

Phasors

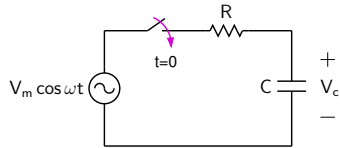


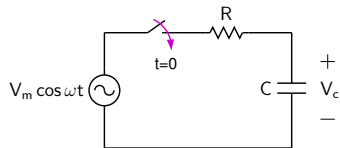
M. B. Patil

mbpatil@ee.iitb.ac.in

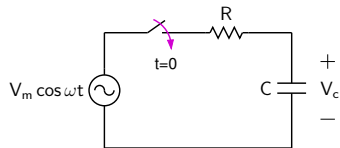
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Department of Electrical Engineering
Indian Institute of Technology Bombay



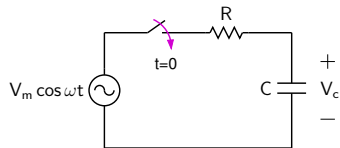


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The solution $V_c(t)$ is made up of two components, $V_c(t) = V_c^{(h)}(t) + V_c^{(p)}(t)$.

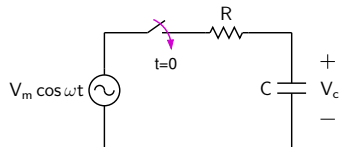


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The solution $V_c(t)$ is made up of two components, $V_c(t) = V_c^{(h)}(t) + V_c^{(p)}(t)$. $V_c^{(h)}(t)$ satisfies the homogeneous differential equation,

$$R C V_c' + V_c = 0, \quad (2)$$

from which, $V_c^{(h)}(t) = A \exp(-t/\tau)$, with $\tau = RC$.



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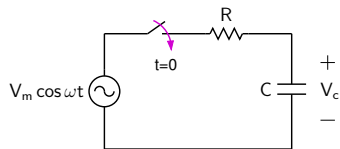
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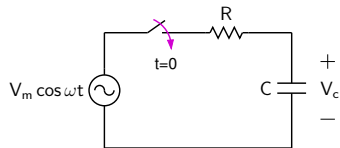
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Substituting in (1), we get,

$$\omega R C (-C_1 \sin \omega t + C_2 \cos \omega t) + C_1 \cos \omega t + C_2 \sin \omega t = V_m \cos \omega t.$$



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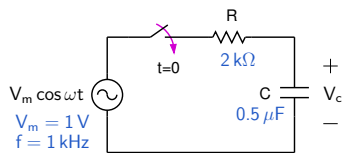
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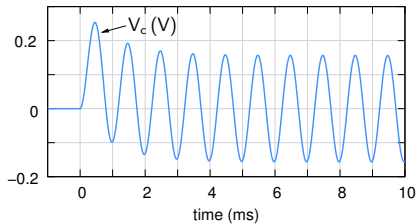
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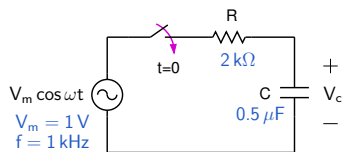
C_1 and C_2 can be found by equating the coefficients of $\sin \omega t$ and $\cos \omega t$ on the left and right sides.

Sinusoidal steady state

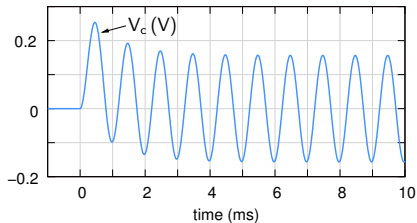


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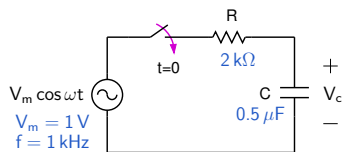




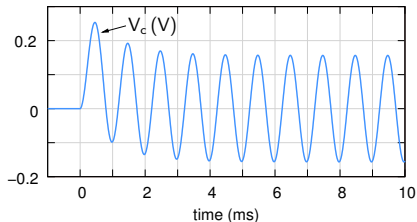
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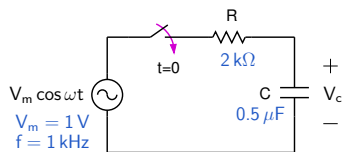


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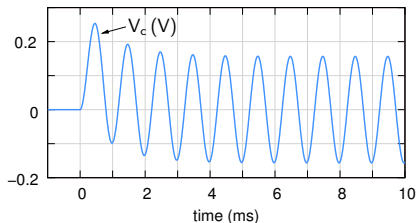


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- * As $t \rightarrow \infty$, the exponential term becomes zero, and we are left with $V_c(t) = C_1 \cos \omega t + C_2 \sin \omega t$.

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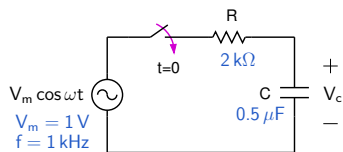


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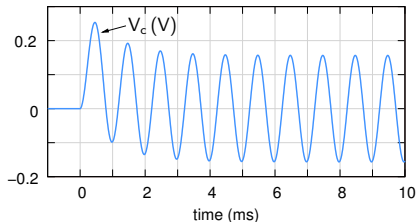


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- * This is known as the “sinusoidal steady state” response since all quantities (currents and voltages) in the circuit are sinusoidal in nature.

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- * This is known as the “sinusoidal steady state” response since all quantities (currents and voltages) in the circuit are sinusoidal in nature.
- * Any circuit containing resistors, capacitors, inductors, sinusoidal voltage and current sources (of the same frequency), dependent (linear) sources behaves in a similar manner, viz., each current and voltage in the circuit becomes purely sinusoidal as $t \rightarrow \infty$.

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 $\mathbf{X} = X_m \angle \theta = X_m \exp(j\theta)$,
with the following interpretation in the time domain.

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Sinusoidal steady state: phasors

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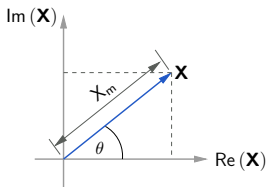
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* Note that a phasor can be written in the polar form or rectangular form,

$$\mathbf{X} = X_m \angle \theta = X_m \exp(j\theta) = X_m \cos \theta + j X_m \sin \theta.$$

The term ωt is always *implicit*.



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Consider addition of two sinusoidal quantities:

$$\begin{aligned}v(t) &= v_1(t) + v_2(t) \\ &= V_{m1} \cos(\omega t + \theta_1) + V_{m2} \cos(\omega t + \theta_2)\end{aligned}$$

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$$\begin{aligned}\tilde{v}(t) &= \text{Re} [\mathbf{V}e^{j\omega t}] \\ &= \text{Re} [(V_{m1}e^{j\theta_1} + V_{m2}e^{j\theta_2}) e^{j\omega t}] \\ &= \text{Re} [V_{m1}e^{j(\omega t + \theta_1)} + V_{m2}e^{j(\omega t + \theta_2)}]\end{aligned}$$

Consider addition of two sinusoidal quantities:

$$\begin{aligned}v(t) &= v_1(t) + v_2(t) \\ &= V_{m1} \cos(\omega t + \theta_1) + V_{m2} \cos(\omega t + \theta_2)\end{aligned}$$

Now consider addition of the phasors corresponding to $v_1(t)$ and $v_2(t)$.

$$\begin{aligned}\mathbf{V} &= \mathbf{V}_1 + \mathbf{V}_2 \\ &= V_{m1} e^{j\theta_1} + V_{m2} e^{j\theta_2}\end{aligned}$$

In the time domain, \mathbf{V} corresponds to $\tilde{v}(t)$, with

$$\begin{aligned}\tilde{v}(t) &= \text{Re} [\mathbf{V} e^{j\omega t}] \\ &= \text{Re} [(V_{m1} e^{j\theta_1} + V_{m2} e^{j\theta_2}) e^{j\omega t}] \\ &= \text{Re} [V_{m1} e^{j(\omega t + \theta_1)} + V_{m2} e^{j(\omega t + \theta_2)}] \\ &= V_{m1} \cos(\omega t + \theta_1) + V_{m2} \cos(\omega t + \theta_2)\end{aligned}$$

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which is the same as $v(t)$.

- * Addition of sinusoidal quantities in the time domain can be replaced by addition of the corresponding phasors in the sinusoidal steady state.

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- * The KCL and KVL equations,

$$\sum i_k(t) = 0 \text{ at a node, and}$$

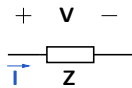
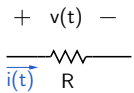
$$\sum v_k(t) = 0 \text{ in a loop,}$$

amount to addition of sinusoidal quantities and can therefore be replaced by the corresponding phasor equations,

$$\sum \mathbf{I}_k = \mathbf{0} \text{ at a node, and}$$

$$\sum \mathbf{V}_k = \mathbf{0} \text{ in a loop.}$$

Impedance of a resistor



Impedance of a resistor



Let $i(t) = I_m \cos(\omega t + \theta)$.

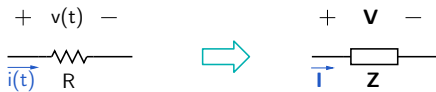
Impedance of a resistor



$$\text{Let } i(t) = I_m \cos(\omega t + \theta).$$

$$v(t) = R i(t)$$

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$$\begin{aligned}v(t) &= R i(t) \\ &= R I_m \cos(\omega t + \theta) \\ &\equiv V_m \cos(\omega t + \theta).\end{aligned}$$

The phasors corresponding to $i(t)$ and $v(t)$ are, respectively,

$$\mathbf{I} = I_m \angle \theta, \quad \mathbf{V} = R \times I_m \angle \theta.$$

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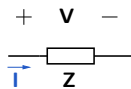
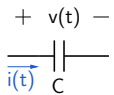
$$\mathbf{I} = I_m \angle \theta, \quad \mathbf{V} = R \times I_m \angle \theta.$$

We have therefore the following relationship between \mathbf{V} and \mathbf{I} : $\mathbf{V} = R \times \mathbf{I}$.

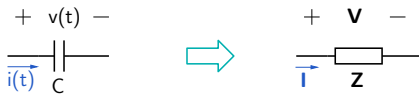
Thus, the *impedance* of a resistor, defined as, $\mathbf{Z} = \mathbf{V}/\mathbf{I}$, is

$$\mathbf{Z} = R + j0$$

Impedance of a capacitor

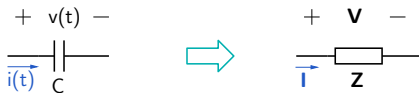


Impedance of a capacitor



Let $v(t) = V_m \cos(\omega t + \theta)$.

Impedance of a capacitor



$$\text{Let } v(t) = V_m \cos(\omega t + \theta).$$

$$i(t) = C \frac{dv}{dt} = -C \omega V_m \sin(\omega t + \theta).$$

Impedance of a capacitor



Let $v(t) = V_m \cos(\omega t + \theta)$.

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Using the identity, $\cos(\phi + \pi/2) = -\sin \phi$, we get

$$i(t) = C \omega V_m \cos(\omega t + \theta + \pi/2).$$

Impedance of a capacitor



Let $v(t) = V_m \cos(\omega t + \theta)$.

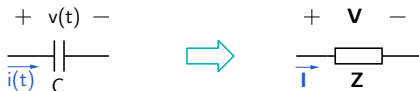
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In terms of phasors, $\mathbf{V} = V_m \angle \theta$, $\mathbf{I} = \omega C V_m \angle (\theta + \pi/2)$.

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\mathbf{I} can be rewritten as,

$$\mathbf{I} = \omega C V_m e^{j(\theta + \pi/2)} = \omega C V_m e^{j\theta} e^{j\pi/2} = j\omega C (V_m e^{j\theta}) = j\omega C \mathbf{V}$$

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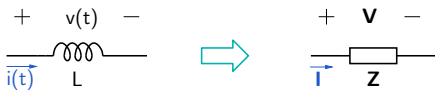
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Thus, the *impedance* of a capacitor, $\mathbf{Z} = \mathbf{V}/\mathbf{I}$, is $\boxed{\mathbf{Z} = 1/(j\omega C)}$,

and the *admittance* of a capacitor, $\mathbf{Y} = \mathbf{I}/\mathbf{V}$, is $\boxed{\mathbf{Y} = j\omega C}$.

Impedance of an inductor



Impedance of an inductor



Let $i(t) = I_m \cos(\omega t + \theta)$.

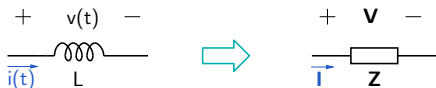
Impedance of an inductor



$$\text{Let } i(t) = I_m \cos(\omega t + \theta).$$

$$v(t) = L \frac{di}{dt} = -L\omega I_m \sin(\omega t + \theta).$$

Impedance of an inductor



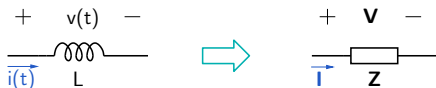
Let $i(t) = I_m \cos(\omega t + \theta)$.

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Using the identity, $\cos(\phi + \pi/2) = -\sin \phi$, we get

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Impedance of an inductor



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In terms of phasors, $\mathbf{I} = I_m \angle \theta$, $\mathbf{V} = \omega L I_m \angle (\theta + \pi/2)$.

Impedance of an inductor



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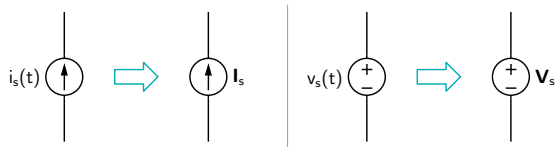
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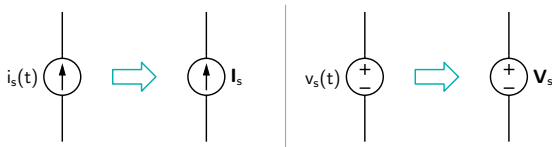
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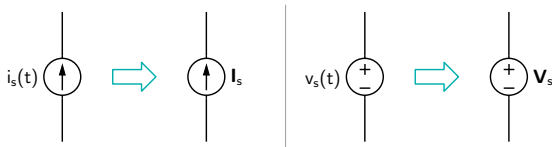
Thus, the *impedance* of an inductor, $\mathbf{Z} = \mathbf{V}/\mathbf{I}$, is $\boxed{\mathbf{Z} = j\omega L}$,

and the *admittance* of an inductor, $\mathbf{Y} = \mathbf{I}/\mathbf{V}$, is $\boxed{\mathbf{Y} = 1/(j\omega L)}$.

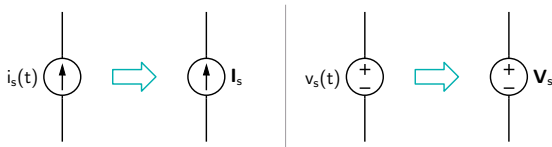




- * An independent sinusoidal current source, $i_s(t) = I_m \cos(\omega t + \theta)$, can be represented by the phasor $I_m \angle \theta$ (i.e., a *constant* complex number).



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- * Dependent (linear) sources can be treated in the sinusoidal steady state in the same manner as a resistor, i.e., by the corresponding phasor relationship.
For example, for a CCVS, we have,
 $v(t) = r i_c(t)$ in the time domain.
 $\mathbf{V} = r \mathbf{I}_c$ in the frequency domain.

- * The time-domain KCL and KVL equations $\sum i_k(t) = 0$ and $\sum v_k(t) = 0$ can be written as $\sum \mathbf{I}_k = \mathbf{0}$ and $\sum \mathbf{V}_k = \mathbf{0}$ in the frequency domain.

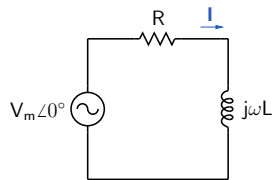
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- * Resistors, capacitors, and inductors can be described by $\mathbf{V} = \mathbf{Z}\mathbf{I}$ in the frequency domain, which is similar to $V = RI$ in DC conditions (except that we are dealing with complex numbers in the frequency domain).

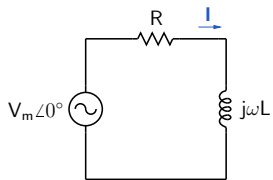
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- * Circuit analysis in the sinusoidal steady state using phasors is therefore very similar to DC circuits with independent and dependent sources, and resistors.

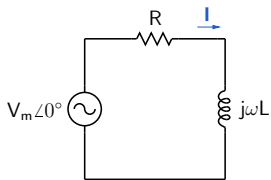
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- * Resistors, capacitors, and inductors can be described by $\mathbf{V} = \mathbf{Z}\mathbf{I}$ in the frequency domain, which is similar to $V = RI$ in DC conditions (except that we are dealing with complex numbers in the frequency domain).
- * An independent sinusoidal source in the frequency domain behaves like a DC source, e.g., $\mathbf{V}_s = \text{constant}$ (a complex number).
- * For dependent sources, a time-domain relationship such as $i(t) = \beta i_c(t)$ translates to $\mathbf{I} = \beta \mathbf{I}_c$ in the frequency domain.
- * Circuit analysis in the sinusoidal steady state using phasors is therefore very similar to DC circuits with independent and dependent sources, and resistors.
- * Series/parallel formulas for resistors, nodal analysis, mesh analysis, Thevenin's and Norton's theorems can be directly applied to circuits in the sinusoidal steady state.





$$I = \frac{V_m \angle 0}{R + j\omega L} \equiv I_m \angle (-\theta),$$

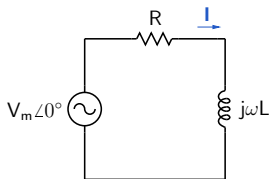
$$\text{where } I_m = \frac{V_m}{\sqrt{R^2 + \omega^2 L^2}}, \text{ and } \theta = \tan^{-1}(\omega L/R).$$



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In the time domain, $i(t) = I_m \cos(\omega t - \theta)$, which *lags* the source voltage since the peak (or zero) of $i(t)$ occurs $t = \theta/\omega$ seconds after that of the source voltage.



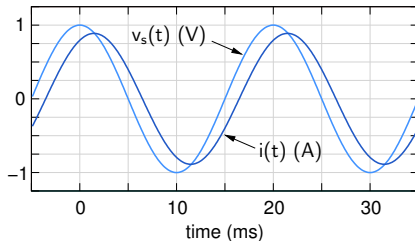
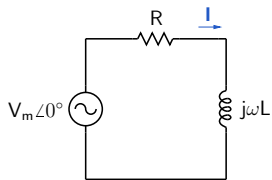
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For $R = 1 \Omega$, $L = 1.6 \text{ mH}$, $f = 50 \text{ Hz}$, $\theta = 26.6^\circ$, $t_{\text{lag}} = 1.48 \text{ ms}$.

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$$R = 1 \Omega$$

$$L = 1.6 \text{ mH}$$

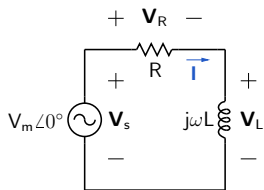
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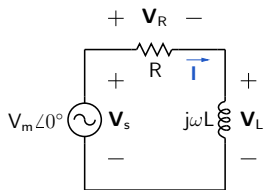
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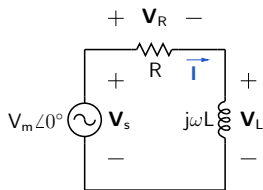


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$$\mathbf{V}_R = \mathbf{I} \times R = R I_m \angle(-\theta),$$

$$\mathbf{V}_L = \mathbf{I} \times j\omega L = \omega I_m L \angle(-\theta + \pi/2),$$



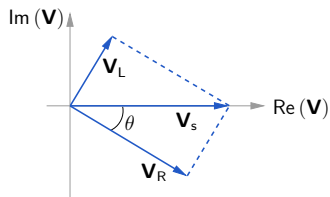
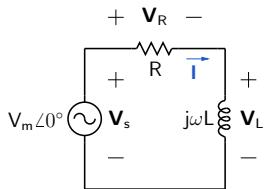
$$\mathbf{I} = \frac{V_m \angle 0}{R + j\omega L} \equiv I_m \angle (-\theta),$$

$$\text{where } I_m = \frac{V_m}{\sqrt{R^2 + \omega^2 L^2}}, \text{ and } \theta = \tan^{-1}(\omega L/R).$$

$$\mathbf{V}_R = \mathbf{I} \times R = R I_m \angle (-\theta),$$

$$\mathbf{V}_L = \mathbf{I} \times j\omega L = \omega I_m L \angle (-\theta + \pi/2),$$

The KVL equation, $\mathbf{V}_s = \mathbf{V}_R + \mathbf{V}_L$, can be represented in the complex plane by a “phasor diagram.”



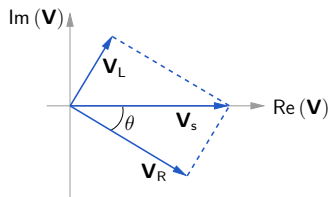
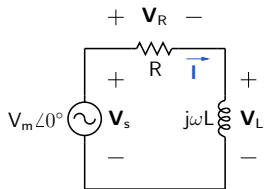
$$\mathbf{I} = \frac{V_m \angle 0}{R + j\omega L} \equiv I_m \angle (-\theta),$$

$$\text{where } I_m = \frac{V_m}{\sqrt{R^2 + \omega^2 L^2}}, \text{ and } \theta = \tan^{-1}(\omega L/R).$$

$$\mathbf{V}_R = \mathbf{I} \times R = R I_m \angle (-\theta),$$

$$\mathbf{V}_L = \mathbf{I} \times j\omega L = \omega I_m L \angle (-\theta + \pi/2),$$

The KVL equation, $\mathbf{V}_s = \mathbf{V}_R + \mathbf{V}_L$, can be represented in the complex plane by a “phasor diagram.”



$$\mathbf{I} = \frac{V_m \angle 0}{R + j\omega L} \equiv I_m \angle (-\theta),$$

$$\text{where } I_m = \frac{V_m}{\sqrt{R^2 + \omega^2 L^2}}, \text{ and } \theta = \tan^{-1}(\omega L/R).$$

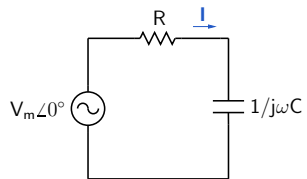
$$\mathbf{V}_R = \mathbf{I} \times R = R I_m \angle (-\theta),$$

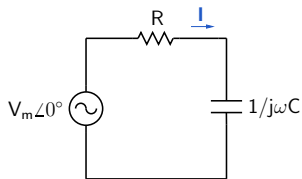
$$\mathbf{V}_L = \mathbf{I} \times j\omega L = \omega I_m L \angle (-\theta + \pi/2),$$

The KVL equation, $\mathbf{V}_s = \mathbf{V}_R + \mathbf{V}_L$, can be represented in the complex plane by a “phasor diagram.”

If $R \gg |j\omega L|$, $\theta \rightarrow 0$, $|\mathbf{V}_R| \simeq |\mathbf{V}_s| = V_m$.

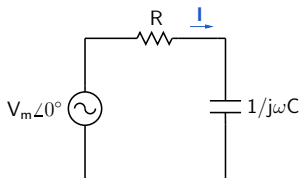
If $R \ll |j\omega L|$, $\theta \rightarrow \pi/2$, $|\mathbf{V}_L| \simeq |\mathbf{V}_s| = V_m$.





$$I = \frac{V_m \angle 0}{R + 1/j\omega C} \equiv I_m \angle \theta,$$

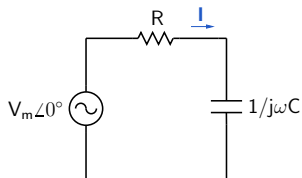
$$\text{where } I_m = \frac{\omega C V_m}{\sqrt{1 + (\omega RC)^2}}, \text{ and } \theta = \pi/2 - \tan^{-1}(\omega RC).$$



$$I = \frac{V_m \angle 0}{R + 1/j\omega C} \equiv I_m \angle \theta,$$

$$\text{where } I_m = \frac{\omega C V_m}{\sqrt{1 + (\omega RC)^2}}, \text{ and } \theta = \pi/2 - \tan^{-1}(\omega RC).$$

In the time domain, $i(t) = I_m \cos(\omega t + \theta)$, which *leads* the source voltage since the peak (or zero) of $i(t)$ occurs $t = \theta/\omega$ seconds before that of the source voltage.



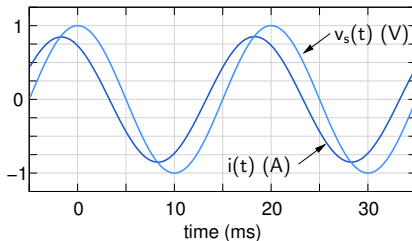
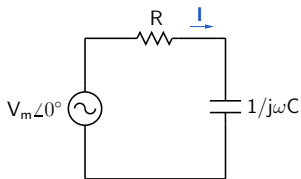
$$I = \frac{V_m \angle 0}{R + 1/j\omega C} \equiv I_m \angle \theta,$$

$$\text{where } I_m = \frac{\omega C V_m}{\sqrt{1 + (\omega RC)^2}}, \text{ and } \theta = \pi/2 - \tan^{-1}(\omega RC).$$

In the time domain, $i(t) = I_m \cos(\omega t + \theta)$, which *leads* the source voltage since the peak (or zero) of $i(t)$ occurs $t = \theta/\omega$ seconds before that of the source voltage.

For $R = 1 \Omega$, $C = 5.3 \text{ mF}$, $f = 50 \text{ Hz}$, $\theta = 31^\circ$, $t_{\text{lead}} = 1.72 \text{ ms}$.

(SEQUEL file: ee101_rc_ac_1.sqproj)



$$R = 1 \Omega$$

$$C = 5.3 \text{ mF}$$

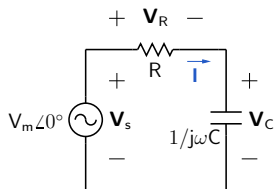
$$\mathbf{I} = \frac{V_m \angle 0}{R + 1/j\omega C} \equiv I_m \angle \theta,$$

$$\text{where } I_m = \frac{\omega C V_m}{\sqrt{1 + (\omega RC)^2}}, \text{ and } \theta = \pi/2 - \tan^{-1}(\omega RC).$$

In the time domain, $i(t) = I_m \cos(\omega t + \theta)$, which *leads* the source voltage since the peak (or zero) of $i(t)$ occurs $t = \theta/\omega$ seconds before that of the source voltage.

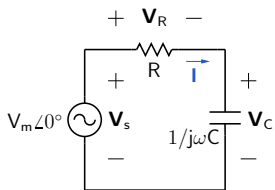
For $R = 1 \Omega$, $C = 5.3 \text{ mF}$, $f = 50 \text{ Hz}$, $\theta = 31^\circ$, $t_{\text{lead}} = 1.72 \text{ ms}$.

(SEQUEL file: ee101_rc_ac.1.sqproj)



$$\mathbf{I} = \frac{V_m \angle 0}{R + 1/j\omega C} \equiv I_m \angle \theta,$$

$$\text{where } I_m = \frac{\omega C V_m}{\sqrt{1 + (\omega RC)^2}}, \text{ and } \theta = \pi/2 - \tan^{-1}(\omega RC).$$

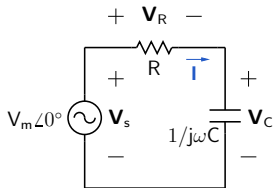


$$I = \frac{V_m \angle 0}{R + 1/j\omega C} \equiv I_m \angle \theta,$$

$$\text{where } I_m = \frac{\omega C V_m}{\sqrt{1 + (\omega RC)^2}}, \text{ and } \theta = \pi/2 - \tan^{-1}(\omega RC).$$

$$V_R = I \times R = R I_m \angle \theta,$$

$$V_C = I \times (1/j\omega C) = (I_m/\omega C) \angle (\theta - \pi/2),$$



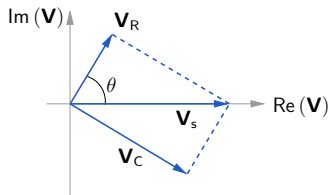
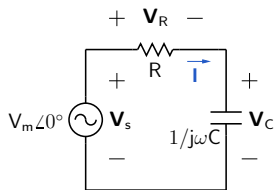
$$I = \frac{V_m \angle 0}{R + 1/j\omega C} \equiv I_m \angle \theta,$$

$$\text{where } I_m = \frac{\omega C V_m}{\sqrt{1 + (\omega RC)^2}}, \text{ and } \theta = \pi/2 - \tan^{-1}(\omega RC).$$

$$V_R = I \times R = R I_m \angle \theta,$$

$$V_C = I \times (1/j\omega C) = (I_m/\omega C) \angle (\theta - \pi/2),$$

The KVL equation, $V_s = V_R + V_C$, can be represented in the complex plane by a “phasor diagram.”



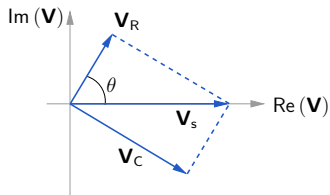
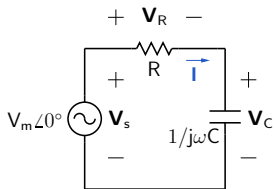
$$\mathbf{I} = \frac{V_m \angle 0}{R + 1/j\omega C} \equiv I_m \angle \theta,$$

$$\text{where } I_m = \frac{\omega C V_m}{\sqrt{1 + (\omega RC)^2}}, \text{ and } \theta = \pi/2 - \tan^{-1}(\omega RC).$$

$$\mathbf{V}_R = \mathbf{I} \times R = R I_m \angle \theta,$$

$$\mathbf{V}_C = \mathbf{I} \times (1/j\omega C) = (I_m/\omega C) \angle (\theta - \pi/2),$$

The KVL equation, $\mathbf{V}_s = \mathbf{V}_R + \mathbf{V}_C$, can be represented in the complex plane by a “phasor diagram.”



$$\mathbf{I} = \frac{V_m \angle 0}{R + 1/j\omega C} \equiv I_m \angle \theta,$$

$$\text{where } I_m = \frac{\omega C V_m}{\sqrt{1 + (\omega RC)^2}}, \text{ and } \theta = \pi/2 - \tan^{-1}(\omega RC).$$

$$\mathbf{V}_R = \mathbf{I} \times R = R I_m \angle \theta,$$

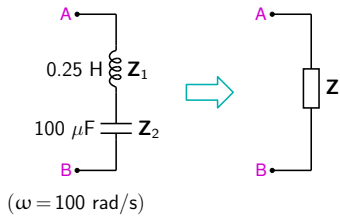
$$\mathbf{V}_C = \mathbf{I} \times (1/j\omega C) = (I_m/\omega C) \angle (\theta - \pi/2),$$

The KVL equation, $\mathbf{V}_s = \mathbf{V}_R + \mathbf{V}_C$, can be represented in the complex plane by a “phasor diagram.”

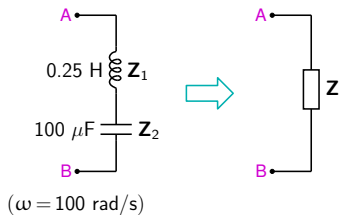
If $R \gg |1/j\omega C|$, $\theta \rightarrow 0$, $|\mathbf{V}_R| \simeq |\mathbf{V}_s| = V_m$.

If $R \ll |1/j\omega C|$, $\theta \rightarrow \pi/2$, $|\mathbf{V}_C| \simeq |\mathbf{V}_s| = V_m$.

Series/parallel connections



Series/parallel connections

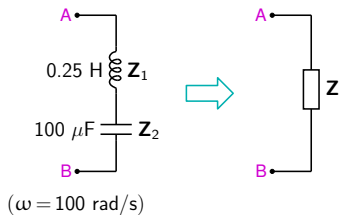


$$\mathbf{Z}_1 = j \times 100 \times 0.25 = j25\ \Omega$$

$$\mathbf{Z}_2 = -j / (100 \times 100 \times 10^{-6}) = -j100\ \Omega$$

$$\mathbf{Z} = \mathbf{Z}_1 + \mathbf{Z}_2 = -j75\ \Omega$$

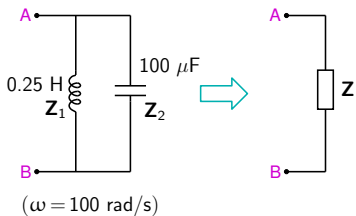
Series/parallel connections

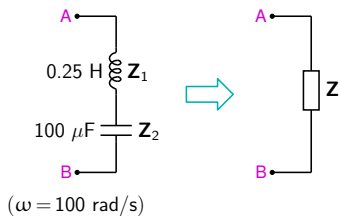


$$Z_1 = j \times 100 \times 0.25 = j25\ \Omega$$

$$Z_2 = -j / (100 \times 100 \times 10^{-6}) = -j100\ \Omega$$

$$Z = Z_1 + Z_2 = -j75\ \Omega$$

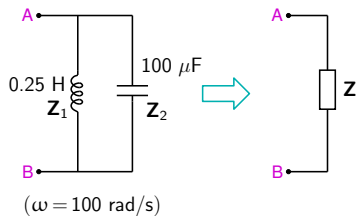




$$\mathbf{Z}_1 = j \times 100 \times 0.25 = j25 \Omega$$

$$\mathbf{Z}_2 = -j / (100 \times 100 \times 10^{-6}) = -j100 \Omega$$

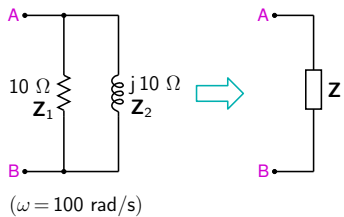
$$\mathbf{Z} = \mathbf{Z}_1 + \mathbf{Z}_2 = -j75 \Omega$$



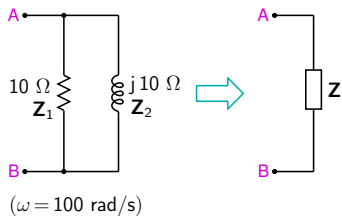
$$\begin{aligned} \mathbf{Z} &= \frac{\mathbf{Z}_1 \mathbf{Z}_2}{\mathbf{Z}_1 + \mathbf{Z}_2} \\ &= \frac{(j25) \times (-j100)}{j25 - j100} \\ &= \frac{25 \times 100}{-j75} \\ &= j33.3 \Omega \end{aligned}$$

Impedance example

Obtain Z in polar form.



Obtain Z in polar form.



Method 1:

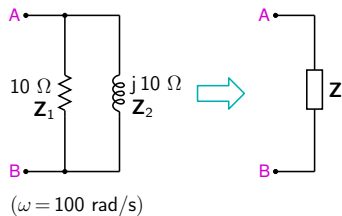
$$\mathbf{Z} = \frac{10 \times j10}{10 + j10} = \frac{j10}{1 + j}$$

$$= \frac{j10}{1 + j} \times \frac{1 - j}{1 - j}$$

$$= \frac{10 + j10}{2} = 5 + j5 \Omega$$

Convert to polar form $\rightarrow \mathbf{Z} = 7.07 \angle 45^\circ \Omega$

Obtain Z in polar form.



Method 1:

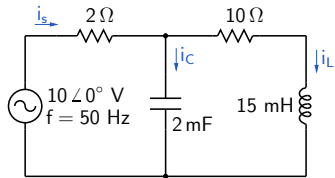
$$\begin{aligned}
 Z &= \frac{10 \times j10}{10 + j10} = \frac{j10}{1 + j} \\
 &= \frac{j10}{1 + j} \times \frac{1 - j}{1 - j} \\
 &= \frac{10 + j10}{2} = 5 + j5 \Omega
 \end{aligned}$$

Convert to polar form $\rightarrow Z = 7.07 \angle 45^\circ \Omega$

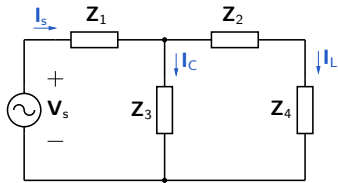
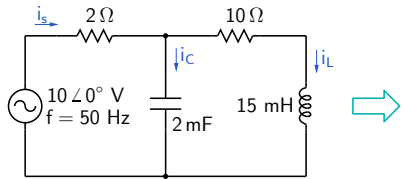
Method 2:

$$\begin{aligned}
 Z &= \frac{10 \times j10}{10 + j10} = \frac{100 \angle \pi/2}{10\sqrt{2} \angle \pi/4} \\
 &= 5\sqrt{2} \angle (\pi/2 - \pi/4) = 7.07 \angle 45^\circ \Omega
 \end{aligned}$$

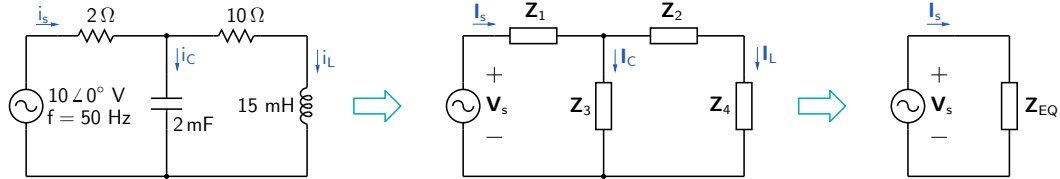
Circuit example



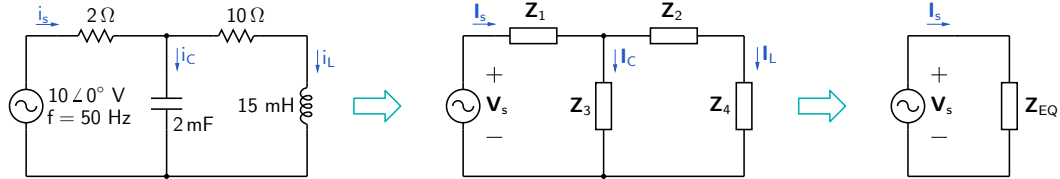
Circuit example



Circuit example

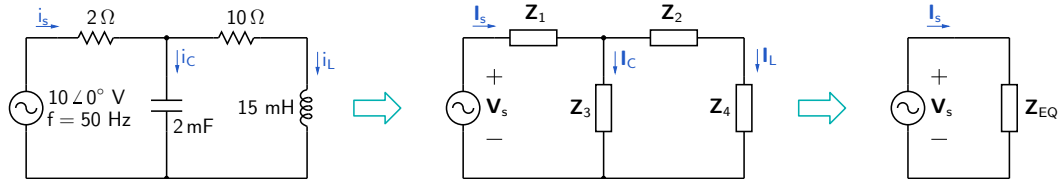


Circuit example



$$\mathbf{Z}_3 = \frac{1}{j \times 2\pi \times 50 \times 2 \times 10^{-3}} = -j1.6 \Omega$$

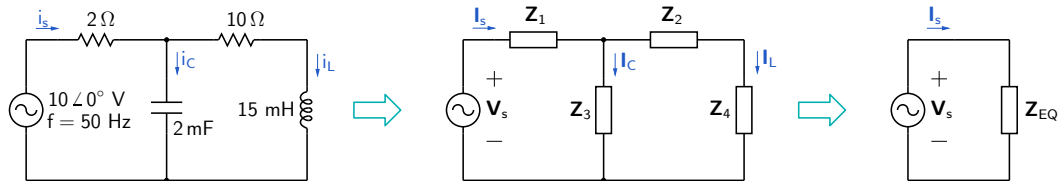
Circuit example



$$\mathbf{Z}_3 = \frac{1}{j \times 2\pi \times 50 \times 2 \times 10^{-3}} = -j1.6 \Omega$$

$$\mathbf{Z}_4 = j2\pi \times 50 \times 15 \times 10^{-3} = j4.7 \Omega$$

Circuit example

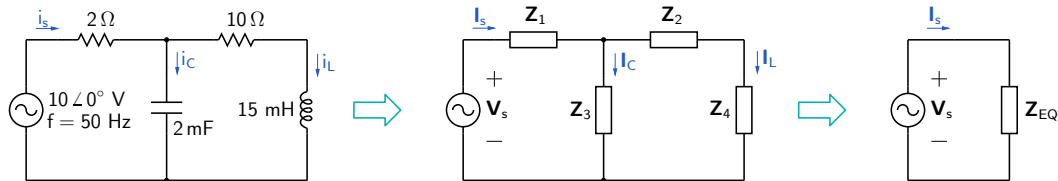


$$\mathbf{Z}_3 = \frac{1}{j \times 2\pi \times 50 \times 2 \times 10^{-3}} = -j1.6 \Omega$$

$$\mathbf{Z}_4 = j2\pi \times 50 \times 15 \times 10^{-3} = j4.7 \Omega$$

$$\mathbf{Z}_{EQ} = \mathbf{Z}_1 + \mathbf{Z}_3 \parallel (\mathbf{Z}_2 + \mathbf{Z}_4)$$

Circuit example



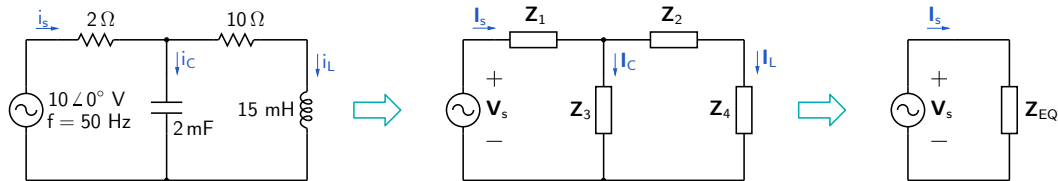
$$\mathbf{Z}_3 = \frac{1}{j \times 2\pi \times 50 \times 2 \times 10^{-3}} = -j1.6 \Omega$$

$$\mathbf{Z}_4 = j2\pi \times 50 \times 15 \times 10^{-3} = j4.7 \Omega$$

$$\mathbf{Z}_{EQ} = \mathbf{Z}_1 + \mathbf{Z}_3 \parallel (\mathbf{Z}_2 + \mathbf{Z}_4)$$

$$= 2 + (-j1.6) \parallel (10 + j4.7) = 2 + \frac{(-j1.6) \times (10 + j4.7)}{-j1.6 + 10 + j4.7}$$

Circuit example



$$Z_3 = \frac{1}{j \times 2\pi \times 50 \times 2 \times 10^{-3}} = -j1.6 \Omega$$

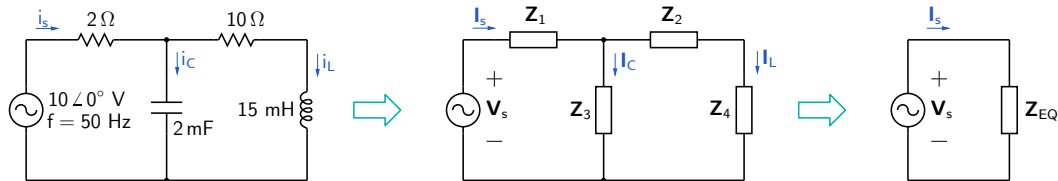
$$Z_4 = j2\pi \times 50 \times 15 \times 10^{-3} = j4.7 \Omega$$

$$Z_{EQ} = Z_1 + Z_3 \parallel (Z_2 + Z_4)$$

$$= 2 + (-j1.6) \parallel (10 + j4.7) = 2 + \frac{(-j1.6) \times (10 + j4.7)}{-j1.6 + 10 + j4.7}$$

$$= 2 + \frac{1.6 \angle (-90^\circ) \times 11.05 \angle (25.2^\circ)}{10.47 \angle (17.2^\circ)} = 2 + \frac{17.7 \angle (-64.8^\circ)}{10.47 \angle (17.2^\circ)}$$

Circuit example



$$\mathbf{Z}_3 = \frac{1}{j \times 2\pi \times 50 \times 2 \times 10^{-3}} = -j1.6 \Omega$$

$$\mathbf{Z}_4 = j2\pi \times 50 \times 15 \times 10^{-3} = j4.7 \Omega$$

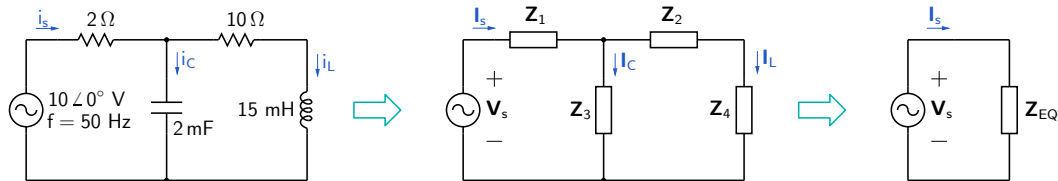
$$\mathbf{Z}_{EQ} = \mathbf{Z}_1 + \mathbf{Z}_3 \parallel (\mathbf{Z}_2 + \mathbf{Z}_4)$$

$$= 2 + (-j1.6) \parallel (10 + j4.7) = 2 + \frac{(-j1.6) \times (10 + j4.7)}{-j1.6 + 10 + j4.7}$$

$$= 2 + \frac{1.6 \angle (-90^\circ) \times 11.05 \angle (25.2^\circ)}{10.47 \angle (17.2^\circ)} = 2 + \frac{17.7 \angle (-64.8^\circ)}{10.47 \angle (17.2^\circ)}$$

$$= 2 + 1.69 \angle (-82^\circ) = 2 + (0.235 - j1.67)$$

Circuit example



$$\mathbf{Z}_3 = \frac{1}{j \times 2\pi \times 50 \times 2 \times 10^{-3}} = -j1.6 \Omega$$

$$\mathbf{Z}_4 = j2\pi \times 50 \times 15 \times 10^{-3} = j4.7 \Omega$$

$$\mathbf{Z}_{EQ} = \mathbf{Z}_1 + \mathbf{Z}_3 \parallel (\mathbf{Z}_2 + \mathbf{Z}_4)$$

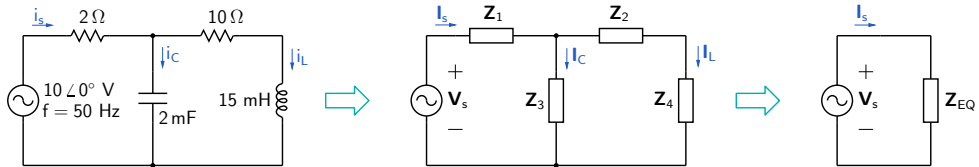
$$= 2 + (-j1.6) \parallel (10 + j4.7) = 2 + \frac{(-j1.6) \times (10 + j4.7)}{-j1.6 + 10 + j4.7}$$

$$= 2 + \frac{1.6 \angle (-90^\circ) \times 11.05 \angle (25.2^\circ)}{10.47 \angle (17.2^\circ)} = 2 + \frac{17.7 \angle (-64.8^\circ)}{10.47 \angle (17.2^\circ)}$$

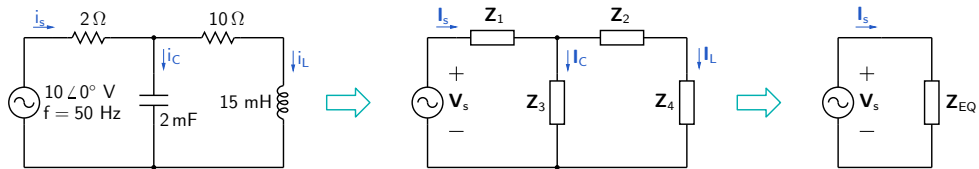
$$= 2 + 1.69 \angle (-82^\circ) = 2 + (0.235 - j1.67)$$

$$= 2.235 - j1.67 = 2.79 \angle (-36.8^\circ) \Omega$$

Circuit example (continued)

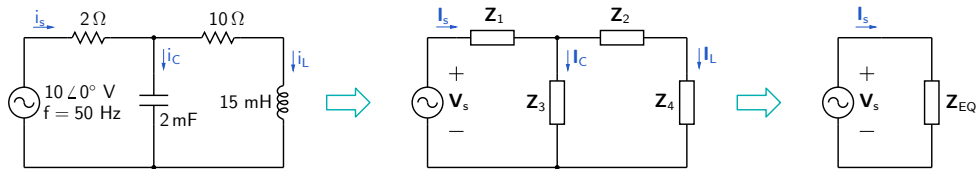


Circuit example (continued)



$$I_s = \frac{V_s}{Z_{EQ}} = \frac{10 \angle (0^\circ)}{2.79 \angle (-36.8^\circ)} = 3.58 \angle (36.8^\circ) \text{ A}$$

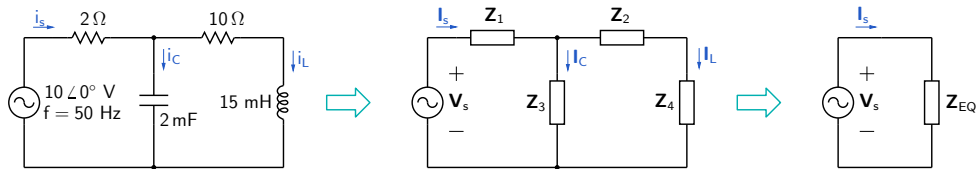
Circuit example (continued)



$$I_s = \frac{V_s}{Z_{EQ}} = \frac{10 \angle (0^\circ)}{2.79 \angle (-36.8^\circ)} = 3.58 \angle (36.8^\circ) \text{ A}$$

$$I_C = \frac{(Z_2 + Z_4)}{Z_3 + (Z_2 + Z_4)} \times I_s = 3.79 \angle (44.6^\circ) \text{ A}$$

Circuit example (continued)

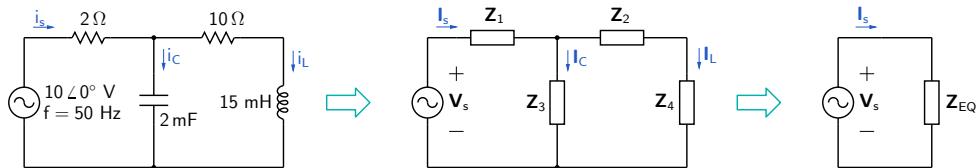


$$I_s = \frac{V_s}{Z_{EQ}} = \frac{10 \angle (0^\circ)}{2.79 \angle (-36.8^\circ)} = 3.58 \angle (36.8^\circ) \text{ A}$$

$$I_C = \frac{(Z_2 + Z_4)}{Z_3 + (Z_2 + Z_4)} \times I_s = 3.79 \angle (44.6^\circ) \text{ A}$$

$$I_L = \frac{Z_3}{Z_3 + (Z_2 + Z_4)} \times I_s = 0.546 \angle (-70.6^\circ) \text{ A}$$

Circuit example (continued)



$$I_s = \frac{V_s}{Z_{EQ}} = \frac{10 \angle (0^\circ)}{2.79 \angle (-36.8^\circ)} = 3.58 \angle (36.8^\circ) \text{ A}$$

$$I_C = \frac{(Z_2 + Z_4)}{Z_3 + (Z_2 + Z_4)} \times I_s = 3.79 \angle (44.6^\circ) \text{ A}$$

$$I_L = \frac{Z_3}{Z_3 + (Z_2 + Z_4)} \times I_s = 0.546 \angle (-70.6^\circ) \text{ A}$$

