} x^* \\ u_1^* \\ u_2^* \end{bmatrix}^T \begin{bmatrix} Q & 0 & S_2 \\ 0 & 0 & 0 \\ S_2^T & 0 & \hat{R} \end{bmatrix} \begin{bmatrix} x^* \\ u_1^* \\ u_2^* \end{bmatrix} = \begin{bmatrix} x_s \\ u_{s_1} \\ u_{s_2} \end{bmatrix}^T \begin{bmatrix} Q & 0 & S_2 \\ 0 & 0 & 0 \\ S_2^T & 0 & \hat{R} \end{bmatrix} \begin{bmatrix} x_s \\ u_{s_1} \\ u_{s_2} \end{bmatrix}.$$

543 Recall from Theorem 3.3 that K_{\max} is symmetric. Due to Lemma 3.6 we also have
544 $K_{\max}W = 0$. Therefore, it follows that

$$545 \quad x_0^T K_{\max} x_0 = (V_{1\Lambda}\alpha + W\beta)^T K_{\max} (V_{1\Lambda}\alpha + W\beta) = (V_{1\Lambda}\alpha)^T K_{\max} V_{1\Lambda}\alpha = x_{0s}^T K_{\max} x_{0s}.$$

546 Hence, using equation (4.12) in Statement 3 of Lemma 4.1, we conclude that

$$547 \quad \int_0^\infty \begin{bmatrix} x^* \\ u_1^* \\ u_2^* \end{bmatrix}^T \begin{bmatrix} Q & 0 & S_2 \\ 0 & 0 & 0 \\ S_2^T & 0 & \hat{R} \end{bmatrix} \begin{bmatrix} x^* \\ u_1^* \\ u_2^* \end{bmatrix} dt = \int_0^\infty \begin{bmatrix} x_s \\ u_{s_1} \\ u_{s_2} \end{bmatrix}^T \begin{bmatrix} Q & 0 & S_2 \\ 0 & 0 & 0 \\ S_2^T & 0 & \hat{R} \end{bmatrix} \begin{bmatrix} x_s \\ u_{s_1} \\ u_{s_2} \end{bmatrix} dt = x_0^T K_{\max} x_0.$$

548

549 3. By Theorem 3.3, we know that K_{\max} is the maximal rank-minimizing solution of
550 the LQR LMI 2.3. Therefore, using [11, Theorem 2] we infer that given an initial con-
551 dition x_0 , the minimal cost attainable for the singular LQR Problem 2.6 is $x_0^T K_{\max} x_0$.
552 Also, since we have assumed that the primal Σ is a left-invertible system, the optimal
553 trajectories must be unique [3]. Hence, from Statement 2 of this theorem, it is evi-
554 dent that $\text{col}(x^*, u_1^*, u_2^*)$ is the optimal trajectory for the singular LQR problem 2.6
555 corresponding to the initial condition x_0 . \square

556

557 **5. PD feedback design.** In this section we design a PD-feedback controller
558 that restricts the system to only the optimal trajectories (Theorem 5.5). Two different
559 direct-sum decompositions of \mathcal{R}_s are crucially used in order to design this feedback.
560 The following lemma provides these direct-sum decompositions.

561 **LEMMA 5.1.** *Recall that \mathcal{R}_s denotes the fast space of the primal and $\mathbf{n}_f = \dim \mathcal{R}_s$.
562 Also recall that $\mathbf{d} = \text{nullity } R$. There exists a subspace $\tilde{\mathcal{R}}_s \subseteq \mathcal{R}_s$ of dimension equal
563 to $\mathbf{n}_f - \mathbf{d}$ satisfying the following properties:*

- 564 1. $A_r \tilde{\mathcal{R}}_s \subseteq \mathcal{R}_s$, $\dim(A_r \tilde{\mathcal{R}}_s) = \mathbf{n}_f - \mathbf{d}$, and $\mathcal{R}_s = \text{im } B_r \oplus A_r \tilde{\mathcal{R}}_s$.
- 565 2. There exists $W_e \in \mathbb{R}^{\mathbf{n} \times \mathbf{d}}$ full column-rank such that $\mathcal{R}_s = \tilde{\mathcal{R}}_s \oplus \text{im } W_e$.

566 *Proof* By Lemma 3.2, we know that $\mathcal{R}_s = \text{im} [B_r \ A_r B_r \ \dots \ A_r^{\mathbf{n}_f - \mathbf{d}} B_r] N$, where $N \in$
567 $\mathbb{R}^{\mathbf{d}(\mathbf{n}_f - \mathbf{d} + 1) \times \mathbf{n}_f}$ is a matrix such that its columns form a basis for the kernel of \mathcal{M} .

568 Due to the structure of \mathcal{M} , it follows that there exists $\tilde{N} \in \mathbb{R}^{\mathbf{d}(\mathbf{n}_f - \mathbf{d}) \times (\mathbf{n}_f - \mathbf{d})}$ such that
569 the columns of $\begin{bmatrix} I_{\mathbf{d}} & 0 \\ 0 & \tilde{N} \end{bmatrix}$ form a basis for $\ker \mathcal{M}$. Therefore, \mathcal{R}_s is given by

$$570 \quad (5.1) \quad \mathcal{R}_s = \text{im} \underbrace{[B_r \ A_r B_r \ \dots \ A_r^{\mathbf{n}_f - \mathbf{d}} B_r]}_{\tilde{W}} \begin{bmatrix} I_{\mathbf{d}} & 0 \\ 0 & \tilde{N} \end{bmatrix} = \text{im } B_r \oplus \text{im} [A_r B_r \ A_r^2 B_r \ \dots \ A_r^{\mathbf{n}_f - \mathbf{d}} B_r] \tilde{N}.$$

571 Recall from Lemma 3.2 that \widehat{W} is full column-rank, which leads to the direct-sum
572 decomposition in the above equation.

573 Now, by Lemma 3.8, it is evident that $\text{im} \begin{bmatrix} 0 & \tilde{N} \\ 0 & 0 \end{bmatrix} = \text{im} \begin{bmatrix} \tilde{N} \\ 0 \end{bmatrix} \subseteq \ker \mathcal{M}$. Since $\begin{bmatrix} \tilde{N} \\ 0 \end{bmatrix}$ is full
574 column-rank, there exists $\tilde{N}_{12} \in \mathbb{R}^{\mathbf{d}(\mathbf{n}_f - \mathbf{d}) \times \mathbf{d}}$ and $\tilde{N}_{22} \in \mathbb{R}^{\mathbf{d} \times \mathbf{d}}$ such that the columns of
575 the matrix $\begin{bmatrix} \tilde{N} & \tilde{N}_{12} \\ 0 & \tilde{N}_{22} \end{bmatrix}$ form a basis for $\ker \mathcal{M}$. So, \mathcal{R}_s is also given by

576 (5.2)
$$\mathcal{R}_s = \text{im} [B_r \ A_r B_r \ \dots \ A_r^{\mathfrak{n}_f - \mathfrak{d}} B_r] \begin{bmatrix} \tilde{N} & \tilde{N}_{12} \\ 0 & \tilde{N}_{22} \end{bmatrix} = \text{im} \tilde{W} \oplus \text{im} W_e,$$

577 where $\tilde{W} := [B_r \ A_r B_r \ \dots \ A_r^{\mathfrak{n}_f - \mathfrak{d} - 1} B_r] \tilde{N}$ and $W_e := [B_r \ A_r B_r \ \dots \ A_r^{\mathfrak{n}_f - \mathfrak{d}} B_r] \begin{bmatrix} \tilde{N}_{12} \\ \tilde{N}_{22} \end{bmatrix}$.

578 Define $\tilde{\mathcal{R}}_s := \text{im} \tilde{W}$. Then, clearly $\tilde{\mathcal{R}}_s \subseteq \mathcal{R}_s$ and $\dim(\tilde{\mathcal{R}}_s) = \mathfrak{n}_f - \mathfrak{d}$. Next, we show
579 that $\tilde{\mathcal{R}}_s$ satisfies all the required properties.

580 1. Applying equation (5.2) in equation (5.1) we get that

581 (5.3)
$$\mathcal{R}_s = \text{im} B_r \oplus \text{im} A_r \tilde{W} = \text{im} B_r \oplus A_r \tilde{\mathcal{R}}_s.$$

582 Hence, $A_r \tilde{\mathcal{R}}_s \subseteq \mathcal{R}_s$, $\dim(A_r \tilde{\mathcal{R}}_s) = \mathfrak{n}_f - \mathfrak{d}$, and $\mathcal{R}_s = \text{im} B_r \oplus A_r \tilde{\mathcal{R}}_s$.

583 2. This property trivially follows. \square

584 *Justification of Remark 3.12:* Recall from Lemma 4.2 and Theorem 4.3 that, corre-
585 sponding to the initial condition $x_0 = W\beta$, where $\beta \in \mathbb{R}^{\mathfrak{n}_f}$, the optimal state trajectory
586 is given by $x_f = -[W_1\delta + W_2\delta^{(1)} + \dots + W_{\mathfrak{n}_f - \mathfrak{d}}\delta^{(\mathfrak{n}_f - \mathfrak{d} - 1)}]\beta$. Next, using Lemma 3.10
587 along with equation (4.1) and equation (5.3), it follows that $W_i\beta = 0 \Rightarrow W_{i+1}\beta = 0$
588 (note that, columns of \tilde{W} form a basis for $\text{im} W_1$ and $A_r \tilde{W}$ is full column-rank).
589 Hence, if $\delta^{(i)}$ does not appear in the optimal state trajectory, then $\delta^{(i+1)}$, too, cannot
590 appear in the same.

591 From Theorem 4.3 and equation (2.4), it follows that, corresponding to an initial
592 condition $x_0 = W\beta$, where $\beta \in \mathbb{R}^{\mathfrak{n}_f}$, the optimal output trajectory of the primal is
593 given by $y^*(t) = C_r x_f - D_2 \hat{R}^{-1} B_2^T K_{\max} x_f$. Then, Lemma 3.11 together with Lemma
594 3.6 implies that $y^*(t) \equiv 0$. \square

595

596 REMARK 5.2. Recall from Theorem 4.3 that $\text{col}(x^*, u_1^*, u_2^*)$ is the optimal tra-
597 jectory for an arbitrary initial condition x_0 . Further recall that $u_2^* = u_{s_2} + u_{f_2} =$
598 $-\hat{R}^{-1}(S_2^T + B_2^T K_{\max})(x_s + x_f) = -\hat{R}^{-1}(S_2^T + B_2^T K_{\max})x^*$. Thus, the second compo-
599 nent of the optimal input, i.e., u_2^* , is already given in state-feedback form. Therefore,
600 it remains to show that the first component, i.e., u_1^* , admits a formulation in terms of
601 a PD state-feedback. To design this feedback, we need the following assumption.

602 ASSUMPTION 5.3. *Zero eigenvalues of $(A_r - LK_{\max})$, if any, are controllable for*
603 *the pair $(A_r - LK_{\max}, B_r)$, where A_r, L , and B_r are as defined in equation (2.8).³*

604 REMARK 5.4. Recall the matrix $\tilde{W} = [B_r \ A_r B_r \ \dots \ A_r^{\mathfrak{n}_f - \mathfrak{d} - 1} B_r] \tilde{N}$ from equation
605 (5.2). It can be understood from the proof of Lemma 5.1 that the columns of the
606 matrix $\tilde{N} \in \mathbb{R}^{\mathfrak{d}(\mathfrak{n}_f - \mathfrak{d}) \times (\mathfrak{n}_f - \mathfrak{d})}$ form a basis for $\ker \mathcal{M}_t$, where \mathcal{M}_t is obtained by remov-
607 ing the first \mathfrak{d} columns and first \mathfrak{p} rows from \mathcal{M} , that is, $\mathcal{M} = \begin{bmatrix} 0_{\mathfrak{p}, \mathfrak{d}} & 0_{\mathfrak{p}, \mathfrak{d}(\mathfrak{n}_f - \mathfrak{d})} \\ 0_{\mathfrak{p}(\mathfrak{n}_f - \mathfrak{d}), \mathfrak{d}} & \mathcal{M}_t \end{bmatrix}$. It

608 also follows that there exists $W_e \in \mathbb{R}^{\mathfrak{n} \times \mathfrak{d}}$ such that columns of the matrix $[\tilde{W} \ W_e]$ form
609 a basis for the fast space \mathcal{R}_s of the primal. Furthermore, the columns of the matrix
610 $[B_r \ A_r \tilde{W}]$, too, form a basis for \mathcal{R}_s . Therefore, from Statement 1 of Theorem 3.3, it
611 is evident that $X_1 := [V_{1\Lambda} \ \tilde{W} \ W_e]$ and $X_2 := [V_{1\Lambda} \ B_r \ A_r \tilde{W}]$ are non-singular. \square

612 We now prove the titular main result of this paper, which provides a PD feedback
613 controller that solves the singular LQR problem.

³It should be noted here that Assumption 5.3 is not restrictive because of the following reasons:
in the statement of Problem 2.6 we have assumed that the system $\frac{d}{dt}x = Ax + B_1 u_1 + B_2 u_2$ is
stabilizable. The feedback $u_2 = -\hat{R}^{-1}(S_2^T + B_2^T K_{\max})x$ makes sure that \mathfrak{n}_s number of eigenvalues
of A are stabilized (see Lemma 3.1 and Lemma 4.1). With this feedback the closed-loop system
becomes $\frac{d}{dt}x = (A_r - LK_{\max})x + B_1 u_1$. Assumption 5.3 *does not* require existence of a feedback
 $u_1 = Fx$ such that the other $\mathfrak{n}_f = \mathfrak{n} - \mathfrak{n}_s$ eigenvalues are stabilized. It just requires existence of an
 F such that if there are any zero eigenvalues in the remaining \mathfrak{n}_f number of eigenvalues, then those
eigenvalues can be made non-zero via a suitable feedback. Thus, the assumption holds generically.

614 THEOREM 5.5. Let Assumption 5.3 hold. Recall the matrices $X_1 := [V_{1\Lambda} \ \tilde{W} \ w_e]$
615 and $X_2 := [V_{1\Lambda} \ B_r \ A_r \ \tilde{W}]$ from Remark 5.4. Then the following are true:

- 616 1. There exist $g_0 \in \mathbb{R}^{d \times (n_f - d)}$ and $g_1 \in \mathbb{R}^{d \times d}$ such that $(A_r - LK_{\max} + B_r F_p)$ is
617 non-singular, where L is as defined in equation (2.8) and $F_p := [V_{3\Lambda} \ g_0 \ g_1] X_1^{-1}$.
618 2. Define $F_d := [0 \ I_d \ -g_0] X_2^{-1}$ and $F_{reg} := -\hat{R}^{-1}(S_2^T + B_2^T K_{\max})$. Then, the
619 feedback laws $u_1 = F_p x + F_d \frac{d}{dt} x$ and $u_2 = F_{reg} x$ solve the singular LQR
620 Problem 2.6.

621 *Proof.* 1. We first do a similarity transformation on the matrices $(A_r - LK_{\max})$
622 and B_r by the matrix X_2 . From the definition of X_2 , it is easy to verify that

$$623 \quad (5.4) \quad B_t := X_2^{-1} B_r = \begin{bmatrix} 0_{n_s, d} \\ \tilde{B} \end{bmatrix}, \text{ where } \tilde{B} := \begin{bmatrix} I_d \\ 0_{(n_f - d), d} \end{bmatrix}.$$

624 Again, $A_t := X_2^{-1}(A_r - LK_{\max})X_2 = X_2^{-1}(A_r - LK_{\max})[V_{1\Lambda} \ \tilde{W}]$, where $\widehat{W} :=$
625 $[B_r \ A_r \ \tilde{W}]$. Now, using equation (3.1) and equation (5.4), we deduce that

$$626 \quad (5.5) \quad (A_r - LK_{\max})V_{1\Lambda} = A_r V_{1\Lambda} - LV_{2\Lambda} = V_{1\Lambda}\Gamma - B_r V_{3\Lambda} = X_2 \begin{bmatrix} \Gamma \\ A_{21} \end{bmatrix},$$

$$627 \quad \text{where } A_{21} := -\tilde{B}V_{3\Lambda} = \begin{bmatrix} -V_{3\Lambda} \\ 0_{(n_f - d), n_s} \end{bmatrix}.$$

628 Also, using Lemma 3.6 and non-singularity of X_2 , we have

$$629 \quad (5.6) \quad (A_r - LK_{\max})\widehat{W} = A_r \widehat{W} =: X_2 \begin{bmatrix} A_{12} \\ A_{22} \end{bmatrix}, \text{ for some } A_{12} \in \mathbb{R}^{n_s \times n_f}, A_{22} \in \mathbb{R}^{n_f \times n_f}.$$

630 Combining equation (5.5) and equation (5.6), we infer that

$$631 \quad (5.7) \quad A_t = X_2^{-1}(A_r - LK_{\max})X_2 = \begin{bmatrix} \Gamma & A_{12} \\ A_{21} & A_{22} \end{bmatrix}.$$

632 We claim that the pair (A_{22}, \tilde{B}) is such that the zero eigenvalues of A_{22} , if any, are
633 controllable. We prove this claim by contradiction. So, to the contrary, we assume that
634 the claim is false. Thus, by the Popov-Belevitch-Hautus criterion for controllability,
635 there exists $v \in \mathbb{R}^{n_f} \setminus \{0\}$ such that

$$636 \quad (5.8) \quad v^T A_{22} = 0 \text{ and } v^T \tilde{B} = 0.$$

637 Due to the structure of \tilde{B} (see equation (5.4)), we must have $v = \begin{bmatrix} 0_{d, 1} \\ v_2 \end{bmatrix}$ for some
638 $v_2 \in \mathbb{R}^{(n_f - d)} \setminus \{0\}$. Further, non-singularity of X_2 ensures that there exists $w \in \mathbb{R}^n \setminus \{0\}$
639 such that $w^T X_2 = [0_{1, n_s} \ v^T] = [0_{1, (n_s + d)} \ v_2^T]$. Therefore, from equation (5.7), we have

$$640 \quad w^T (A_r - LK_{\max}) = w^T X_2 A_t X_2^{-1} = [0_{1, n_s} \ v^T] \begin{bmatrix} \Gamma & A_{12} \\ A_{21} & A_{22} \end{bmatrix} X_2^{-1} = [v^T A_{21} \ v^T A_{22}] X_2^{-1}.$$

642 But, $v^T A_{21} = [0_{1, d} \ v_2^T] \begin{bmatrix} -V_{3\Lambda} \\ 0_{(n_f - d), n_s} \end{bmatrix} = 0$. Hence, using equation (5.8), we further have

643 $w^T (A_r - LK_{\max}) = 0$. Also, $w^T B_r = w^T X_2 B_t = [0_{1, n_s} \ v^T] \begin{bmatrix} 0_{n_s, d} \\ \tilde{B} \end{bmatrix} = v^T \tilde{B} = 0$. This
644 contradicts Assumption 5.3. Hence, the claim that the zero eigenvalues of A_{22} , if any,
645 are controllable by \tilde{B} must be true. This proves the claim.

646 In view of this claim, it is evident that there exists $\bar{g} \in \mathbb{R}^{d \times n_f}$ such that $(A_{22} + \tilde{B}\bar{g})$ is
647 non-singular. Next, define $F_p := [V_{3\Lambda} \ \bar{g}] X_2^{-1}$. Then, $A_r - LK_{\max} + B_r F_p = X_2(A_t +$
648 $B_t [V_{3\Lambda} \ \bar{g}])X_2^{-1}$, where B_t and A_t are as defined in equation (5.4) and equation (5.7),
649 respectively. Now,

$$650 \quad A_t + B_t [V_{3\Lambda} \ \bar{g}] = \begin{bmatrix} \Gamma & A_{12} \\ A_{21} & A_{22} \end{bmatrix} + \begin{bmatrix} 0_{n_s, n_s} & 0_{n_s, n_f} \\ \tilde{B}V_{3\Lambda} & \tilde{B}\bar{g} \end{bmatrix} = \begin{bmatrix} \Gamma & A_{12} \\ A_{21} + \tilde{B}V_{3\Lambda} & A_{22} + \tilde{B}\bar{g} \end{bmatrix}.$$

651 But, from equation (5.4) and equation (5.5), it is clear that $A_{21} + \tilde{B}V_{3\Lambda} = \begin{bmatrix} -V_{3\Lambda} \\ 0_{(n_f - d), n_s} \end{bmatrix} +$
652 $\begin{bmatrix} V_{3\Lambda} \\ 0_{(n_f - d), n_s} \end{bmatrix} = 0$. Therefore, $A_t + B_t [V_{3\Lambda} \ \bar{g}] = \begin{bmatrix} \Gamma & A_{12} \\ 0 & A_{22} + \tilde{B}\bar{g} \end{bmatrix}$. Since Γ is Hurwitz and

653 $(A_{22} + \tilde{B}\bar{g})$ is non-singular, we must have that $(A_t + B_t [V_{3\Lambda} \bar{g}])$ is non-singular; which
654 further implies that $(A_r - LK_{\max} + B_r F_p)$ is non-singular.
655 Since $\text{im} [B_r \ A_r \ \tilde{W}] = \text{im} [\tilde{W} \ W_e]$, it follows from the structures of X_2 and X_1 that
656 there exists a non-singular matrix $T \in \mathbb{R}^{n_r \times n_r}$ such that $X_2 = X_1 \begin{bmatrix} I_{n_s} & 0 \\ 0 & T^{-1} \end{bmatrix}$. Say,
657 $g_0 \in \mathbb{R}^{d \times (n_r - d)}$ and $g_1 \in \mathbb{R}^{d \times d}$ is defined as $[g_0 \ g_1] := \bar{g}T$. Thus, $F_p = [V_{3\Lambda} \bar{g}] X_2^{-1} =$
658 $[V_{3\Lambda} \bar{g}] \begin{bmatrix} I_{n_s} & 0 \\ 0 & T \end{bmatrix} X_1^{-1} = [V_{3\Lambda} \bar{g}T] X_1^{-1} = [V_{3\Lambda} g_0 \ g_1] X_1^{-1}$. But, we have already proved
659 that $(A_r - LK_{\max} + B_r F_p)$ is non-singular. Hence, there exist $g_0 \in \mathbb{R}^{d \times (n_r - d)}$ and
660 $g_1 \in \mathbb{R}^{d \times d}$ such that $(A_r - LK_{\max} + B_r F_p)$ is non-singular, where $F_p = [V_{3\Lambda} g_0 \ g_1] X_1^{-1}$.
661

2. Recall from Theorem 4.3 that for an arbitrary initial condition x_0 , the optimal trajectory of the primal Σ is given by $\text{col}(x^*, u_1^*, u_2^*)$. Our aim is to show that the feedback laws defined in this theorem restrict the system to exhibit the optimal trajectories only. So, we first show that the optimal trajectories satisfy the system's equation under the proposed feedback laws and then we show that, for a given initial condition, the optimal trajectory is the only trajectory that the system admits. We show that the given feedback laws admit the optimal trajectory in three steps: first, we show that the trajectory $\text{col}(x_s, u_{s_1}, u_{s_2})$ (defined in Lemma 4.1) corresponding to the initial condition $V_{1\Lambda}\alpha$ is an allowable trajectory by the feedback law. Then, we show that the trajectory $\text{col}(x_f, u_{f_1}, u_{f_2})$ (defined in Lemma 4.2) corresponding to the initial condition $W\beta$ is an allowable trajectory, too. Finally, we show that the optimal trajectory $\text{col}(x^*, u_1^*, u_2^*)$ is an allowable trajectory.

Recall that $x_s = V_{1\Lambda}e^{\Gamma t}\alpha$, $u_{s_1} = V_{3\Lambda}e^{\Gamma t}\alpha$, and $u_{s_2} = -\hat{R}^{-1}(S_2^T + B_2^T K_{\max})x_s$. So,

$$F_p x_s + F_d \frac{d}{dt} x_s = (F_p V_{1\Lambda} + F_d V_{1\Lambda} \Gamma) e^{\Gamma t} \alpha.$$

But, from the definition of F_p and F_d , $F_p V_{1\Lambda} = V_{3\Lambda}$ and $F_d V_{1\Lambda} = 0$. Thus,

$$F_p x_s + F_d \frac{d}{dt} x_s = V_{3\Lambda} e^{\Gamma t} \alpha = u_{s_1}.$$

Therefore, from Statement 2 of Lemma 4.1, we infer that

$$A x_s + B_1 (F_p x_s + F_d \frac{d}{dt} x_s) + B_2 F_{reg} x_s = A x_s + B_1 u_{s_1} + B_2 u_{s_2} = \frac{d}{dt} x_s.$$

662 Hence, the feedback law allows the trajectory $\text{col}(x_s, u_{s_1}, u_{s_2})$.
663 Recall that $x_f := -[W_1 \delta + W_2 \delta^{(1)} + \dots + W_{n_r - d} \delta^{(n_r - d - 1)}] \beta$, $u_{f_1} = -[\delta I_d \ \delta^{(1)} I_d \ \dots \ \delta^{(n_r - d)} I_d] N \beta$,
664 and $u_{f_2} := -\hat{R}^{-1}(S_2^T + B_2^T K_{\max}) x_f$, where N is as defined in equation (3.2). Also recall
665 from equation (4.2) that $\frac{d}{dt} x_f = A_r x_f + B_r u_{f_1}$. Hence,

$$\begin{aligned} 666 \quad F_p x_f + F_d \frac{d}{dt} x_f &= -F_p \sum_{i=1}^{n_r - d} W_i \beta \delta^{(i-1)} - F_d A_r \sum_{i=1}^{n_r - d} W_i \beta \delta^{(i-1)} + F_d B_r u_{f_1}. \\ 667 \quad (5.9) \quad &= -\sum_{i=1}^{n_r - d} (F_p W_i + F_d A_r W_i) \beta \delta^{(i-1)} + u_{f_1} \quad (\text{since } F_d B_r = I_d). \end{aligned}$$

668 Partition N as $N = \text{col}(N_0, \bar{N}_1)$ with $N_0 \in \mathbb{R}^{d \times n_r}$ and $\bar{N}_1 \in \mathbb{R}^{d(n_r - d) \times n_r}$. Recall from
669 equation (3.2) and equation (5.1) that $\text{im} \begin{bmatrix} I_d & 0 \\ 0 & \tilde{N} \end{bmatrix} = \ker \mathcal{M} = \text{im } N = \text{im} \begin{bmatrix} N_0 \\ \bar{N}_1 \end{bmatrix} \Rightarrow$
670 $\text{im } \bar{N}_1 = \text{im } \tilde{N}$. Hence, from Lemma 3.10 and Remark 5.4, we infer that $\text{im } W_1 = \text{im } \tilde{W}$.
671 From Lemma 3.10 we further get that $\text{im } W_{n_r - d} \subseteq \text{im } W_{n_r - d - 1} \subseteq \dots \subseteq \text{im } W_1 = \text{im } \tilde{W}$.
672 Therefore, for all $i \in \{1, 2, \dots, (n_r - d)\}$ there exists $T_i \in \mathbb{R}^{(n_r - d) \times n_r}$ such that $W_i =$
673 $\tilde{W} T_i$. Thus, from equation (5.9) we further get that

$$674 \quad F_p x_f + F_d \frac{d}{dt} x_f = -\sum_{i=1}^{n_r - d} (F_p \tilde{W} + F_d A_r \tilde{W}) T_i \beta \delta^{(i-1)} + u_{f_1} = -\sum_{i=1}^{n_r - d} (g_0 - g_0) T_i \beta \delta^{(i-1)} + u_{f_1} = u_{f_1}.$$

Therefore, from Statement 3 of Lemma 4.2, it is clear that

$$Ax_f + B_1(F_p x_f + F_d \frac{d}{dt} x_f) + B_2 F_{reg} x_f = Ax_f + B_1 u_{f_1} + B_2 u_{f_2} = \frac{d}{dt}(x_f).$$

Hence, the feedback laws admit the trajectory (x_f, u_{f_1}, u_{f_2}) . Finally, since $x^* = x_s + x_f$, $u_1^* = u_{s_1} + u_{f_1}$, and $u_2^* = u_{s_2} + u_{f_2}$, using linearity, we conclude that corresponding to an arbitrary initial condition $x_0 = [V_{1\Lambda} \ W] \begin{bmatrix} \alpha \\ \beta \end{bmatrix}$, the optimal trajectory (x^*, u_1^*, u_2^*) is an allowable trajectory by the feedback law. The only thing that remains to be shown is that given an arbitrary initial condition x_0 , the trajectory of the closed-loop system can be uniquely determined. It can be easily seen that the feedback laws mentioned in Statement 2 of this theorem results in the closed-loop system

$$(5.10) \quad \underbrace{(I_n - B_r F_d)}_{E_{CL}} \frac{d}{dt} x(t) = \underbrace{(A_r - LK_{\max} + B_r F_p)}_{A_{CL}} x(t).$$

So, for a given initial condition, the trajectory of the closed-loop system is uniquely determined if and only if the matrix pencil $(sE_{CL} - A_{CL})$ is regular [25]. In Statement 1 of this theorem, we have already shown that $A_{CL} = (A_r - LK_{\max} + B_r F_p)$ is non-singular. Note that, non-singularity of A_{CL} ensures that $\det(sE_{CL} - A_{CL}) \neq 0$ (see [25, Theorem 1.2.1]). Hence, the matrix pencil $(sE_{CL} - A_{CL})$ is regular. Since, we have already showed that given an arbitrary initial condition x_0 , x^* satisfies the equation (5.10), we conclude that the closed-loop system admits the optimal trajectories only. Therefore, the feedback laws given in the Statement 2 of this theorem solve the singular LQR Problem 2.6. \square

6. Regularity and internal stability of the closed-loop system. The optimal PD feedback law provided in Theorem 5.5 results in the closed-loop system as given by equation (5.10). Note that, Assumption 5.3, which we have made in order to design the optimal PD feedback controller, does not necessitate that the partial closed-loop system $(A_r - LK_{\max}, B_r)$ be stabilizable. Therefore, a natural question that arises is: does the optimal feedback law guarantee that the closed-loop system is internally stable? The answer is affirmative. To explain this, we first note that Assumption 5.3 is made in order to guarantee that there exists a feedback matrix F_p as defined in Theorem 5.5 such that A_{CL} is non-singular. This enables us to write the following theorem.

THEOREM 6.1. *The matrix pencil $(sE_{CL} - A_{CL})$ as defined in equation (5.10) is a regular matrix pencil, that is, $\det(sE_{CL} - A_{CL}) \neq 0$.*

Proof Recall from Statement 1 of Theorem 5.5 that A_{CL} is non-singular. Hence, $\det(sE_{CL} - A_{CL}) \neq 0$. \square

Since the matrix E_{CL} is singular (because $E_{CL} B_r = 0$), the closed-loop system is a singular descriptor system. So, in order to show that the closed-loop system is internally stable, we need to consider the notion of stability for a singular descriptor system. The following proposition from [25, Theorem 3.1.1] characterizes such systems, which are asymptotically stable.

PROPOSITION 6.2. Consider the singular descriptor system as given in equation (5.10). Then, the system is asymptotically stable if and only if $\sigma(E_{CL}, A_{CL}) \subseteq \mathbb{C}_-$.

Note that, from Proposition 6.2, it follows that the stability of the closed-loop system is not governed by the eigenvalues of A_{CL} , but rather, by the eigenvalues of the matrix pair (E_{CL}, A_{CL}) . We now show that the closed-loop system is asymptotically stable.

THEOREM 6.3. *The closed-loop system as given in equation (5.10) is asymptotically stable.*

Proof Recall from the definition of F_d that $F_d V_{1\Lambda} = 0$. Hence, $E_{CL} V_{1\Lambda} = V_{1\Lambda}$. So, by equation (3.1) and the definition of F_p , it follows that $A_{CL} V_{1\Lambda} = E_{CL} V_{1\Lambda} \Gamma$. Therefore,

721 $\sigma(\Gamma) \subseteq \sigma(E_{CL}, A_{CL})$. We now show that $\sigma(\Gamma)$ is, in fact, equal to $\sigma(E_{CL}, A_{CL})$; that
722 is, all the slow modes of the closed-loop singular descriptor system are given by the
723 eigenvalues of the matrix Γ . We show this indirectly by utilizing the general expression
724 of an arbitrary trajectory of the closed-loop system.

725 Recall from Theorem 6.1 that the matrix pencil $(sE_{CL} - A_{CL})$ is regular. This
726 further ensures that for an arbitrary initial condition $x_0 = [V_{1\Lambda} \ W] \begin{bmatrix} \alpha \\ \beta \end{bmatrix}$, the trajectory
727 of the closed-loop system is uniquely determined. This trajectory has been shown in
728 Theorem 5.5 to be the optimal trajectory $x^*(t) = V_{1\Lambda} e^{\Gamma t} \alpha - [W_1 \delta + W_2 \delta^{(1)} + \dots +$
729 $W_{n_f - d} \delta^{(n_f - d - 1)}] \beta$. Hence, $\sigma(E_{CL}, A_{CL}) = \sigma(\Gamma) \subseteq \mathbb{C}_-$. Consequently, the closed-loop
730 system is asymptotically stable. Alternatively, since $\sigma(\Gamma) \subseteq \mathbb{C}_-$, we must have that
731 $\lim_{t \rightarrow \infty} x^*(t) = 0$. Thus, the closed-loop system is asymptotically stable. \square
732

733 **7. An illustrative example.** Consider the system $\frac{d}{dt} x(t) = Ax(t) + B_1 u_1(t) +$
734 $B_2 u_2(t)$, where

$$735 \quad A = \begin{bmatrix} 3 & 0 & -2 & 2 & 0 \\ 1 & -3 & 2 & -1 & 5 \\ -2 & 8 & 3 & -1 & -8 \\ -5 & 3 & 2 & -2 & -4 \\ 1 & -5 & 0 & 0 & 6 \end{bmatrix}, B_1 = \begin{bmatrix} 1 & 0 \\ 0 & 1 \\ -1 & -1 \\ -2 & -1 \\ 0 & 1 \end{bmatrix}, \text{ and } B_2 = \begin{bmatrix} -1 & 0 \\ 0 & 1 \\ 0 & -2 \\ 1 & -1 \\ -1 & 2 \end{bmatrix}.$$

736 For an arbitrary initial condition $x_0 = \text{col}(x_{01}, x_{02}, x_{03}, x_{04}, x_{05})$, our objective is to
737 find an optimal input $u^* = \text{col}(u_1^*, u_2^*)$ that minimizes the functional (2.2), where

$$738 \quad Q = \begin{bmatrix} 18 & -4 & 0 & 9 & 13 \\ -4 & 15 & 8 & -6 & -5 \\ 0 & 8 & 6 & -3 & 1 \\ 9 & -6 & -3 & 6 & 6 \\ 13 & -5 & 1 & 6 & 13 \end{bmatrix}, S_2 = \begin{bmatrix} -3 & -6 \\ 9 & 2 \\ 3 & 2 \\ -3 & -4 \\ -6 & -2 \end{bmatrix}, \text{ and } \widehat{R} = \begin{bmatrix} 9 & 0 \\ 0 & 4 \end{bmatrix}.$$

We also design a PD state-feedback for the optimal input.

Note that $\mathbf{d} = \mathbf{m} - \mathbf{r} = 4 - 2 = 2$. We first compute the reduced Hamiltonian matrix pair
 (E_r, H_r) as $E_r = \begin{bmatrix} I_5 & 0 & 0 \\ 0 & I_5 & 0 \\ 0 & 0 & 0_{2,2} \end{bmatrix}$ and $H_r = \begin{bmatrix} A_r & -L & B_r \\ -Q_r & -A_r^T & 0 \\ 0 & B_r^T & 0_{2,2} \end{bmatrix}$, where $A_r := A - B_2 \widehat{R}^{-1} S_2^T$,
 $Q_r := Q - S_2 \widehat{R}^{-1} S_2^T$, $L := B_2 \widehat{R}^{-1} B_2^T$, and $B_r := B_1$. It can be found out that
 $\det(sE_r - H_r) = 64(s^2 - \frac{4}{9})$. Therefore, $2n_s = \text{degdet}(sE_r - H_r) = 2 \Rightarrow n_s = 1$.
Also. $\sigma(E_r, H_r) \cap \mathbb{C}_- = -\frac{2}{3}$.

The good slow space of the Hamiltonian system: Solve $H_r V_\Lambda = E_r V_\Lambda \Gamma$ for
a $V_\Lambda \in \mathbb{R}^{12 \times 1}$, where $\Gamma = -\frac{2}{3}$. It can be verified that $V_\Lambda = \begin{bmatrix} V_{1\Lambda} \\ V_{2\Lambda} \\ V_{3\Lambda} \end{bmatrix}$ with $V_{1\Lambda} =$

$$\begin{bmatrix} 2 \\ 1 \\ -2.8 \\ -9 \\ 3 \end{bmatrix}, V_{2\Lambda} = -38.4 \begin{bmatrix} 2 \\ 1 \\ 0 \\ 1 \\ 0 \end{bmatrix}, \text{ and } V_{3\Lambda} = \begin{bmatrix} 0.4 \\ -\frac{217}{15} \end{bmatrix} \text{ satisfies the equation. Hence, the good}$$

slow space of the Hamiltonian is given by $\mathcal{O}_{wg} = \text{im} \begin{bmatrix} V_{1\Lambda} \\ V_{2\Lambda} \end{bmatrix}$ (see Lemma 3.1).

The fast space of the primal: Since $\text{rank} \begin{bmatrix} Q & 0 & S_2 \\ 0 & 0_{2,2} & 0 \\ S_2^T & 0 & \widehat{R} \end{bmatrix} = 4$, we obtain the ma-
trices $C \in \mathbb{R}^{4 \times 5}$ and $D_2 \in \mathbb{R}^{4 \times 2}$ such that $\begin{bmatrix} Q & 0 & S_2 \\ 0 & 0_{2,2} & 0 \\ S_2^T & 0 & \widehat{R} \end{bmatrix} = \begin{bmatrix} C^T \\ 0_{2,4} \\ D_2^T \end{bmatrix} [C \ 0_{4,2} \ D_2]$. $C =$

$$\begin{bmatrix} -2 & 1 & 0 & -1 & -2 \\ -2 & -2 & -2 & 0 & -2 \\ -1 & 3 & 1 & -1 & -2 \\ -3 & 1 & 1 & -2 & -1 \end{bmatrix} \text{ and } D_2 = \begin{bmatrix} 0 & 0 \\ 0 & 0 \\ 3 & 0 \\ 0 & 2 \end{bmatrix} \text{ provides the desired factorization.}$$

Now, by Lemma 3.2, the dimension of the fast space \mathcal{R}_s of the primal is $\dim \mathcal{R}_s =$
 $n_f = n - n_s = 5 - 1 = 4$. By following Lemma 3.2, we compute a matrix $N \in \mathbb{R}^{6 \times 4}$
which is full column-rank such that $\mathcal{M}N = 0$, where $\mathcal{M} = \begin{bmatrix} 0_{4,2} & 0 & 0 \\ 0 & 0 & C_r B_r \\ 0 & C_r B_r & C_r A_r B_r \end{bmatrix}$ and

$$C_r = C - D_2 \widehat{R}^{-1} S_2^T. \text{ Notice that } N = \begin{bmatrix} N_0 \\ N_1 \\ N_2 \end{bmatrix} \text{ with } N_0 = \begin{bmatrix} 1 & 0 & 0 & 0 \\ 0 & 1 & 0 & 0 \end{bmatrix}, N_1 = \begin{bmatrix} 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 0 \end{bmatrix}, \text{ and}$$

$N_2 = \begin{bmatrix} 0 & 0 & 0 & 1 \\ 0 & 0 & 0 & 0 \end{bmatrix}$ gives the desire result. Compute the matrix W as

$$W = [B_r \ A_r B_r \ A_r^2 B_r] \begin{bmatrix} N_0 \\ N_1 \\ N_2 \end{bmatrix} = \begin{bmatrix} 1 & 0 & 1 & 3 \\ 0 & 1 & 1 & 0 \\ -1 & -1 & -3 & -8 \\ -2 & -1 & -3 & -6 \\ 0 & 1 & 1 & 2 \end{bmatrix}. \text{ Then, } \mathcal{R}_s = \text{im } W.$$

The maximal rank-minimizing solution K_{\max} of the singular LQR LMI: Following Theorem 3.3, we first compute the matrices $X = [V_{1\Lambda} \ W]$ and $Y = [V_{2\Lambda} \ 0_{5,4}]$.

$$\text{Then, } K_{\max} = YX^{-1} = 9.6 \begin{bmatrix} 4 & 2 & 0 & 2 & 0 \\ 2 & 1 & 0 & 1 & 0 \\ 0 & 0 & 0 & 0 & 0 \\ 2 & 1 & 0 & 1 & 0 \\ 0 & 0 & 0 & 0 & 0 \end{bmatrix}.$$

Optimal trajectories: We first compute $\alpha \in \mathbb{R}^1$ and $\beta \in \mathbb{R}^4$ such that $x_0 = [V_{1\Lambda} \ W] \begin{bmatrix} \alpha \\ \beta \end{bmatrix} = X \begin{bmatrix} \alpha \\ \beta \end{bmatrix}$. It can be verified that

$$\alpha = -\frac{1}{4}(2x_{01} + x_{02} + x_{04}) \text{ and } \beta = \begin{bmatrix} \beta_1 \\ \beta_2 \\ \beta_3 \\ \beta_4 \end{bmatrix} = \frac{1}{4} \begin{bmatrix} 16.4x_{01} + 4.2x_{02} + 4x_{03} + 4.2x_{04} + 4x_{05} \\ 16.4x_{01} + 4.2x_{02} + 4x_{03} + 6.2x_{04} + 10x_{05} \\ -14.4x_{01} + 0.8x_{02} - 4x_{03} - 5.2x_{04} - 10x_{05} \\ 2x_{01} - x_{02} + x_{04} + 2x_{05} \end{bmatrix}.$$

Next, we compute W_1 and W_2 as defined in Lemma 3.10. They are found out to be

$$W_1 = [B_r \ A_r B_r] \begin{bmatrix} N_1 \\ N_2 \end{bmatrix} = \begin{bmatrix} 0 & 0 & 1 & 1 \\ 0 & 0 & 0 & 1 \\ 0 & 0 & -1 & -3 \\ 0 & 0 & -2 & -3 \\ 0 & 0 & 0 & 1 \end{bmatrix} \text{ and } W_2 = B_r N_2 = \begin{bmatrix} 0 & 0 & 0 & 1 \\ 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & -1 \\ 0 & 0 & 0 & -2 \\ 0 & 0 & 0 & 0 \end{bmatrix}.$$

Then, by Theorem 4.3, the optimal state trajectory is given by

$$x^*(t) = V_{1\Lambda} e^{\Gamma t} \alpha - W_1 \beta \delta - W_2 \beta \delta^{(1)} = \begin{bmatrix} 2 \\ 1 \\ -2.8 \\ -9 \\ 3 \end{bmatrix} e^{-\frac{2}{3}t} \alpha - \begin{bmatrix} \beta_3 + \beta_4 \\ \beta_4 \\ -\beta_3 - 3\beta_4 \\ -2\beta_3 - 3\beta_4 \\ \beta_4 \end{bmatrix} \delta - \begin{bmatrix} \beta_4 \\ 0 \\ -\beta_4 \\ -2\beta_4 \\ 0 \end{bmatrix} \delta^{(1)}.$$

739 The optimal input is given by $u^*(t) = \text{col}(u_1^*(t), u_2^*(t))$, where

$$740 \quad u_1^*(t) = V_{3\Lambda} e^{\Gamma t} \alpha - [\delta I_2 \quad \delta^{(1)} I_2 \quad \delta^{(2)} I_2] N \beta = \begin{bmatrix} 0.4 \\ -\frac{217}{15} \end{bmatrix} e^{-\frac{2}{3}t} \alpha - \begin{bmatrix} \beta_1 \\ \beta_2 \end{bmatrix} \delta - \begin{bmatrix} \beta_3 \\ 0 \end{bmatrix} \delta^{(1)} - \begin{bmatrix} \beta_4 \\ 0 \end{bmatrix} \delta^{(2)},$$

$$741 \quad u_2^*(t) = -\widehat{R}^{-1}(S_2^T + B_2^T K_{\max}) x^*(t).$$

PD feedback design: Notice that $N = \begin{bmatrix} I_2 & 0 \\ 0 & \widetilde{N} \end{bmatrix}$, where $\widetilde{N} = \begin{bmatrix} 1 & 0 \\ 0 & 0 \\ 0 & 1 \\ 0 & 0 \end{bmatrix}$. Then, we find out matrices $\widetilde{N}_{12} \in \mathbb{R}^{4 \times 2}$ and $\widetilde{N}_{22} \in \mathbb{R}^{2 \times 2}$ such that $\text{im} \begin{bmatrix} \widetilde{N} & \widetilde{N}_{12} \\ 0 & \widetilde{N}_{22} \end{bmatrix} = \text{im } N$. We find out these matrices to be $\widetilde{N}_{12} = \begin{bmatrix} 0 & 0 \\ 1 & 0 \\ 0 & 0 \\ 0 & 0 \end{bmatrix}$ and $\widetilde{N}_{22} = \begin{bmatrix} 0 & 1 \\ 0 & 0 \end{bmatrix}$. Then, by following Theorem 5.5 we first get the matrices $\widetilde{W} = [B_r \ A_r B_r] \widetilde{N}$, $W_e = [B_r \ A_r B_r \ A_r^2 B_r] \begin{bmatrix} \widetilde{N}_{12} \\ \widetilde{N}_{22} \end{bmatrix}$, $X_1 = [V_{1\Lambda} \ \widetilde{W} \ W_e]$, and $X_2 = [V_{1\Lambda} \ B_r \ A_r \widetilde{W}]$. Now, we compute the matrices $F_p = [V_{3\Lambda} \ g_0 \ g_1] X_1^{-1}$ and $F_d = [0 \ I_2 \ -g_0] X_2^{-1}$ with $g_0 = g_1 = 0_{2,2}$ to get

$$F_p = \begin{bmatrix} -0.2 & -0.1 & 0 & -0.1 & 0 \\ \frac{217}{30} & \frac{217}{60} & 0 & \frac{217}{60} & 0 \end{bmatrix} \text{ and } F_d = \begin{bmatrix} 4.1 & 1.05 & 1 & 1.05 & 1 \\ 4.1 & 1.05 & 1 & 1.55 & 2.5 \end{bmatrix}.$$

742 $F_{reg} = -\widehat{R}^{-1}(S_2^T + B_2^T K_{\max}) = \begin{bmatrix} \frac{37}{15} & \frac{1}{15} & -\frac{1}{3} & 1.4 & \frac{2}{3} \\ 1.5 & -0.5 & -0.5 & 1 & 0.5 \end{bmatrix}$. Then, the feedback law $u_1 =$

743 $F_p x(t) + F_d \frac{d}{dt} x(t)$, $u_2 = F_{reg} x(t)$ solves the given singular LQR problem.

744 The closed-loop system is given by $E_{CL} \frac{d}{dt} x(t) = A_{CL} x(t)$, where $E_{CL} = (I_5 - B_r F_d)$
745 and $A_{CL} = (A_r - L K_{\max} + B_r F_p)$. It can be verified that $\det(s E_{CL} - A_{CL}) =$
746 $-\frac{71}{12}(s + \frac{2}{3})$, that is, the matrix pencil $(s E_{CL} - A_{CL})$ is regular.

747 **Simulation result:** For the given singular LQR problem, we use the feedback law
748 $u_1 = F_p x(t) + F_d \frac{d}{dt} x(t)$, $u_2 = F_{reg} x(t)$ to the primal. Then, for the initial condition
749 $x_0 = [0 \ -1 \ 1.2 \ -3 \ 1]^T$ the system exhibits the trajectory as shown in Figure 1. For

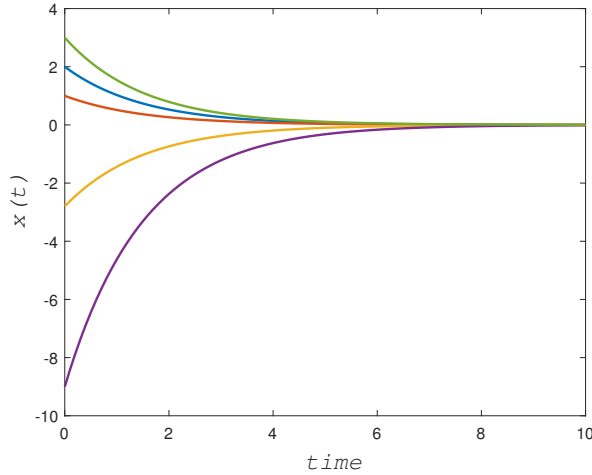


FIG. 1. The state trajectory under the optimal PD feedback law for the illustrative example

750 the given initial condition, the optimal trajectory is analytically found to be $x^*(t) =$
751 $\begin{bmatrix} 2 \\ 1 \\ -2.8 \\ -9 \\ 3 \end{bmatrix} e^{-\frac{2}{3}t}$. The trajectory shown in the figure matches with this trajectory.

752 **8. Comparison with the existing results in the literature.** In this section
753 we compare our results with the ones presented in [4] and [5]. We show that the result
754 presented in this paper overcomes the restrictions of the aforementioned works.

755 **8.1. Comparison with the result presented in [4].** In [4], the authors provide
756 a polynomial matrix based method to design a PD feedback controller that solves
757 a given singular LQR problem. But, unfortunately, the result presented there has several
758 shortcomings which we discuss next.

- 759 • The most important shortcoming of [4] is that it cannot account for arbitrary initial
760 conditions, which is not desirable; because the initial condition of a state space
761 system should ideally be free. [4] considers only those initial conditions for which
762 the optimal state does not contain any impulses, while the optimal input may
763 contain δ , but never $\delta^{(1)}$ or any higher derivatives. The authors call such initial
764 conditions which does not satisfy this condition the *inadmissible* initial conditions.
765 Using the results presented in our paper, it can be shown that such a condition is
766 satisfied if and only if the initial condition belongs to the subspace $\text{im} [V_{1\Lambda} \ B_r]$.
767 On the other hand, the result presented in this paper does not impose any restriction
768 on the initial condition of the system.
- 769 • The applicability of the result in [4] needs the system to be controllable. However,
770 the result presented here needs only stabilizability of the system, which is a standard
771 assumption in the literature.
- 772 • Another assumption of [4] that we do not need in this paper is the observability of
773 the pair (Q, A) .

774 **8.2. Comparison with the result presented in [5].** The deflating subspace
775 based method presented in [5] assumes that the states and the inputs of the system are
776 from the space of locally square-integrable functions, that is, $\mathfrak{L}_2^{\text{loc}}$. This assumption,
777 in turn, imposes a restriction on the initial condition x_0 of the system. This is due to
778 the fact that for an arbitrary x_0 , the optimal trajectory of a singular LQR problem is
779 distributional in nature, that is, it contains impulses and its derivatives [3]. Therefore,

780 the optimal trajectory does not belong to the space $\mathfrak{L}_2^{\text{loc}}$. Even though the cost
781 functional can be made arbitrarily close to the optimal cost, it will never achieve the
782 optimal cost using an input from $\mathfrak{L}_2^{\text{loc}}$. As has been shown in the illustrative example
783 in Section 7 that corresponding to an arbitrary initial condition $x_0 = V_{1\Lambda}\alpha + W\beta$,
784 both the optimal state x^* and the optimal input $u^* = \text{col}(u_1^*, u_2^*)$ are distributional
785 in nature and hence do not belong to $\mathfrak{L}_2^{\text{loc}}$. It can be easily verified that the optimal
786 state and the optimal input belongs to $\mathfrak{L}_2^{\text{loc}}$ only if $\beta = 0$, that is, the initial condition
787 is restricted to the subspace $\text{im } V_{1\Lambda}$.

788 The most important advantage of the result presented here is the implementability
789 of the optimal input as a PD state-feedback over the implicit control law of the form
790 $Px + Tu = 0$ as presented in [5]. To demonstrate this, we use the same example that
791 has been presented in Section 7. Following the method presented in [5], we evaluate
792 $\mathcal{L}_t(K)$ defined in equation 2.3 at K_{\max} and then obtain a factorization of $\mathcal{L}_t(K_{\max})$ as

$$793 \quad \mathcal{L}_t(K_{\max}) = \begin{bmatrix} A^T K_{\max} + K_{\max} A + Q & K_{\max} B_1 & K_{\max} B_2 + S_2 \\ B_1^T K_{\max} & 0 & 0 \\ B_2^T K_{\max} + S_2^T & 0 & \hat{R} \end{bmatrix} = \begin{bmatrix} P^T \\ T_1^T \\ T_2^T \end{bmatrix} [P \ T_1 \ T_2]$$

794 with $P \in \mathbb{R}^{4 \times 5}$ and $T_1, T_2 \in \mathbb{R}^{4 \times 2}$. It can be verified that

$$795 \quad P = \begin{bmatrix} -9.732429 & -1.4724515 & 0.059265 & -4.895847 & -3.3048654 \\ -0.2425838 & -3.5039419 & -2.4053162 & 1.0813662 & -0.2253242 \\ 0.1039512 & -0.4134482 & 0.2850169 & -0.0905329 & 0.8929492 \\ -0.1008634 & -0.6191429 & 0.3601488 & -0.2305061 & 1.1089344 \end{bmatrix},$$

$$796 \quad T_1 = \begin{bmatrix} 0 & 0 \\ 0 & 0 \\ 0 & 0 \\ 0 & 0 \end{bmatrix}, \text{ and } T_2 = \begin{bmatrix} 2.323045 & 0.6121941 \\ -0.9972075 & -0.8357937 \\ 1.6152251 & -1.4021297 \\ 0.0093261 & 0.9801527 \end{bmatrix}$$

797 achieve the desired factorization. Therefore, the control law proposed in [5] is given by
798 $Px + T_1 u_1 + T_2 u_2 = 0$, that is, $Px + T_2 u_2 = 0$. Note that, the optimal trajectory that
799 has been evaluated in the illustrated example also satisfies this control law. However,
800 this control law, unfortunately, cannot be implemented as a feedback law, because the
801 law does not provide any information about the input u_1 . On the other hand, using
802 the method presented in this paper, we have provided a PD feedback controller that
803 solves the singular LQR problem given in Section 7. A feedback controller is always
804 advantageous from an engineering point of view, which is bolstered by [6].

805 **9. Conclusion.** In this paper, we first presented a method to compute the max-
806 imal rank-minimizing solution of the LMI arising from a singular LQR problem (The-
807 orem 3.3). We have developed this method using the notions of slow space (weakly
808 unobservable subspace) of the Hamiltonian system and the fast space (strongly reach-
809 able subspace) of the primal. We have shown that augmenting the basis of the good
810 slow space of the Hamiltonian system Σ_{Ham} with the basis of the fast space of the pri-
811 mal Σ is the crucial idea that leads to the method. Using the maximal rank-minimizing
812 solution, we computed the optimal trajectories for the singular LQR problem. Finally,
813 we provided a feedback law of the form $u = F_p x + F_d \frac{d}{dt} x$, i.e., a PD feedback that
814 solves the singular LQR problem. This work makes use of the ideas introduced in [3],
815 [16], [17] that used impulsive-smooth distributions as the function-space for the states
816 and inputs. Such a setting seems particularly advantageous for differential-algebraic
817 systems, since such systems inherently admit impulsive states. Hence, the approach
818 adapted in this paper to solve singular LQR problems for state-space systems have
819 the potential of being generalized to differential-algebraic systems as well. This will
820 be a matter of our future research.

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